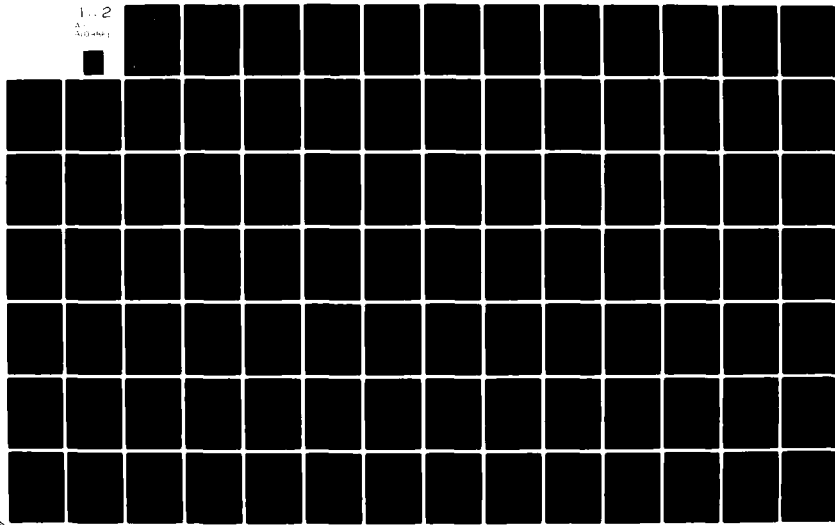


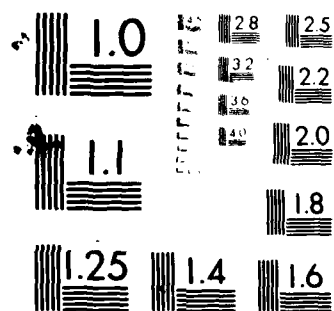
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A SHORT TAKEOFF PERFORMANCE COMPUTER PROGRAM

David Bruce Kobus
Aircraft and Crew Systems Technology Directorate
NAVAL AIR DEVELOPMENT CENTER
Warminster, Pennsylvania

25 NOVEMBER 1981

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FINAL REPORT
AIRTASK NO. ZR020302
Work Unit No. GC172

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Prepared for
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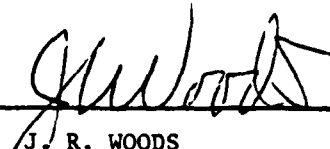
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SUMMARY

A computer program has been developed which is capable of analyzing the short takeoff of typical V/STOL aircraft configurations. This program can be used as a means for performance estimation as well as for assisting in aircraft conceptual design.

This program was written in FORTRAN for use on a CDC 6600 and uses five supporting subroutines. This report describes the analytical development and logic development for the program. In addition it includes a user description and complete listing of the program

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LIST OF SYMBOLS

a_x, a_z	Longitudinal and vertical acceleration (m/sec^2 , or ft/sec^2)
a/g	Normalized longitudinal acceleration
C_D	Drag coefficient
C_L	Lift coefficient
C_M	Pitching moment coefficient
D	Drag (N or lb f)
F_G	Gross thrust (N or lb f)
F_{GF}, F_{GA}	Fore and aft engine gross thrust (N or lb f)
F_{GH}, F_{GV}	Horizontal and vertical gross thrust (N or lb f)
g	Acceleration due to gravity ($9.8 m/sec^2$ or $32.2 ft/sec^2$)
I_{yycg}	Lateral moment of inertia ($kg-m^2$ or $slug-ft^2$)
L	Lift (N or lb f)
M_y	Lateral pitching moment (N-m or ft-lb f)
m	Aircraft mass (kg or lb)
R_F, R_A	Fore and aft gear wheel reaction force (N or lb f)
RD_F, RDA	Fore and aft engine ram drag (N or lb f)
S_x, S_z	Longitudinal and vertical distance (m or ft)
T	Time (sec)
V_x, V_z	Longitudinal and vertical velocity (m/sec or ft/sec)
WOD	Wind over deck
W_F	Fuel flow (kg/hr or lb/hr)
W	Aircraft weight ($m*g$)
α	Angle of attack (deg)
α_{MG}	Angular acceleration about main gear wheel (deg/sec^2)
γ	Flight path angle (deg)

LIST OF SYMBOLS

Δ	Increment
δ_e	Control surface deflection angle (deg)
θ_j	Jet nozzle inclination angle (deg)
θ_p	Pitch Angle (deg)
μ	Coefficient of friction
Σ	Sum

INTRODUCTION

A methodology for predicting the short takeoff (STO) performance of Vertical or Short Takeoff and Landing (V/STOL) aircraft is essential for the preliminary design of these vehicles as the propulsion system may be sized by STO requirements. Since a wide range of VSTOL configurations may be of interest to the Navy, and each would have its own unique set of thrust and drag variations during the takeoff run, a generalized computer program offers the most feasible method of analyzing STO performance.

Several STO programs currently available in the technical community were examined for applicability. It was found that each program was developed for a specific configuration and did not provide the flexibility necessary to examine arbitrary V/STOL aircraft concepts. Since the existing programs could not be easily modified, it was necessary to develop a new program.

The resulting program can be utilized for performance estimation and for aircraft conceptual design. In the performance estimation mode, inputs are aircraft aerodynamics, propulsion data, takeoff gross weight (TOGW), and STO technique while outputs are time, distance, velocity, longitudinal acceleration, lift, drag, and horizontal and vertical gross thrust. These data can be calculated at the condition of liftoff, at some specified rate of climb (R/C), or at some specified sink distance. In the conceptual design mode, inputs are given design parameters such as takeoff distance, rate of climb at liftoff, and longitudinal acceleration (with or without one engine inoperative (OEI)), and outputs such as engine size and optimum STO technique can be determined.

DISCUSSION

Theoretical Considerations

This program utilizes an open form, time history, numerical integration. The forces included in this treatment are lift, drag, gross thrust, and friction. A force diagram is presented in Figure 1. The horizontal forces are summed and divided by the aircraft mass to yield a horizontal acceleration. This acceleration in turn is equated to the following kinematic formula:

$$a_x = \frac{\Delta V_x}{\Delta T} = \frac{1}{\Delta S_x} \Delta(V_x^2)$$

Using time increments, a change in velocity and distance can be determined. More specifically, the basic equations are:

$$\text{DRAG} = C_D * 1/2 \rho V^2 S + D_{\text{ENGINE RELATED}} + D_{\text{STORE}} + D_{\text{OEI}} + D_{\text{INDUCED}}$$

where: $D_{\text{ENGINE RELATED}}$ = ram drag, spillage drag, boattail drag, etc.

$$\text{LIFT} = C_L * 1/2 \rho V^2 S + L_{\text{INDUCED}}$$

Summing vertical gross thrust components:

$$F_{GV} = F_{GFV} + F_{GAV}$$

$$F_{GV} = F_{G1} * \sin \beta_1 + F_{G2} * \sin \beta_2$$

where: $F_{G1} = F_{GF}$ - fore engine gross thrust loss

$F_{G2} = F_{GA}$ - aft engine gross thrust loss

$\beta_1 = \theta_{jF} + \theta_p$ + engine datum angle

$\beta_2 = \theta_{jA} + \theta_p$ + engine datum angle

Summing horizontal gross thrust components:

$$F_{GH} = F_{GFH} + F_{GAH}$$

$$F_{GH} = F_{G1} * \cos \beta_1 + F_{G2} * \cos \beta_2$$

Balancing the vertical forces:

$$\text{BALANCE} = W - \text{Lift} - F_{GV}$$

The change in velocity over a time increment ΔT is:

$$\Delta V_x = \Delta T * g * (F_{GH} - \text{DRAG} - \mu * \text{BALANCE}) / W$$

where: $\Delta V_x = V_{x2} - V_{x1}$

Finally, the distance gained over ΔT is:

$$\Delta S_x = 1/2 * \Delta T * ((V_{x2} - WOD)^2 - (V_{x1} - WOD)^2) / \Delta V_x$$

By using this technique the forces which vary as a function of time and angle can be accurately represented and, in addition, pilot technique can also be closely approximated. Also by using small time increments any procedural changes can be fitted through the input.

Increased program accuracy can be obtained by accounting for and by correcting a pitching moment imbalance. This is done through the following formula:

$$\sum M_y = I_{yycg} \alpha_{MG}$$

By making use of the supplied aircraft moment of inertia and a power-on pitching moment, an angular acceleration about the main gear can be taken into account. The moment about the vehicle center of gravity is:

$$\text{MOMENT} = C_M * 1/2 \rho V^2 * MAC$$

The fore gear wheel reaction force is therefore:

$$R_F = (\text{BALANCE} * \beta_3 - \text{MOMENT}) / (LRF + \beta_3 + \cos \theta_p)$$

where: $\beta_j = LRA \cdot \cos \theta_p + LRA \cdot \mu \cdot \sin \theta_p + LR \cdot \mu \cdot \cos \theta_p - LR \cdot \sin \theta_p$

See Table I for the definitions of LR, LRA, LRF and MAC.

If the supplied aerodynamic data is a function of control surface deflection, the deflection required to nullify any moments can be calculated. This is accomplished by the following algorithm:

```

initialize  $\alpha$ ,  $\theta_j$  and  $\delta e$ 
 $C_L = f(\alpha, \delta e, \theta_j)$ 
 $C_D = f(C_L, \delta e, \theta_j)$ 
 $C_M = f(C_L, \delta e, \theta_j)$ 

DRAG =  $f(C_D)$  + DENGINE RELATED + DSTORE + DOEI + DINDUCED

LIFT =  $f(C_L)$  + LINDUCED

MOMENT =  $f(C_M)$ 

 $F_{GV} = f(F_G, \theta_j, \theta_p)$ 

BALANCE = W - Lift -  $F_{GV}$ 

 $R_F = f(BALANCE, MOMENT)$ 

iterate  $\delta e$  until  $R_F = 0$ 

```

Rates of climb or sink can be calculated if the horizontal component of velocity is considered much larger than the vertical component ($V_z < .02 V_x$). Here the vertical acceleration is: $a_z = \frac{\Delta V_z}{\Delta T}$

and the vertical velocity is: $V_z = \frac{\Delta S_z}{\Delta T}$

Hence, climb or sink accelerations, velocities, and distances can be determined. For rate of climb velocity over the ΔT increment:

$$a_z = (-BALANCE) \cdot g / w$$

$$\bar{a}_z = 1/2 \cdot (a_{z2} + a_{z1})$$

To determine the incremental ROC:

$$\Delta ROC = \bar{a}_z \cdot \Delta T$$

For sink off the bow distance over the ΔT increment:

$$a_z = BALANCE \cdot g / w$$

$$\bar{a}_z = 1/2 \cdot (a_{z2} + a_{z1})$$

$$\Delta V_z = \bar{a}_z \cdot \Delta T$$

$$V_{z2} = V_{z1} + \Delta V_z$$

$$\bar{V}_z = 1/2 * (V_{z2} + V_{z1})$$

The incremental sink distance is:

$$\Delta SINK = \bar{V}_z * \Delta T$$

If an instantaneous ROC at liftoff is needed, the following formula is used:

$$a_x = (F_{GH} - DRAG - \mu * BALANCE) / W$$

Assuming a small flight path angle at liftoff:

$$ROC_{instantaneous} = V \sin \gamma \approx V\gamma$$

$$\text{Where } V\gamma = V * ((LIFT + F_{GV} - W) / F_{GH})$$

The main program logic, which illustrates how all the above equations are implemented, is presented in Appendix D.

Program Description

In addition to the main program, which performs the computations on the dynamic equations, there are five supporting subroutines, as described below.

TAKE 5 - In the formulation of the STO computer program a four degree-of-freedom interpolation routine was developed from an earlier three degree-of-freedom routine (reference (a)). This was done to accomodate aerodynamic inputs which are a function of four variables.

This subroutine has two modes of operation. In the first mode, table data representing aerodynamic and propulsion characteristics are input and stored. Each table is assigned a predetermined reference number. In the second mode, table data is interpolated and extrapolated by the function SPLNQ1 for use in the dynamic calculations. TAKE5 subroutine logic is presented in Appendix D.

SPLNQ1 - This function is used to interpolate or extrapolate tabular data. The interpolation is calculated using a local curve fit scheme described in reference (b). Linear extrapolations are made using each end point slope of the local curve fit.

UPDATE - This subroutine is used to reshape data arrays into a form usable by the function SPLNQ1.

SNEST - This is an iteration subroutine used to solve one degree-of-freedom problems. A slope intercept convergence technique is employed.

ATMOS - This is a 1962 standard atmosphere table which returns properties of density, pressure, temperature, and sound velocity for an input geometric altitude.

The data required for the program consists of a series of single-value, fixed inputs and multiple-valued tabular inputs. The form of the computer data deck necessary to make a run is presented in Figure 2.

The tabular data includes:

- Gross thrust as a function of Mach number and engine speedup time.
- Fuel flow as a function of Mach number and engine speedup time.
- Drag coefficient as a function of lift coefficient, control surface deflection, jet nozzle inclination, and velocity.
- Lift coefficient as a function of angle of attack, control surface deflection, jet nozzle inclination, and velocity.
- Induced lift increment as a function of jet inclination angle
- Induced drag increment as a function of jet inclination angle
- Pitching moment coefficient as a function of lift coefficient, control surface deflection, jet nozzle inclination, and velocity.
- Aircraft moment of inertia as a function of aircraft mass.
- Distance from aircraft center of gravity to main gear wheel as a function of aircraft mass.
- Gross thrust loss relative to zero nozzle deflection gross thrust as a function of jet nozzle angle.
- Throttle dependent, ram, and external store drag as a function of Mach number.

These tabular inputs are graphically illustrated in Appendix A.

The fixed inputs consist of aircraft size and mass data, ambient conditions, initial thrust vector angles and control surface deflections, rotation rates for the nozzles and specification for events that may occur during the takeoff run (e.g. loss of an engine). Table I contains a fixed input variable list.

Program Options

Available to the user are two main options which concern the type of STO vehicle that can be approximated. First, is a Harrier type vehicle which maintains moment balance by a reaction control system, rotates its jet nozzles, and pitches up at a given rate and at a predetermined airspeed. Second, is a vehicle which maintains moment balance by a control surface deflection and has a fixed jet nozzle angle.

For vehicles using control surfaces to maintain moment balance on the ground, the program will search for the start of auto rotation (stick free pitch up) and either give information on the rotation of the aircraft about the aft wheel or attempt to correct this rotation by the deflection of a control surface. Pertinent tabular inputs for this vehicle type include:

$$C_M = f(C_L, \delta_e, \theta_j, V_x)$$

$$I_{yyCG} = f(m)$$

$$\text{Distance from CG to aft wheel} = f(m)$$

Fixed inputs concerned with this type of vehicle are LR, LRA, LRF, DELTAE, VSTARR, MAC, SEGMENT, IYYCG, XCG, YCG, DELMAX and ALPHMIN. Examination of the above data, by considering the descriptions made in Table I and Appendix A, will clearly illustrate the options available for this type of vehicle.

If a Harrier type vehicle is to be considered, the previously mentioned input can be ignored.

By viewing the form of the remaining tabular and fixed input, in Table I and Appendix A, it is seen that a wide variety of pilot techniques can be approximated. This is because any continuous or discontinuous tabular aerodynamic or propulsion function can be fitted. In addition, a large variety of fixed input switches are available for duplication of aircraft rotation and thrust deflection at any prescribed airspeed.

The following comments offer some additional options that can be implemented for a Harrier type vehicle.

1. If a series of data cases are to be run, put the additional aircraft weights or velocities in ascending order. Set RUN not equal to zero for interpolated weight or set RUN and PSINT not equal to zero for interpolated pitch speed.
2. Apply variables RS, ALPHARR, ALPHAAR, ALPHA, PHI2, PHI2AR, and PS for desired rotation method. For the fore engine nozzle variation apply RSF, PHI1, PHI1AR, PHI1RR accordingly.
3. Set NOEDRAG not equal to zero and NOSTORE not equal to zero if engine related drags and store drags exist in reference table 33 (nos. 1 and 2) (see Appendix A). Set NODOEI not equal to zero if engine out drag exists in reference table 33 (no. 3).
4. For OEI at brake release, read in NEF = NEA = 0.5 or any appropriate scale down, or put in single engine tabular data inputs and add failed engine drag in store drag (reference table 33 (no. 2)). For OEI at liftoff, set EFAILA not equal to zero and OEILOSF to an appropriate front engine scale down value and add failed engine drag as additional drag (reference table 33 (no. 3)). Set OEITAB not equal to zero for OEI at liftoff when thrust, fuel flow, and drags (engine related and external store) for one engine out are supplied in tabular form (reference table 10, 11, and 33 (nos. 3 and 4)). Put in RAM for a constant ram drag scale down during OEI.

5. For dynamic R/C constraint, put in ROC limit. Set PHONY not equal to zero when instantaneous R/C is desired (fore and aft nozzle angles and aircraft pitch angle are set to maximum values for instantaneous R/C calculation). Set SINKD to bow height for sink calculations. (If PS, RS, and RSF have not been reached at SINKD, these variables will be set to the airspeed at SINKD). NOTE: rate of climb and sink estimates assume that the horizontal velocity is much greater than the vertical velocity.

ACKNOWLEDGEMENTS

A mention of appreciation is given by the author to Michael Caddy who developed the supporting subroutines and to John Cyrus for his technical concepts.

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- (a) Caddy, M. J., "TREAD/TLOOK - Multipurpose Computer Routine for Interpolation and Extrapolation of Tabular Data," NAVAIRDEVCEEN Report No. NADC-76366-30, 11 January 1977
- (b) Akima, Hiroshi, "Interpolation and Smooth Curve Fitting Based on Local Procedures," Institute for Telecommunication Sciences, 1 March 1972

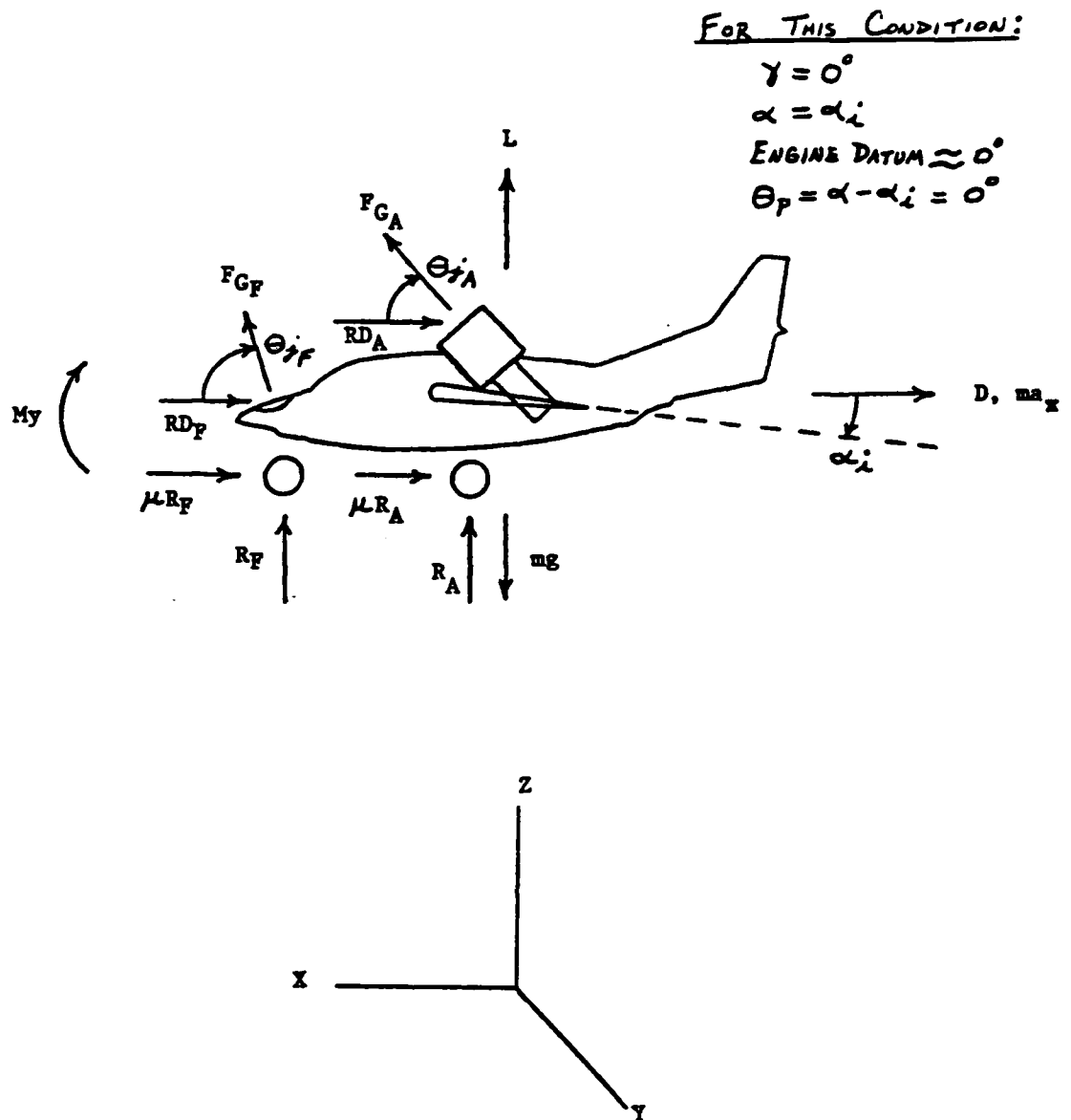


FIGURE 1. Force Diagram (Ground Run)

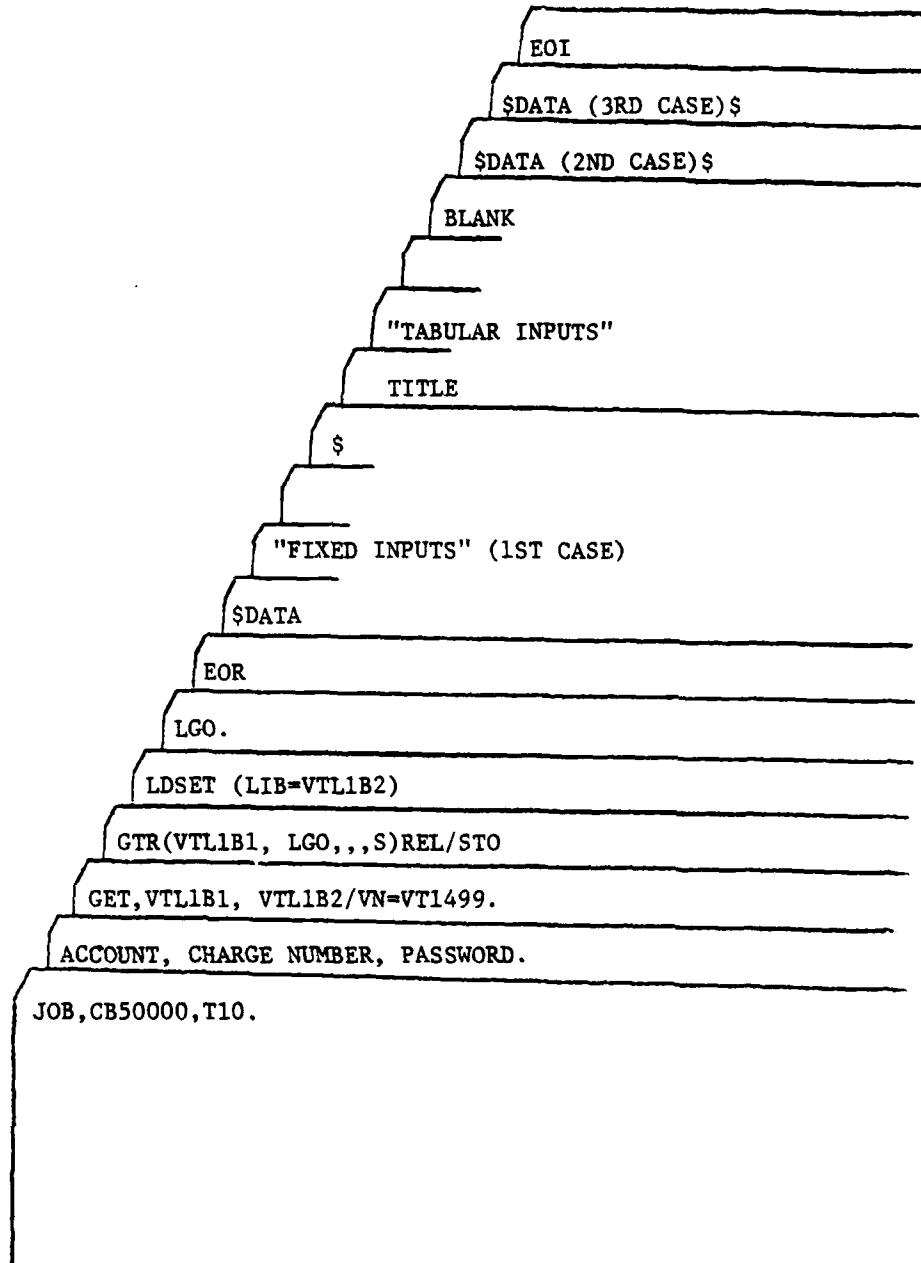


FIGURE 2. Data Input Deck Structure

TABLE I
FIXED INPUT VARIABLE LIST

<u>Variable Name</u>	<u>Description</u>	<u>Units</u>	<u>Default Value</u>
ALPHA	Initial angle of attack (for C_L - α curve)	deg.	----
ALPHAAR	Pitch angle after rotation	deg.	0.0
ALPHARR	Pitch up rotation rate	deg/sec	0.0
ALPHMIN	Maximum angle of attack before auto rotation control attempted	deg	0.0
ALT	Field altitude	m. or ft.	0.0
ANGFRL	Initial fuselage reference line angle (for engine reference)	deg	0.0
DELMAX	Maximum control surface deflection angle (maximum δ_e)	deg	----
DELTAE	Initial control surface deflection angle	deg	0.0
DISTMAX	Abort run if this takeoff distance is exceeded	m. or ft.	106
DT	Time integration increment	sec.	.05
EDATUM	Engine datum (with respect to fuselage reference line)	deg	0.0
EFAILA	If \neq zero, failure of one engine assumed at liftoff	----	0.0
E1	If \neq zero, two thrust vectors are present	----	0.0
FLDTEMP	Field ambient temperature	$^{\circ}\text{C}$ or $^{\circ}\text{F}$	59.
IPRINT	If \neq zero, a time history of parameters will be printed	----	0
IYYCG	Constant aircraft moment of inertia	kg-m ² or slug-ft ²	----
LR	Vertical distance from center of gravity (CG) to ground	m. or ft.	----
LRA	Horizontal distance from CG to aft wheel	m. or ft.	----
LRF	Horizontal distance from CG to fore wheel	m. or ft.	----
MAC	Mean aerodynamic chord	m. or ft.	----
METRIC	If \neq zero, metric units present	----	0
MU	Wheel friction coefficient	----	.02
NEA	Number of lift cruise engines	----	1.
NEF	Number of lift engines	----	1.
NODOEI	If \neq zero, tabular engine out drag present	----	0
NOEDRAG	If \neq zero, tabular throttle dependent drag present (includes ram drag)	----	0
NOSTORE	If \neq zero, tabular external store drag data present	----	0
NPRINT	If \neq zero, tabular input will be printed	----	0
OEILOS	Lift engine scale down when OEI occurs	----	.0
OEITAB	If \neq zero, OEI at liftoff assumed with tabular OEI data present	----	0.
PHI1	Initial lift engine jet nozzle angle (with respect to engine datum)	deg	0.0
PHILAR	Lift engine nozzle angle after rotation	deg	0.0

TABLE I
(Continued)

FIXED INPUT VARIABLE LIST

<u>Variable Name</u>	<u>Description</u>	<u>Units</u>	<u>Default Value</u>
PHI1RR	Lift engine nozzle rotation rate	deg/sec	0.0
PHI2	Initial lift cruise engine jet nozzle angle (with respect to engine datum)	deg	0.0
PHI2AR	Lift cruise engine nozzle angle after rotation	deg	0.0
PHI2RR	Lift cruise nozzle rotation rate	deg/sec	0.0
PHONY	If \neq zero, instantaneous R/C is calculated	-----	0.0
PS	Pitch up aircraft speed	m/sec or ft/sec	0.0
PSINT	If \neq zero, and RUN \neq zero, will give interpolated pitch up speed	-----	0.0
RAM	Ram drag scale factor for OEI; if default value selected, tabular OEI ram drag is used	-----	1.
RDSCALE	Tabular ram drag scale factor	-----	1.
REVTIME	Engine speed up time	sec	0.0
ROC	If \neq zero, dynamic liftoff characteristics at this R/C will be given	m/sec or ft/sec	0.0
RS	Airspeed which initiation of lift cruise engine nozzle rotation occurs	m/sec or ft/sec	0.0
RSF	Airspeed which initiation of lift engine nozzle rotation occurs	m/sec or ft/sec	0.0
RUN	IF \neq zero, STO distance to determine interpolated TOGW	m or ft	0.0
S	Wing area	m ² or ft ²	-----
SEGMENT	If default value used, no pitching moment estimation is entered in calculations; if = 1, auto rotation included in estimates; and if = 2, elevator correction to auto rotation applied	-----	0
SINKD	If \neq zero, this is bow distance for sink calculations	m or ft	0.0
VSTARR	Maximum velocity before which a constant linear extrapolation of aerodynamic tabular data occurs	m/sec or ft/sec	0.0
W	Aircraft mass	kg or lb	-----
WOD	Wind over deck (+ for headwind, - for tailwind)	m/sec or ft/sec	0.0
XCG	Constant horizontal distance from CG to main gear wheel (presumes no tabular CG locations inputting)	m or ft	-----
YCG	Constant vertical distance from CG to main gear wheel (supposes no tabular CG locations inputted)	m or ft	-----

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APPENDIX A

TABULAR INPUTS

A list of the tabular data inputs is presented in graphical form. An example of this data in numerical form can be found in Appendix B and reference (a).

Table Reference No. 13
 $C_D = f(C_L, \delta_e, \theta_j, V_x)$

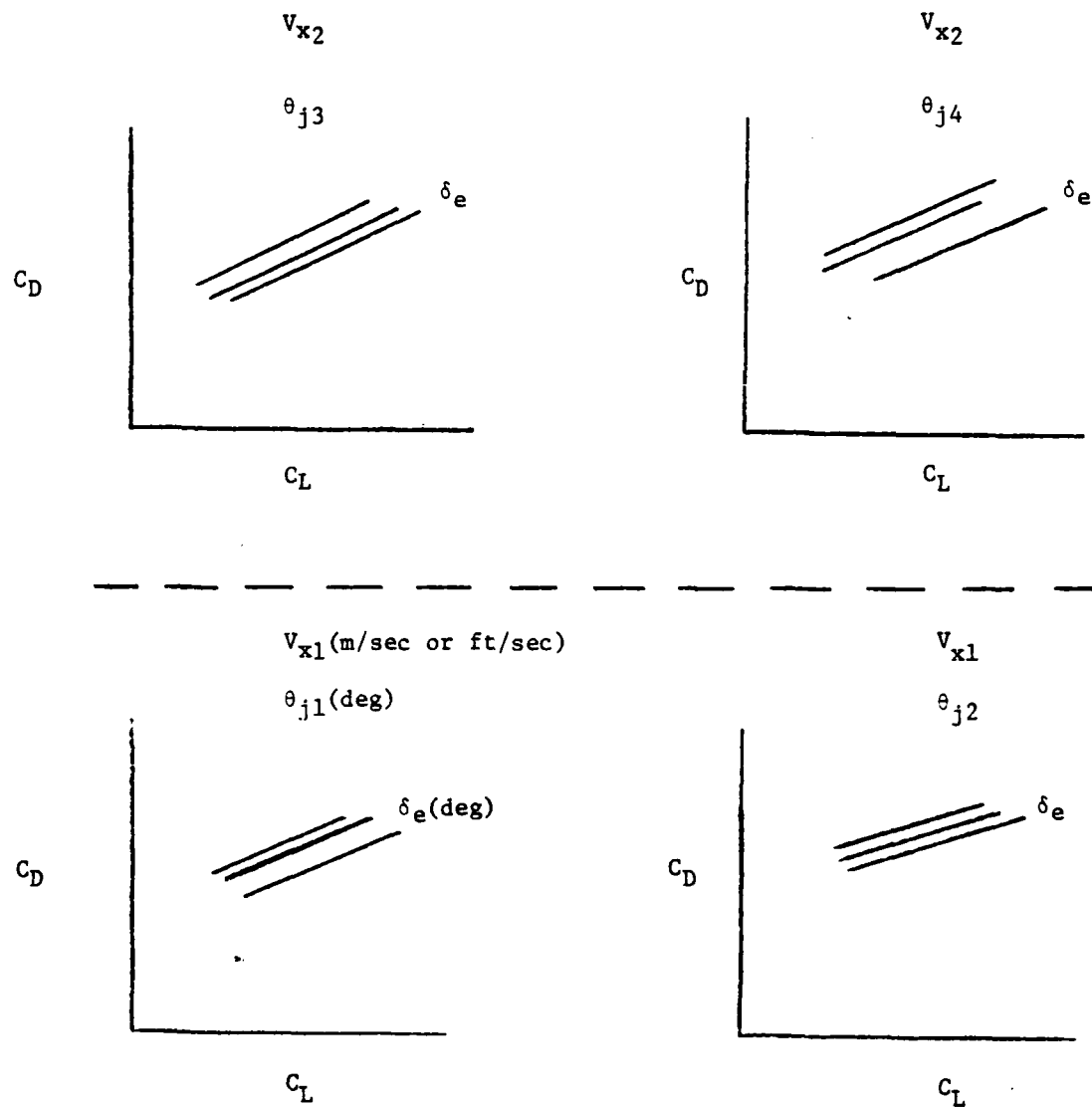


FIGURE A1. Drag Coefficient Tabular Input

Table Reference No. 14
 $C_L = f(\alpha, \delta_e, \theta_j, V_x)$

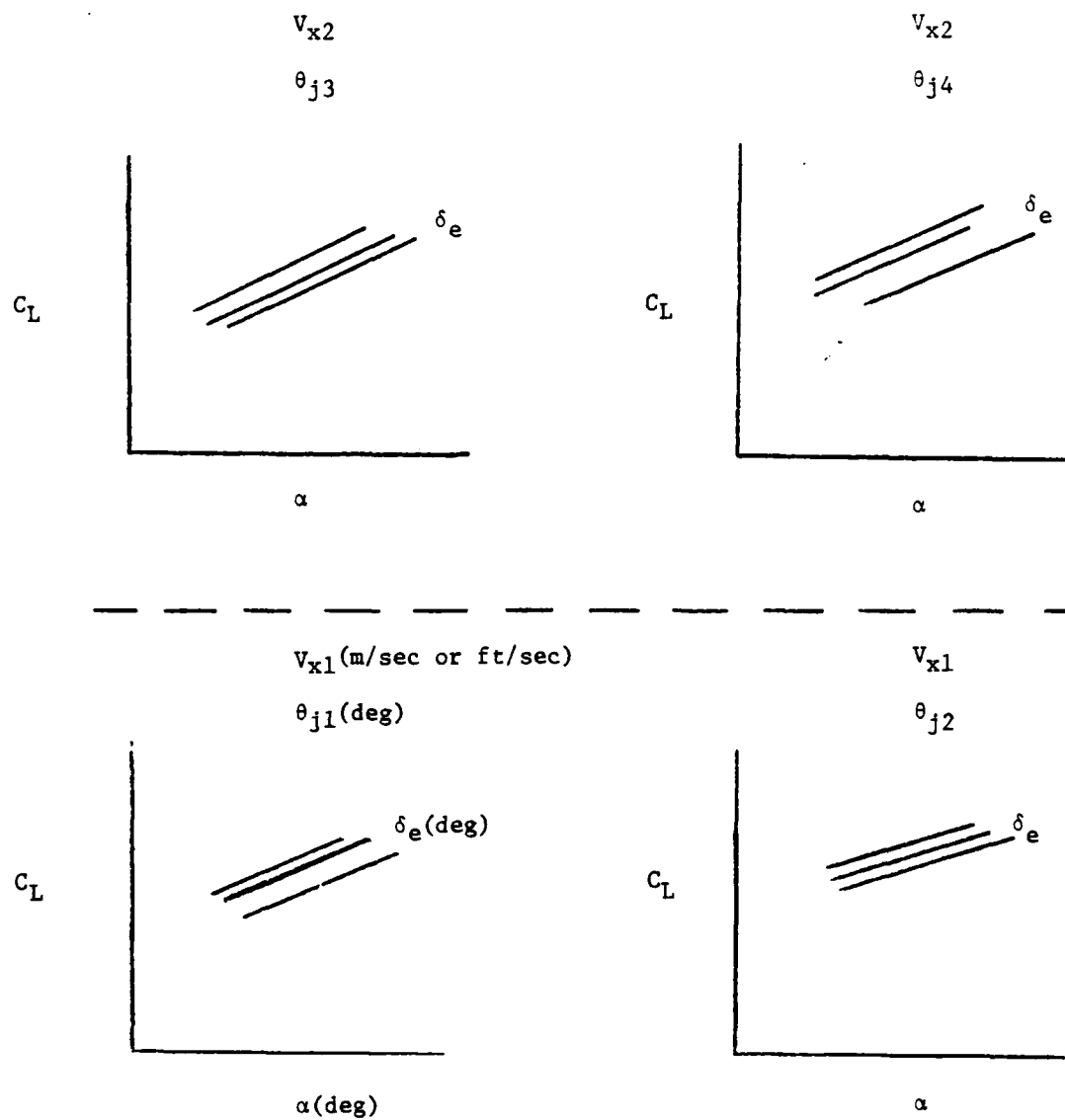


FIGURE A2. Lift Coefficient Tabular Input

Table Reference No. 10
 $F_G = f(\text{MACH, Engine Type, REVTIME})$

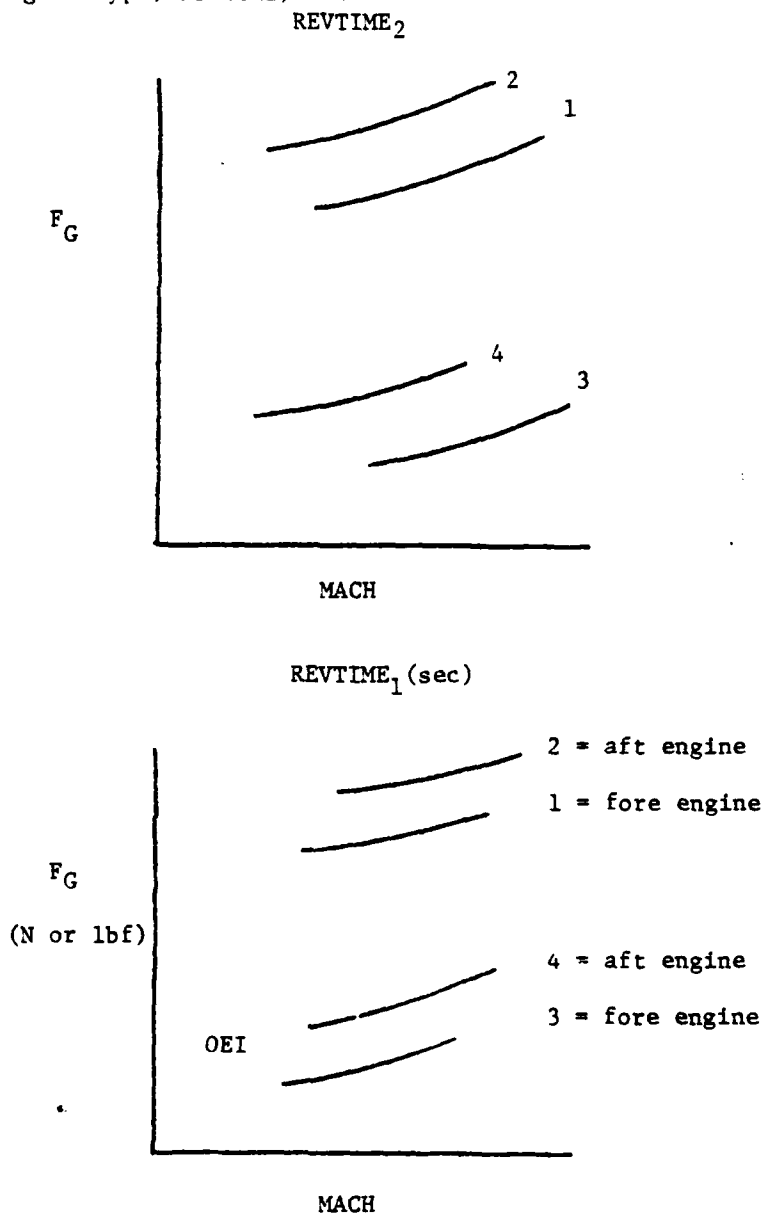


FIGURE A3. Gross Thrust Tabular Input

Table Reference No. 11
 $W_F = f(\text{MACH, Engine Type, REVTIME})$

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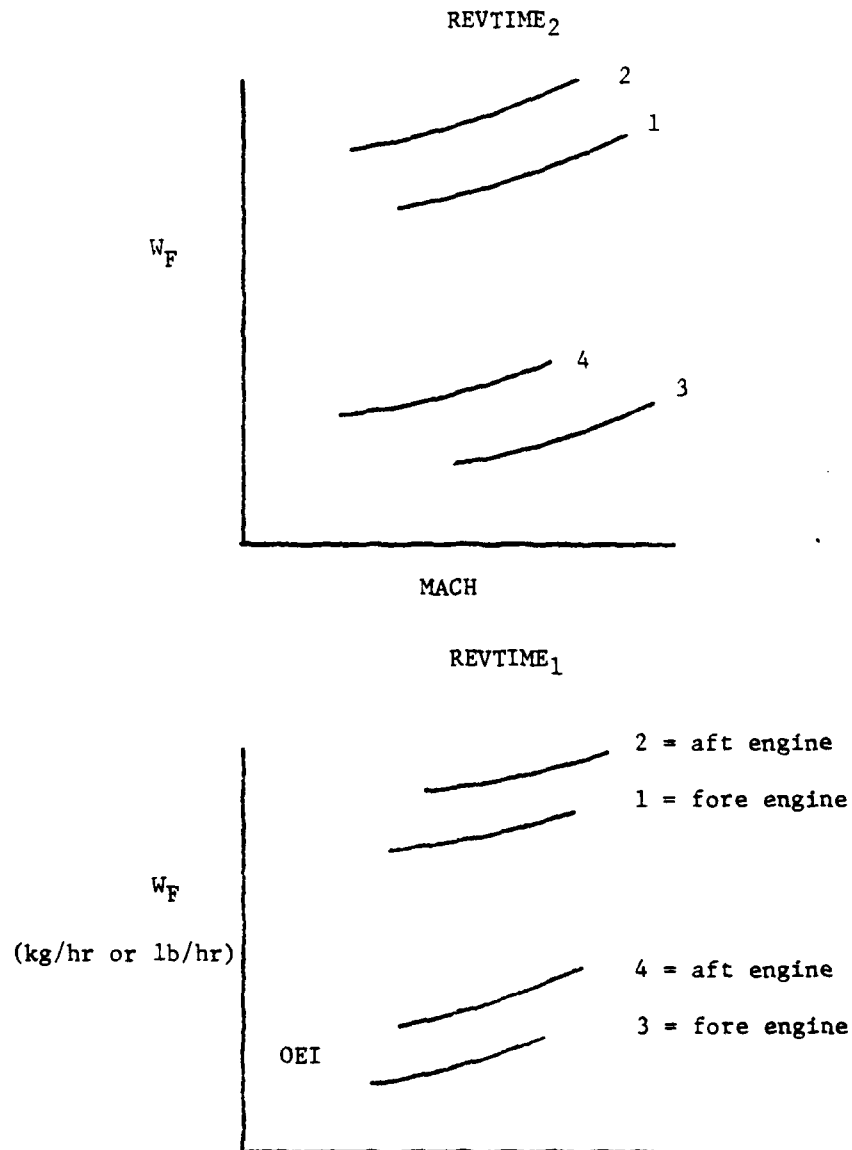


FIGURE A4. Fuel Flow Tabular Input

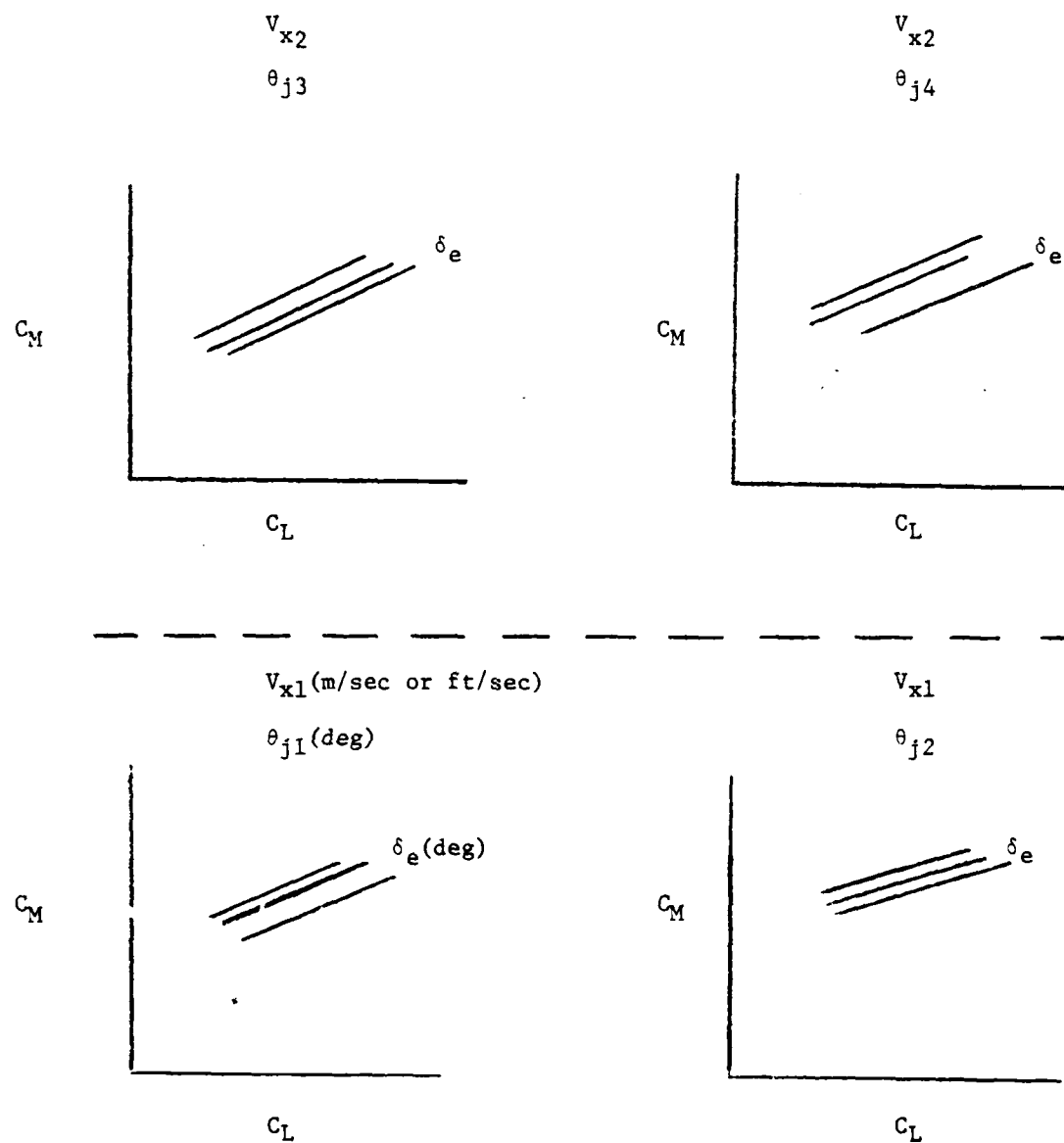


FIGURE A5. Moment Coefficient Tabular Input

Table Reference No. 30
 $I_{yyCG} = f(m)$

I_{yyCG}
 (kg-m² or slug-ft²)

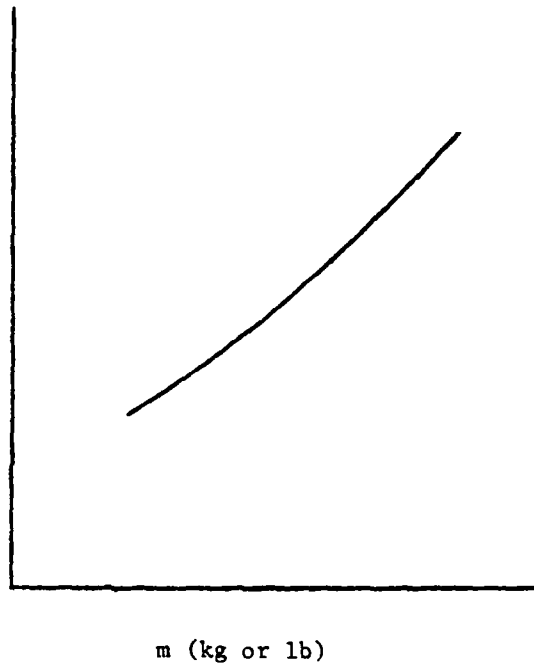


FIGURE A6. Moment of Inertia Tabular Input

Table Reference No. 15
 $\frac{\Delta L}{F_G}, \frac{\Delta D}{F_G} = f(\theta_j)$

$$1 = \frac{\Delta L}{F_G}$$

$$2 = \frac{\Delta D}{F_G}$$

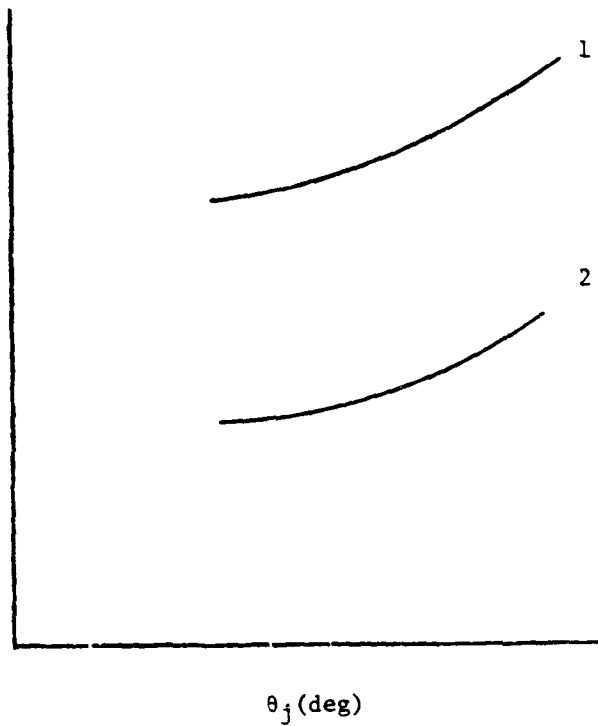


FIGURE A7. Induced Lift and Drag Tabular Input

Table Reference No. 33
 $D = f(\text{MACH}, \text{Drag Type})$

D
 (N or lbf)

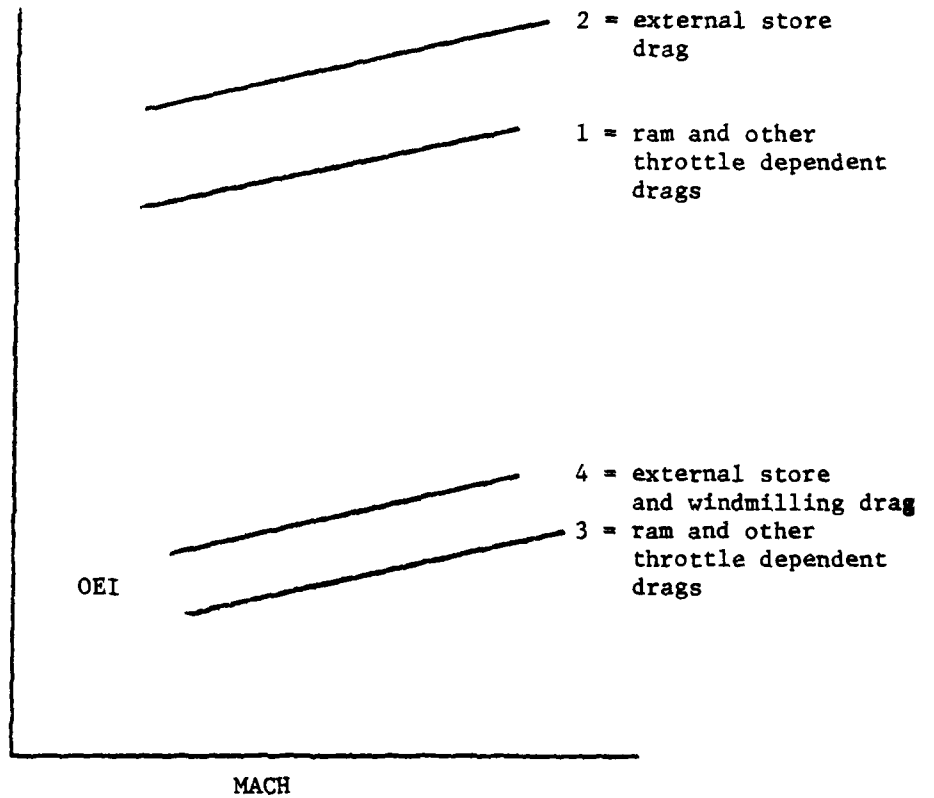


FIGURE A8. External Store and Ram Drag Tabular Input

Reference Table No. 31
 $X_{CG}, Y_{CG} = f(m)$

1 = X_{CG}
 2 = Y_{CG}
 (m or ft)

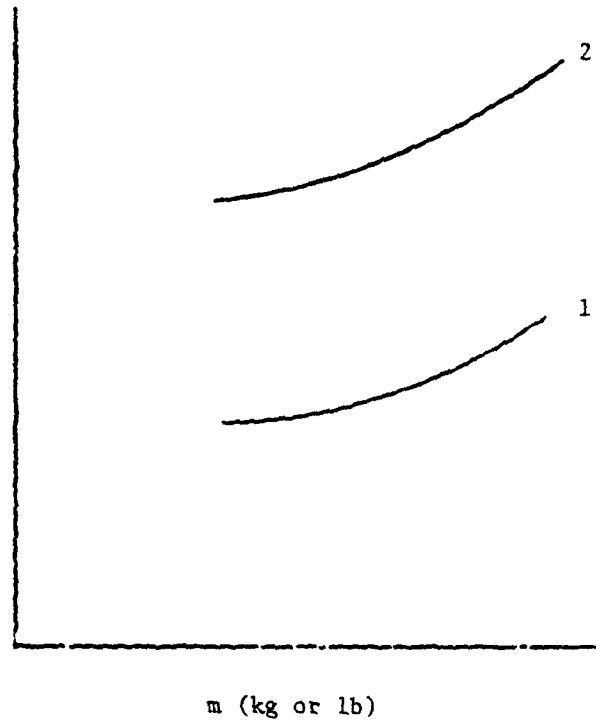


FIGURE A9. Center of Gravity Location Tabular Input

Reference Table No. 12

$$\frac{F_{G\text{Loss}}}{F_{G(\text{no nozzle deflection})}} = f(\theta_j, \text{ENGINE TYPE})$$

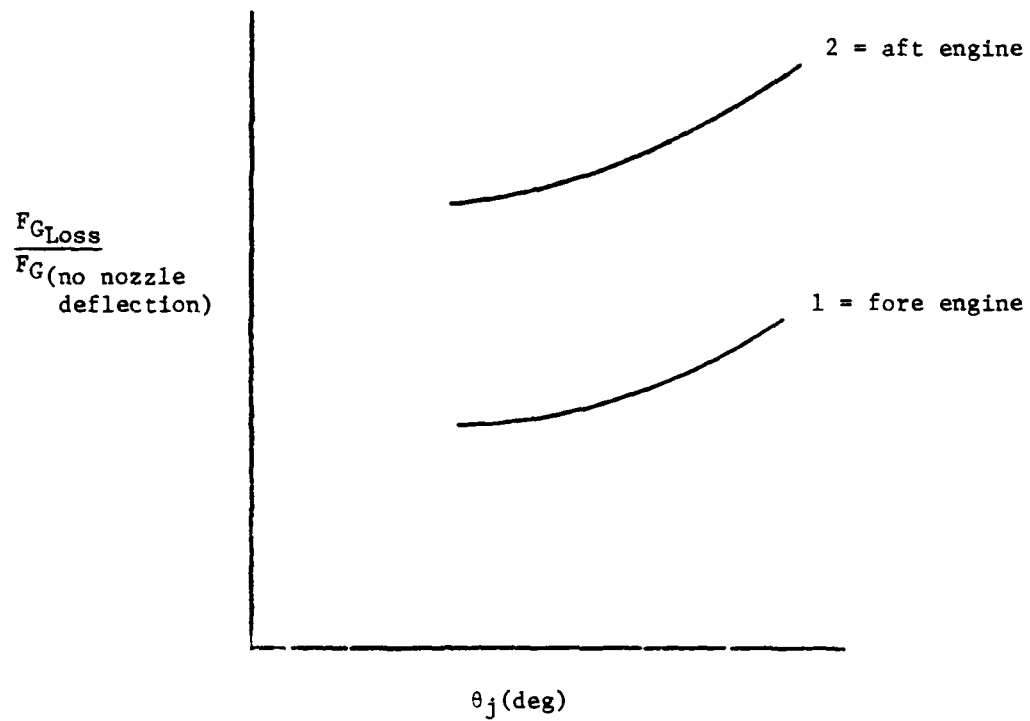


FIGURE A10. Gross Thrust Loss Tabular Input

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APPENDIX B

EXAMPLE CASE

An example card deck and printout is presented. The required programs, supporting subroutines, and control cards to execute this program with any charge number under the NAVAIRDEVCEEN KRONOS 2.1 operating system is illustrated. An explanation of the sample case is also presented.

Example Case

Card Deck

An example card deck listing, similar in form to the arrangement illustrated in Figure 2, is presented. As shown, three cases are to be run and they require less than 50,000 octal central memory core and ten octal seconds central processor unit time.

For the first case an aircraft, with a wing area of 430 square feet, is initially resting on the ground with a wing angle of attack and fuselage reference line at negative five degrees from the horizontal. The lift engine nozzle angle is set at 45 degrees while the cruise engine nozzle angle is set at five degrees. Both nozzle angles are with respect to the fuselage reference line (or to the engine datum line for the cruise engines). On examining the initial case's fixed inputs, at an airspeed of 66 ft/sec the vehicle will rotate its lift engine nozzles to 75 degrees at a rate of 15 degrees/sec and it will rotate its cruise engine nozzles to 54 degrees also at 15 deg/sec. At an airspeed of 80 ft/sec the aircraft will pitch up to 13 degrees at 5.9 deg/sec. This vehicle weighs 40,000 lbs. Additional fixed inputs state that the vehicle has a tabular ram drag input (NOEDRAG), two thrust vectors are present (E1), and the analysis is for a 90°F day (FLDTEMP). The default value of METRIC causes English units to be used. If the deck run exceeds 750 feet the case runs will be terminated. The variables RUN and PSINT are used, in combination, to interpolate or extrapolate the case values of PS. This is to determine the appropriate value of this variable for a deck run of 400 feet. The variable SINKD specifies the carrier bow length and signals for sink calculations to be done for this case. The IPRINT parameter indicates that a time history of pertinent parameters for this specific case will be printed.

Example tabular data includes C_L versus α , drag polars, engine thrusts, ram drag, and induced aerodynamics. The table numbers used for each table are predetermined as outlined in Appendix A. Notice that omitted input, such as fuel flow data, is assumed to be zero by the program.

The second and third fixed input cases switch off the sink calculations and the time history printout and change the lift and cruise nozzle rotation initiation airspeeds. These additional cases also change the airspeed in which the vehicle begins pitching up. Note that a maximum of one card is permitted for each additional case. For the additional cases a value for ROC causes dynamic rate of climb calculations to be made.

TEST.C950001.T10.
 ACCOUNT.CHARGE NUMBER.PASSWORD.
 GET.VTL191.VTL192/UN=VT1499.
 GET.VTL191.LGO...SIFEL/STO
 LDSET(LI9=VTL192)
 LGO.

END OF RECORD

\$DATA ALPHA=-5.5430.PM12=5.PM12AR=54.PM12RR=15.ALPHARR=5.9.ALPHAAR=13.
 ANAFRL=-5.NOEDRAF=1.E1=1.FLDTEMP=90.PM11=45.DISTMAX=750.PM11AR=75.
 PM11RR=15.PS=46.PS=40.RSF=66.W=40000.IPRINT=1.PSINT=1.WIND=400.
 SINKP=200.NPRINT=1.

5

EXAMPLE CASE

14 EXAMPLE CL VS. ALPHA TABLE

VEL	1	0.						
PM12	3	0.	50.	40.				
DLTE	1	0.						
ALPH	9	-0.	-4.	0.	4.	8.	12.	16.
		20.						
CL	4	-0.48	-0.175	0.175	0.45	0.78	1.04	1.375
		1.49						
DLTE	1	0.						
CL	8	-0.13	0.15	0.42	0.69	0.96	1.2	1.45
		1.57						
DLTE	1	0.						
CL	9	0.34	0.59	0.86	1.11	1.34	1.47	1.56
		1.55						

EOT

13 EXAMPLE CRAG POLARS (POWER OFF) TABLE

DUMM	1	0.					
PM12	1	0.					
DLTE	1	0.					
CL	6	-0.4	0.	0.4	0.8	1.2	1.4
CD	6	0.14159	0.02938	0.03742	0.06533	0.17463	0.22905

EOT

10 EXAMPLE ENGINE THRUST TABLE

DUMM	1	0.					
TIME	1	0.					
SET	4	1.	2.	3.	4.		
MACH	5	0.	0.05	0.1	0.15	0.2	
FG	5	13755.	14044.	14332.	14875.	15417.	
FG	5	29437.	29988.	30538.	31606.	32673.	
FG	5	10994.	11330.	11565.	12342.	13018.	
FG	5	23734.	24346.	24958.	25161.	27363.	

EOT

33 EXAMPLE MAX DRAG TABLE

DUMM	1	0.				
TIME	1	0.				
SET	2	1.	3.			
MACH	5	0.	0.05	0.1	0.15	0.2
MACH	5	0.	3926.	9123.	12240.	14021.
MACH	5	0.	3902.	7931.	12023.	14486.

EOT

15 EXAMPLE INCURRED AERODYNAMICS TABLE

DUMM	1	0.			
Y	1	0.			
SET	2	1.	2.		
PM12	3	0.	50.	100.	
DEL	3	0.02	0.12	0.210	
DEL	3	27.3	44.5	64.7	
DEL	3	-0.358	-0.031	0.042	

EOT

NADC-81259-60

BLANK CARD
SDATA SINK0=0,ROC=1,A7,PS=90,RC=76,RSF=76,IPRINT=06
SDATA SINK0=0,ROC=1,A7,PS=100,PS=A4,RSF=A4,IPRINT=06
NOTE: MAXIMUM OF ONE CARD FOR FAC= ADDITIONAL CASE.
END OF INFORMATION

Printout

The computer printout of the previously mentioned card deck is now presented. On the second page of the printout a loader map illustrating all the supporting subroutines and their individual core requirements is presented. On the bottom of this page the fixed inputs for the first case are shown. The variable NPRINT enables the tabular input to be printed in full on the following five successive pages. This data, in turn, is followed by a summary of core requirements for each table. Next, the output data begins with a time history of the first of three sample cases. Each element is a successive point in a time variance of parameters. These parameters include:

W - Aircraft mass (kg or lb) (English units for this example)
 V - Vehicle airspeed (m/sec or ft/sec)
 L - Lift force (N or lbf)
 DR - Drag force (N or lbf)
 RF - Nose gear reaction force (N or lbf) (not used in this example)
 EDRG - Engine related drags (N or lbf)
 FN2 - Cruise engines gross thrust (N or lbf)
 PH2I - Cruise engine nozzle angle (deg)
 ALPHA - Angle of attack (deg)
 T - Time (sec)
 D2 - Distance (m or ft)
 BALANCE - Lifting forces minus weight (N or lbf)
 PH1I - Lift engine nozzle angle (deg)
 FN1 - Lift engines gross thrust (N or lbf)
 C_L - Lift coefficient
 C_D - Drag coefficient
 C_M - Pitching moment coefficient (not used this example)
 A/G - Normalized longitudinal acceleration
 RHO - Atmospheric density (kg/m³ or slug/ft³)
 DELTAE - Control surface deflection angle (deg) (not used this example)

The following parameters were not printed in this listing because they were not used for this example case.

DALPHAD - Angle of attack increment caused by auto rotation (deg)
 IYYCG - Lateral aircraft moment of inertia (kg-m² or slug-ft²)
 XCG - Horizontal distance from CG to main gear wheel (m or ft)
 YCG - Vertical distance from CG to main gear wheel (m or ft)
 N - Iteration number for elevator correction to counter auto rotation
 RF - Nose gear reaction force during iteration (N or lbf)
 DELTAE - Control surface deflection during iteration (deg)

The following parameters are printed if dynamic rate of climb calculations are made. These parameters are printed only after liftoff.

ROC - Dynamic rate of climb (m/sec or ft/sec)
 ACCY - Vertical dynamic acceleration (m/sec² or ft/sec²)

Finally, the following parameters (which are used for this example case) are printed after liftoff when sink calculations are made.

ASINK - Sink acceleration (m/sec² or ft/sec²) (sink calculations cease when this value becomes zero)

VSINK - Sink velocity (m/sec or ft/sec)
DSINK - Sink distance (m or ft)

The time history printout concludes on the following page of output. After liftoff the appropriate sink parameters are shown. After the time history the final liftoff parameters are presented. These parameters include maximum sink height and time, distance, and airspeed at that sink height condition. Other characteristics at this condition include lift, drag, horizontal acceleration, gross thrust, and vertical gross thrust.

Since the IPRINT was switched off for the two additional cases no time history is printed. These cases were done with dynamic rate of climb calculations so instead of sink parameters the prescribed rate of climb along with the vertical height when this rate of climb is achieved is printed.

After all the cases are determined an extrapolation is made to estimate the pitchup airspeed and horizontal acceleration for a deck run of 400 feet.

[illegible]

81/09/28. 14.54.07.

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000 1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 104

LOAD MAP - STO

CYHER LOADER 1.4-485

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PAGE 1

FMA OF THE LOAD 111
LMA+1 OF THE LOAD 32715

TRANSFER ADDRESS -- STO 6206

PROGRAM ENTRY POINTS -- STO 6206

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR	VER	LEVEL	HARDWARE	COMMENTS
/PRINT/	111	1							
STO	112	11662	LGO	78/01/0	FTN	3.0	P380	6666	
/TSIZE/	11774	5671							
TAKES	17465	1353	UL-VTL1R2	77/03/0	FTN	3.0	P380	6666	
SPLN01	21240	504	UL-VTL1R2	77/10/1	FTN	3.0	P380	6666	
UPDATE	21744	135	UL-VTL1R2	75/07/1	FTN	3.0	P380	6666	
ATMOS	22101	213	UL-VTL1R2	76/10/2	FTN	3.0	P380	6666	
SNEST	22314	110	UL-VTL1R2	75/06/1	FTN	3.0	P380	6666	
SYSTEMS	22424	1035	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
ACCOERS	23461	13	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
RACKSPS	23474	334	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
IFENDPS	24030	57	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
INPUTCS	24107	131	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
INPUTNS	24240	1171	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
OUTPUTCS	25431	74	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
REWINNS	25525	52	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
EXPE	25577	44	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
SINCOSE	25643	55	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
SORTE	25720	22	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
XTOYE	25742	7	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
KODERS	25751	1422	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
KRAKERS	27373	1525	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
ALNLOGE	31120	37	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
GETBA	31157	17	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		
STOB	31174	1517	SL-FTN3L1B	R0/09/02	COMPASS	3.6	485		

.106 CP SECONDS

447008 CM STORAGE USED

11 TABLE MOVES

SDATA ALPHA=-5.5430.PH12=5.PH12AR=54.PH12PR=15.ALPHAR=5.9.ALPHAR=13.
 ALPHAR=5.9.ALPHAR=13.F1=1.FLDTFMR=90.PH1=45.01STAY=75J.PH11AR=75.
 PH11PR=15.NS=AA.PS=AA.PSF=AA.W=40000.10PRINT=1.MSINT=1.RUN=400.
 SINAD=200.PRINT=1.

1- EXAMPLE CL VS. ALPHA TABLE

VEL = .0										
PHI2 = .0	CLTE = .0									
	ALPH = -.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02		
	CL = -.48000E+00	-.17500E+00	.17500E+00	.45000E+00	.78000E+00	.10400E+01	.13750E+01	.14900E+01		
VEL = .0										
PHI2 = .50000E+02	CLTE = .0									
	ALPH = -.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02		
	CL = -.13000E+00	.15000E+00	.42000E+00	.69000E+00	.96000E+00	.12000E+01	.14500E+01	.15700E+01		
VEL = .0										
PHI2 = .90000E+02	CLTE = .0									
	ALPH = -.80000E+01	-.40000E+01	.0	.40000E+01	.80000E+01	.12000E+02	.16000E+02	.20000E+02		
	CL = .34000E+00	.59000E+00	.86000E+00	.11100E+01	.13400E+01	.14700E+01	.15600E+01	.15500E+01		

13 EXAMPLE DRAG POLARS (POWER OFF) TABLE

QUMM=	.0	CLTE=	.0						
PHI2=	.0	CL	-.0000E+00	.0	.40000E+00	.80000E+00	.12000E+01	.14000E+01	
		CD	.41540E-01	.29380E-01	.37420E-01	.65330E-01	.17463E+00	.22405E+00	

10 EXAMPLE ENGINE THRUST TABLE

DUMM=	.0	SET =	.10000E+01						
TIME=	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00		
		FG	.11755E+05	.14044E+05	.14312E+05	.14875E+05	.15417E+05		
DUMM=	.0	SET =	.20000E+01						
TIME=	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00		
		FG	.29477E+05	.29944E+05	.30531E+05	.31606E+05	.32673E+05		
DUMM=	.0	SET =	.30000E+01						
TIME=	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00		
		FG	.10994E+05	.11330E+05	.11665E+05	.12342E+05	.13018E+05		
DUMM=	.0	SET =	.40000E+01						
TIME=	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00		
		FG	.23774E+05	.24346E+05	.24958E+05	.26161E+05	.27363E+05		

33 EXAMPLE RAM DMAP TABLE

DUMM#	.0	SET #	.10000E+01				
TIME#	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00
		RAMD	.0	.39460E+04	.81230E+04	.12240E+05	.16621E+05
DUMM#	.0	SET #	.70000E+01				
TIME#	.0	MACH	.0	.50000E-01	.10000E+00	.15000E+00	.20000E+00
		RAMD	.0	.38620E+04	.79310E+04	.12023E+05	.16486E+05

15 EXAMPLE INDUCED AERODYNAMICS TABLE

DUMM=	.0	SET =	.10000E+01		
Y =	.0	PHI2	.0	.50000E+02	.10000E+03
		CEL	.20000E-01	.12000E+00	.21400E+00
DUMM=	.0	SET =	.20000E+01		
Y =	.0	PHI2	.20300E+02	.44500E+02	.84700E+02
		CEL	-.58000E-01	-.31000E-01	.42000E-01

TABLE DATA INPUT SUMMARY 5 TABLES

TABLE NUMBER	REFERENCE NUMBER	ARRAY LOCATION
1	10.	217.
2	13.	178.
3	14.	61.
4	15.	373.
5	33.	316.

DATA STORAGE ALLOCATION 3000
DATA STORAGE NOT USED 2582

-.3466E-01	.24430E-01	11111	.05141E+00	.22429E-02	.0
.40000E+05	.94195E+02	.31384E+04	.41654E+04	11111	.66297E+04
.20000E+02	-.17550E+01	.30000E+01	.15125E+03	.15293E+05	.60000E+02
.10142E+00	.29017E-01	11111	.79463E+00	.22429E-02	.0
.40000E+05	.10139E+03	.41754E+04	.57722E+04	11111	.70759E+04
.23750E+02	-.28000E+00	.32500E+01	.17589E+03	.10990E+05	.63750E+02
.23244E+00	.32481E-01	11111	.77046E+00	.22429E-02	.0
.40000E+05	.10404E+03	.53114E+04	.53659E+04	11111	.74430E+04
.27500E+02	.11450E+01	.35000E+01	.20199E+03	.67826E+04	.67500E+02
.35522E+00	.36059E-01	11111	.65930E+00	.22429E-02	.0
SINK DATA	.54556E+01	.13639E+00	.34097E-02		
.40000E+05	.11111E+03	.65542E+04	.59320E+04	11111	.78481E+04
.31250E+02	.26700E+01	.37500E+01	.22939E+03	.26876E+04	.71250E+02
.47494E+00	.38411E-01	11111	.58321E+00	.22429E-02	.0
SINK DATA	.21614E+01	.10577E+01	.17277E+00		

VEHICLE IS AIRBORNE
 MAXIMUM SINK DISTANCE IS .41562E+00 FT.
 DISTANCE = .25216E+03 FT.
 VELOCITY = .11553E+01 FT./SEC.
 TIME = .40000E+01 SEC.
 END WEIGHT FOR THIS PHASE IS .40400E+05 POUNDS MASS

LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION = .51570E+00 G'S
 LIFT = .76359E+04 POUNDS FORCE
 DRAG = .63560E+04 POUNDS FORCE
 VERTICAL GROSS THRUST = .32863E+05 POUNDS FORCE
 HORIZONTAL GROSS THRUST = .26984E+05 POUNDS FORCE

NEXT NEXT

SOATA SINKD=0.ROC=1.67.PS=90.RS=76.RSF=74.IPRINT=04
 TORG = .40000E+05

INITIAL GROUND RUN PARAMETERS

VEHICLE IS AIRBORNE
 VEHICLE HAS A R/C OF .16700E+01 FT./SEC.
 VERTICAL HEIGHT IS .36921E+00 FT.
 DISTANCE = .35474E+01 FT.
 VELOCITY = .13093E+01 FT./SEC.
 TIME = .40000E+01 SEC.
 END WEIGHT FOR THIS PHASE IS .40000E+05 POUNDS MASS

LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION = .36309E+00 G'S
 LIFT = .11300E+05 POUNDS FORCE
 DRAG = .81452E+04 POUNDS FORCE
 VERTICAL GROSS THRUST = .37272E+05 POUNDS FORCE
 HORIZONTAL GROSS THRUST = .22634E+05 POUNDS FORCE

NEXT NEXT

SOATA SINKD=0.ROC=1.67.PS=100.RS=84.RSF=84.IPRINT=05
 TORG = .40300E+05

INITIAL GROUND RUN PARAMETERS

VEHICLE IS AIRBORNE
 VEHICLE HAS A R/C OF .10700E+01 FT./SEC.
 VERTICAL HEIGHT IS .77650E+00 FT.
 DISTANCE = .77324E+01 FT.
 VELOCITY = .13344E+01 FT./SEC.
 TIME = .00500E+01 SEC.
 END WEIGHT FOR THIS PHASE IS .40000E+05 POUNDS MASS

LIFTOFF CHARACTERISTICS

HORIZONTAL ACCELERATION = .36907E+00 G'S
 LIFT = .11639E+05 POUNDS FORCE
 DRAG = .86602E+04 POUNDS FORCE
 VERTICAL GROSS THRUST = .36441E+05 POUNDS FORCE
 HORIZONTAL GROSS THRUST = .23473E+05 POUNDS FORCE

NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT NEXT

BY CUBIC SPLINE INTERPOLATION OF THE ABOVE DATA POINTS
 FOR A RUN OF .40000E+03 FEET THE PS IS .10320E+03 FT./SEC.
 AND THE HORIZONTAL ACCELERATION IS .37630E+00 G'S

TESTAVI. 01/04/20, 000005 2.1.1-SYS-C25-NADC.

```
.51-TEST-CH50000-110.
.51-ACCOUNT-00334A..
.51-MASTER DEVICE: A
.52-GET-VTL1M1-VTL1M2/IN=V11499.
.57-GET-VTL1M1-LGN...SINEL/STO
.00-EDITING COMPLETE.
.00-LOSETILIN=VTL1R2)
.00-LGO.
.00-STOP
.04-COMPUTER UNITS AT.100 P = 1.
.04-CP      1.680 SEC.      $    0.28
.04-CN      14.323 NAD.      $    0.09
.04-IO      1.895 SEC.      $    0.09
.04-JM      19.878 NAD.
.04-TAPES SCHEDULED 00
.04-PACKS SCHEDULED 00
.04-SERVICE CHARGE          $    2.20
.04-
.04-SUBTOTAL          $    3.17
```

NADC-81259-60

APPENDIX C

Program Listings

A listing of the FORTRAN source code for the main STO program and a four degree-of-freedom interpolating subroutine TAKE5 is presented.

[illegible]

FTV 4.0442E

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9C

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11v

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PROGPA= STD          74/74   JPT=1          FTY 4.6+423      91/07/26. 10.18.43      PAGE      3

115      FN1=(FN1-FLOSSP*FN1)*NEF          STD 0115
      FN2=(FN2-FLOSSA*FN2)*NEA          STD 0116
C ***** INDUCED AERC          STD 0117
      FGTJAL=FN1+FN2          STD 0118
      CALL TLJDS(15,PHI2,1,,J,,J,DLFG)          STD 0119
      CALL TLJDS(15,PHI2,2,,J,,J,DDFG)          STD 0120
      DLFG=DLFG+FGTJAL $ DDG=DDG+FGTJAL          STD 0121
C #####          STD 0122
      PH2I=PHI2          STD 0123
      VSTAR1=V $ IF(V.LT.VSTAR) VSTAR1=VSTAR          STD 0124
      CALL TLJDS(14,ALPHA,DELTA,PH2I,VSTAR1,CL)          STD 0125
      CALL TLJDS(13,CL,DELTA,PH2I,VSTAR1,CD)          STD 0126
      IF(SEGMENT.NE.J) CALL TLJDS(17,CL,DELTA,PH2I,VSTAR1,CM)          STD 0127
      PH12=(PHI2+ANGF*CL)*3.141592654/180.          STD 0128
      D=+.5*CD*V**2*W3*5          STD 0129
      CALL TLJDS(33,MACH,2,,J,,J,EDRAG)          STD 0130
      CALL TLJDS(33,MACH,2,,J,,J,DSTJRE)          STD 0131
      EDRAG=EDRAG*DDSCALE          STD 0132
      IF(EDRAG.EQ.J) EDRAG=0          STD 0133
      IF(DSTJRE.EQ.J) DSTJRE=0          STD 0134
      IF(DSTJRE.NE.J) AND(NCJSEI.NE.J) CALL TLJDS(33,MACH,3,,J,,J,DCEILOF)          STD 0135
      DR=DR+EDRAG*DSTJRE+DCEILOF*DDFG          STD 0136
      PITC=(ALPHA-ALP*AD)*3.141592654/180.          STD 0137
      ANG1=PH11+PITC+EDATJ $ ANG2=PH12+PITC+EDATUM          STD 0138
      L=+.5*CL*V**2*W3*5          STD 0139
      L=L+DLFG          STD 0140
      FGV=FN1*SIN(ANG1)+FN2*SIN(ANG2)          STD 0141
      FGH=FN1*COS(ANG1)+FN2*COS(ANG2)          STD 0142
      BALANCE=L-FGV          STD 0143
      J=DT*G $ (F3H-JR-NJ*BALANCE)/W          STD 0144
      V2=V+DV          STD 0145
      IF(SEGMENT.EQ.J) GO TO 220          STD 0146
      MOMENT=+.5*CH*V**2*W3*5*MAC          STD 0147
      RF=(LEVER*BALANCE-MOMENT)/CLEVER          STD 0148
      IF(PITCH.LE.J) GO TO 220          STD 0149
      ANG1ESS=LRA*COS(PITCH)+NU*LRA*SIN(PITCH)+LR*NJ*COS(PITCH)-LR*SIN(PITCH)          STD 0150
      RF=(BALANCE*ANG1ESS-MOMENT)/(LRF+ANG1ESS*COS(PITCH))          STD 0151
      JZ=0+.5*DT*(V2-JZ)**2-(V-JZ)**2)/DV          STD 0152
      IF(PRINT.EQ.J) JR(J.NE.J) GO TO 250          STD 0153
      ACCX=(FGH-DR-NJ*BALANCE)/W          STD 0154
      PRINT 230,,V,L,JR,RF,EDRAG,FN2          STD 0155
      PRINT 230,PH2I,ALPHA,T,JZ,BALANCE,PH11,FN1          STD 0156
      PRINT 240,CL,CD,CM,ACCX, $ A3,DELTA          STD 0157
      FORMAT(5X,7(E12.5))          STD 0158
      FORMAT(5X,6(E12.5),/,$10(1MT))          STD 0159
      IF(SEGMENT.EQ.J) GO TO 260          STD 0160
      IF(RF.LE.J) GO TO 520          STD 0161
      IF(BALANCE.GT.J) JR(DELTA.EQ.J) GO TO 230          STD 0162
      J=1. $ J=J-1          STD 0163
      DELTAB=0.          STD 0164
      RUSCALE=RAM          STD 0165
      IF(RAM.EQ.1.) Q1=J.          STD 0166
      IF(RAM.EQ.1.) J2=+.          STD 0167
      IF(P4JNY.EQ.J) GO TO 180          STD 0168
      PH11=PH11AR $ PH21=PH21AR $ ALP4A=ALP4AAR          STD 0169
      PRINT 270          STD 0170

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PROGRAM STD	74/74 JPT=1	FTN 4,5+426	31/39/26. 10.18.43	PAGE 4
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175	270 F0RMA1(10X,0INSTANTANEOUS ROTATION AT DEI*)	STD 0172
	P40NY=-.13 & GJ TO 180	STD 0173
	280 IF(BALANCE.GT.0..JR.EFALLA.E3.0..JR.JEI.NE.0.) GJ TO 290	STD 0174
	JEI=1. & NEA=NEA+.5 & NEF=NEF.0. ILJSE & GJ TO 180	STD 0175
	290 D=32 & V=V2 & T=T+DT & W=-(W1+W2)*DT/3600.)	STD 0176
	IF(P4JNT.E3=-.13) GJ TO 350	STD 0177
	IF(CJLT.DISTMAX) GJ TO 310	STD 0178
	PRINT 300	STD 0179
180	300 F0RMA1(10X,0CASE TERMINATED (DISTMAX EXCEEDED)*)	STD 0180
	GJ TO 730	STD 0181
	310 IF(ICJUNT.GT.1000) GJ TO 410	STD 0182
	IF(BALANCE.GE.0..JR.RJC.E3.0.) GJ TO 330	STD 0183
185	WU=.5 AGYL=AGY & DRJCL=DRJC	STD 0184
	AGY=(-BALANCE)*G/4	STD 0185
	AGYA=(AGY+AGYL)*.5	STD 0186
	DRJCL=DRJCL+AGYA*DT	STD 0187
	ARJC=(DRJC+DRJCL)*.5	STD 0188
	RJC4=ARJC+ARJC*DT	STD 0189
190	IF(1PRINT.NE.0.AND.J.E3.1) PRINT 320,DRJC,AGYA	STD 0190
	320 F0RMA1(1X,0CLIN3 DATA,Z(10X,E20.5))	STD 0191
	IF(DRJC.GE.RJC) GJ TO 430	STD 0192
	GJ TO 350	STD 0193
	330 IF(SINK.GT.0..AND.SINK.LE.0) GJ TO 900	STD 0194
195	340 IF(BALANCE.LE.0.) GJ TO 430	STD 0195
	350 ICJUNT=ICJUNT+1	STD 0196
	GJ TO 180	STD 0197
	360 IF(METRIC.NE.0) GJ TO 380	STD 0198
	PRINT 370,D,V,T,4	STD 0199
200	370 F0RMA1(10X,0DISTANCE = *,E20.5,* FT.,/,10X,0VELOCITY = *,E20.5,*	STD 0200
	(FT./SEC.,/,10X,0TIME = *,5X,E20.5,* SEC.,/,10X,0END WEIGHT FOR T4STD	STD 0201
	(IS PHASE IS *,E20.5,* POUNDS PASS*)	STD 0202
	GJ TO 400	STD 0203
	380 PRINT 390,D,V,T,4	STD 0204
205	390 F0RMA1(10X,0DISTANCE = *,E20.5,* 1.,/,10X,0VELOCITY = *,E20.5,*	STD 0205
	(1./SEC.,/,10X,0TIME = *,5X,E20.5,* SEC.,/,10X,0END WEIGHT FOR T4STD	STD 0206
	(IS PHASE IS *,E20.5,* KILGRAMS *)	STD 0207
	400 IF(SEGMENT.E3.0) GJ TO 630	STD 0208
	GJ TO (500,610), SEGMENT	STD 0209
210	410 PRINT 420	STD 0210
	420 F0RMA1(10X,0TJ3 4UCH TIME*)	STD 0211
	GJ TO 360	STD 0212
	430 PRINT 440	STD 0213
	440 F0RMA1(10X,0VEHICLE IS AIRBORNE*)	STD 0214
215	ISINK=104 FT.	STD 0215
	IF(METRIC.NE.0) ISINK=104 1.	STD 0216
	IF(SINK.GT.0.) PRINT 450,ISINK,ISINK	STD 0217
	450 F0RMA1(10X,0MAXIMUM SINK DISTANCE IS*,E20.5,A10)	STD 0218
	IF(JEI.NE.0..JR.JJ.NE.0.) PRINT 460	STD 0219
220	460 F0RMA1 (10X,0DEI AT PSEUDO LIFTOFF*)	STD 0220
	IF(RJC.E3.0.) GJ TO 490	STD 0221
	IRJC=104 FT./SEC.	STD 0222
	IF(METRIC.NE.0) IRJC=104 1./SEC.	STD 0223
	PRINT 470,RJC,IRJC	STD 0224
225	470 F0RMA1(10X,0VEHICLE HAS A R/C OF *,E20.5,A10)	STD 0225
	IRJC=104 FT.	STD 0226
	IF(METRIC.NE.0) IRJC=104 1.	STD 0227
	PRINT 480,RJC,IRJC	STD 0228

74/74

122-1

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PAGE

3

STO	J229
STO	J230
STO	J231
STO	J232
STJ	J233
STO	J234
STJ	J235
STJ	J236
STJ	J237
STJ	J238
STJ	J239
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STJ	J242
STO	J243
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STO	J256
STJ	J257
STO	J258
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STO	J261
STO	J262
STJ	J263
STO	J264
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STO	J283
STO	J284
STO	J285

PROGRAM STL 74/74 JPT-1

FTN 4,0420

51/07/25. 10.18.43

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      IF(METRIC.EQ.0) GO TO 550
      I400=104 1/SEC
      PH40=P400/60.
240  650 PRINT 600,PH40,I400
      660 FJ44AT(104,INSTANTANEOUS R/C IS *E20.5,A10)
      670 IF(METRIC.NE.0) GO TO 580
      PRINT 680,AG4,L,DR,F40,F44
290  680 FJ44AT(104,HORIZONTAL ACCELERATION **E20.5* G(S**10X,
      **LIFT **19X,E20.5* POUNDS FORCE**10X,*DRAG **19X,E20.5,
      ** POUNDS FORCE**10X,*VERTICAL GROSS THRUST **2X,E20.5,
      ** POUNDS FORCE**10X,*HORIZONTAL GROSS THRUST **E20.5,
      ** POUNDS FORCE*)
      GO TO 710
300  690 PRINT 700,AG4,L,DR,F40,F44
      700 FJ44AT(104,HORIZONTAL ACCELERATION **E20.5* G(S**10X,
      **LIFT **19X,E20.5* NEUTONS **10X,*DRAG **19X,E20.5,
      ** NEUTONS **10X,*VERTICAL GROSS THRUST **2X,E20.5,
      ** NEUTONS **10X,*HORIZONTAL GROSS THRUST **E20.5,
      ** NEUTONS *)
305  710 IF(RJN.LE.0.) GO TO 730
      CALL UPDATE(AGDATA,D,AG4)
      IF(P40MY.EQ.-.13) CALL UPDATE(PHDATA,D,PH40)
      IF(PSINT.LE.0.) GO TO 720
      CALL UPDATE(RUNDATA,D,PS)
310  720 CALL UPDATE(RUNDATA,D,T300)
      730 PRINT 740
      740 FJ44AT(1,1X,22(64 NEXT ),/)
      GO TO 10
315  750 IF(RJN.LE.0.) STOP
      IF(P40DATA(1).EQ.0.) GO TO 770
      PH40=SPLNGL(1,P40DATA,RJN)
      PRINT 760,PH40,I400
320  760 FJ44AT(104,INSTANTANEOUS INTERPOLATED R/C IS *E20.5,A10)
      770 AG=SPLNGL(1,AGDATA,RJN)
      RUN=SPLNGL(1,RJNDATA,RJN)
      K(1)=64 FEET * K(2)=64 T300 * K(3)=104 POUNDS MA * K(4)=2HSS
      IF(METRIC.EQ.0.AND.PSINT.EQ.0.) GO TO 780
      K(1)=64 MA * K(3)=104 KILGRAMS * K(4)=2H
      IF(PSINT.EQ.0.) GO TO 780
325  K(2)=64 PS * K(3)=104 1/SEC.
      IF(METRIC.NE.0) GO TO 780
      K(1)=64 FEET * K(3)=104 FT./SEC.
      780 PRINT 790,RUN,K(1),K(2),RJN,K(3),K(4),AG
330  790 FJ44AT(104,334 CUBIC SPLINE INTERPOLATION OF THE ABOVE DATA POINTS
      **1/25X**FOR A RUN OF *E20.5*AB,THE *AG*IS*,E20.5,A10*,A3,*,60X*STO
      **AND THE HORIZONTAL ACCELERATION IS *E20.5* G(S*)
      STOP
      C????????????????? SINK OFF THE 334 CALCULATIONS
      800 IF(RJN.EQ.0) GO TO 810
335  IF(PS.GT.0.) PS=V * IF(RS.GT.0.) RS=V * IF(RSF.GT.0.) RSF=V * V=JSTO
      810 ASINKL=ASINK * VSINKL=VSINK * OSINKL=OSINK
      ASINK=ABALANCE*0.4
      ASINKA=(ASINK+ASINKL)*.5
      VSINK=VSINKL+ASINKA*0.5
      VSINKA=(VSINK+VSINKL)*.5
      JSINK=OSINKL+VSINKA*0.5
340  IF(IPRINT.NE.0.AND.J.EQ.1) PRINT 920,ASINK,VSINK,OSINK

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      STD 0280
      STD 0287
      STD 0288
      STD 0289
      STD 0290
      STD 0291
      STD 0292
      STD 0293
      STD 0294
      STD 0295
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      STD 0297
      STD 0298
      STD 0299
      STD 0300
      STD 0301
      STD 0302
      STD 0303
      STD 0304
      STD 0305
      STD 0306
      STD 0307
      STD 0308
      STD 0309
      STD 0310
      STD 0311
      STD 0312
      STD 0313
      STD 0314
      STD 0315
      STD 0316
      STD 0317
      STD 0318
      STD 0319
      STD 0320
      STD 0321
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      STD 0323
      STD 0324
      STD 0325
      STD 0326
      STD 0327
      STD 0328
      STD 0329
      STD 0330
      STD 0331
      STD 0332
      STD 0333
      STD 0334
      STD 0335
      STD 0336
      STD 0337
      STD 0338
      STD 0339
      STD 0340
      STD 0341
      STD 0342

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PR35249 STD 74/74 JPT=1

FTN 4.6*425

31/09/20. 20.19.43

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820 FORMATE(11,0SING DATA,31104,E20.511) STD 0343
63 TD 340 STD 0344
343 [..... STD 0345
END STD 0346

RTD 4.5042.

61/00/25. 25.13.43

Page 1

TAK50001
TAK50002
TAK50003
TAK50004
TAK50005
TAK50006
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TAK50056
TAK50057

SUBROUTINE TAMEX 76/76 JPT=1

FTN 4,50020

31/03/76, 10.16.43

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      K2=L
      IF(TDATA(K1).LT.TDATA(K2)) GO TO 130
      XSAVE=TDATA(K1)
      TDATA(K1)=TDATA(K2)
      TDATA(K2)=XSAVE
      XSAVE=TDATA(K1+33)
      TDATA(K1+30)=TDATA(K2+33)
      TDATA(K2+30)=XSAVE
      XSAVE=L
130  CONTINUE
      IF(NJONE.EQ.0) GO TO 120
140  IF(II.LE.0) GO TO 473
      IF(NPRINT.EQ.0) GO TO 150
      PRINT 150
150  FORMAT(11)
160  PRINT 170,NTBL
170  FORMAT ( 35X,24MTABLE DATA IN-JT SUMMARY,11I2,1X,54TABLES,/,25
75  1X,44TABLE NUMBER REFERENCE NUMBER ARRAY LOCATION )
      PRINT 180,((N,TDATA(N),TDATA(N+30)),N=1,NTBL)
180  FORMAT (32X,I2,12X,F5.3,15X,F5.0)
      PRINT 190, NMAX,NREX
190  FORMAT (/,35X,24M DATA STORAGE ALLOCATION ,14,/,35X,24M DATA STORAGE
80  1 NOT USED ,14,/)
      IF(MRIGEL.GT.0) PRINT 200,((SIRIJS(I2),I2=1,MRIGEL)
200  FORMAT(10X,*,THE FOLLOWING TABLES HAVE BEEN REPLACED*,5(1X,F10.3),*,
      210  Z=,/,8(1X,F10.3),*,/)
      PRINT 1111,((N,TDATA(N)),N=1,LOC)
85  C1111 FORMAT(5(1X,I4,1X,E12.5))
      RETURN
210  IP=1
      IF(NPRINT.EQ.0) IP=0
      PRINT 30, IP,ITAINQ
90  IF(NPRINT.NE.0) PRINT 220
220  FORMAT(////////)
      ICC = 0
      L=LIC
      IO=44
95  DO 230 ICL=1,5
230  ICL=ICL+4H
240  ICL=IO
      READ 250,IO,N,(A(I),I=1,N)
100 250  FORMAT(A4,I3,3A,(7I1,7F10.3))
      IF(IJ.EQ.4HEOT) GO TO 20
      ICC=ICC+1
      IF(ICC.LE.5) IO=ICC+10
      IF(IJ.EQ.IDL) GO TO 35
      IF(IJ.NE.IDO(3)) GO TO 150
105  IF(IJL.E3.IDO(3)) GO TO 350
      LJC=LE
      L=LX
      GO TO 290
110 260  TDATA(LOC)=N
      L=LJC
      IF(IJ.EQ.IDO(2)) GO TO 330
270  IF(IJ.EQ.IDO(4)) LX=L
      IF(IJ.NE.IDO(3)) GO TO 330
      L=L
      TAK50058
      TAK50059
      TAK50060
      TAK50061
      TAK50062
      TAK50063
      TAK50064
      TAK50065
      TAK50066
      TAK50067
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      TAK50110
      TAK50111
      TAK50112
      TAK50113
      TAK50114

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SUBROUTINE TAKES 74/74 JPT=1

FTN 4.0+428

31/09/28. 10.19.43

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110      LZ=LZ+1
      GO TO 330
290    IF(IP.EQ.0) GO TO 330
      LY=LY+1
      IF(NPRINT.NE.0) PRINT 290,IDD(1),TDATA(LY)
120    290 FJRMAT(IX,AY,14,E13.5)
      IF(NPRINT.NE.0) PRINT 300,IDD(2),TDATA(LY),IDD(3),TDATA(LY)
      300 FJRMAT(IX,AY,14,E13.5,IX,AY,14,E13.5)
      JF=0
      NN=
125    LF=LK
      NP=
      IF(N.GT.8)NP=
      LE=LF+NP
130    LF=LF+1
      IF(NPRINT.NE.0) PRINT 320,IDD(4),TDATA(I),I=LF,LE)
      320 FJRMAT(2IX,AY,14,E13.5)
      LF=LE
      JE=JF+NP
      JF=JF+1
135    IF(NPRINT.NE.0) PRINT 320,IDD(5),A(I),I=JF,JE)
      JF=JE
      IF(N.GT.0) GO TO 310
      330 DO 340 I=1,N
      LJC=LJC+1
140    TDATA(LJC)=A(I)
      LE=LJC
      IF(IJ.EQ.IDD(5)) TDATA(LJC+2)=1.
      LJC=LJC+3
145    IF(LJC.GT.NMAX)370,240
      350 TDATA(LJC)=TDATA(LX)
      L=LJC
      DO 360 I=1,N
      LJC=LJC+1
150    TDATA(LJC)=TDATA(LX+I)
      GO TO 280
      370 PRINT 380, ITABNJ
      380 FJRMAT (IX,32H*****TABLE OVER FL3H ,TABLE ,IS,11H NOT LOADED)
      GO TO 40
155    LZ=LJC 5 LW=LW+1 5 GO TO 270
      ENTRY TLJDS
      *****
      IF(II.LE.0) RETURN
      000 SEARCH FOR CORRECT TABLE
      NL=NTBL+1
      NL=1
      K=LAST
      XTAB=II
      KT=J
160    400 KT=KT+1
      IF(KT.GT.0) GO TO 470
      IF((XTAB-TDATA(K)).EQ.0.) GO TO 430
      IF((XTAB-TDATA(K)).LT.0.) GO TO 410
      NL
      GO TO 420
170    410 NL=K
      470

```

TAK50115
TAK50116
TAK50117
TAK50118
TAK50119
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TAK50170
TAK50171

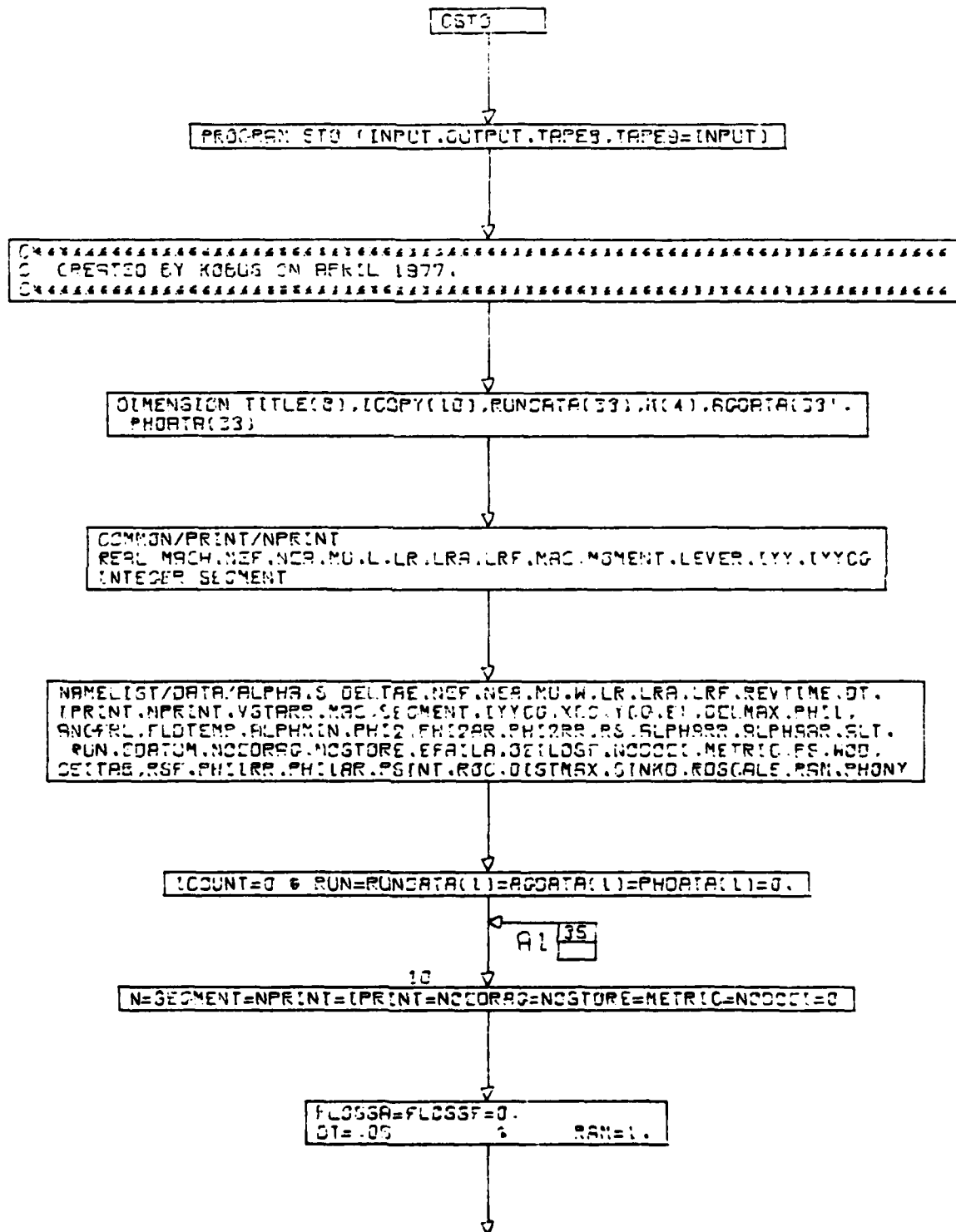
SUBROUTINE TAKES	74/74	3PT=1	FTN 4.50428	01/09/28. 10.10.43	PAGE 4
426	K=(M4-NL)/2+NL			TAK50172	
	GO TO 403			TAK50173	
430	1LAST=K			TAK50174	
175	IZ=TDATA(M+30)			TAK50175	
	INZ=TDATA(IZ)			TAK50176	
	IV=3*INZ+IZ+3			TAK50177	
	IX=IV			TAK50178	
	IZ1=IZ+INZ+1			TAK50179	
180	IZ2=IZ+2*INZ			TAK50180	
	DO 450 IZ5=IZ1,IZ2			TAK50181	
	INV=TDATA(IV)			TAK50182	
	IX=3*INV+IX+3			TAK50183	
	IX=IX			TAK50184	
185	IV1=IV+INV+1			TAK50185	
	IV2=IV+2*INV			TAK50186	
	DO 450 IV5=IV1,IV2			TAK50187	
	IX=TDATA(IX)			TAK50188	
	IX=3*IX+IX+3			TAK50189	
190	IX1=IX+IX+1			TAK50190	
	IX2=IX+2*IX			TAK50191	
	DO 440 IX5=IX1,IX2			TAK50192	
	TDATA(IX5)=SPLN01(IX,TDATA,M)			TAK50193	
440	IX=IX+3*TDATA(IX)+3			TAK50194	
195	TDATA(IV5)=SPLN01(IX,TDATA,M)			TAK50195	
450	IX=IX			TAK50196	
	TDATA(IZ5)=SPLN01(IV,TDATA,M)			TAK50197	
460	IV=IV			TAK50198	
	IX=IX			TAK50199	
200	470 RETURN			TAK50200	
	END			TAK50201	

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APPENDIX D

Program Logic

Flow charts for the main STO program and the subroutine TAKE5 are presented.



REVTIME=ANGFRL=ALPHMIN=EDRSG=OSTORE=V=T=ALT=DEL=WF1=PHI1=PHI2=
FN1=FN2=OLFG=DDFG=VGSTARR=EDATUM=EFALLA=DET=OS*LOGI=0.

OS*LOF=RSF=PHI1AR=PHI1RR=PSINT=AGY=DRDC=ROC=WD=ROCH=PHONY=0.
WF2=RS=DELTA=PHI2AR=PHI2RR=ALPHARR=ALPHARR=RUN=PG=OS*ITAB=QQ=0.
FLOTEMP=59. \$ MU=.02 \$ NCP=NCF=1. \$ Q1=1. \$ Q2=2. \$ DISTMAX=1.26
SINKO=ASINK=VSINK=OSINK=0. \$ ROSCALE=1.

IF(ICOUNT.NE.0)

GO TO 99

IC=1

READ 30,ICOPY

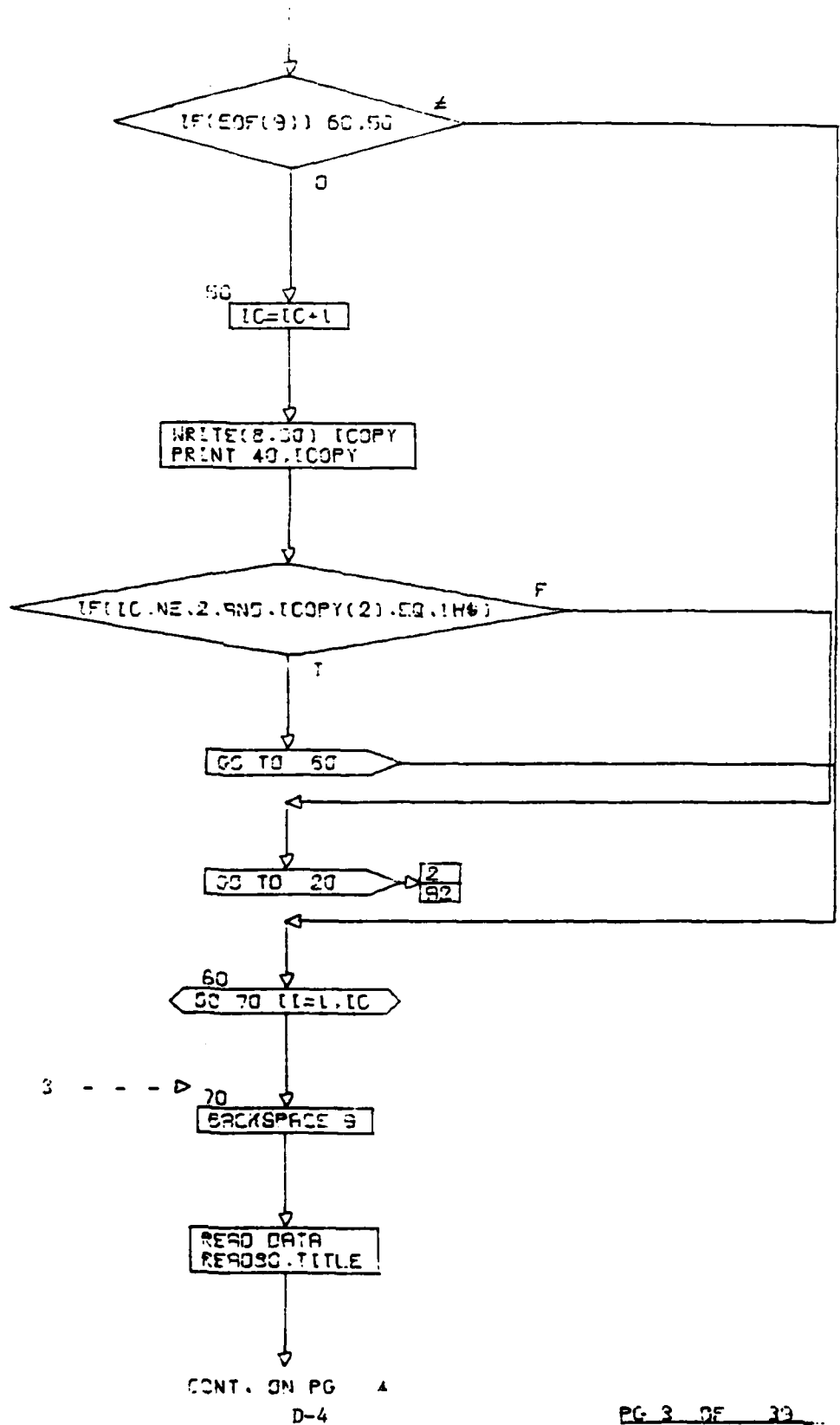
FORMAT(29I,.69.7B:C)

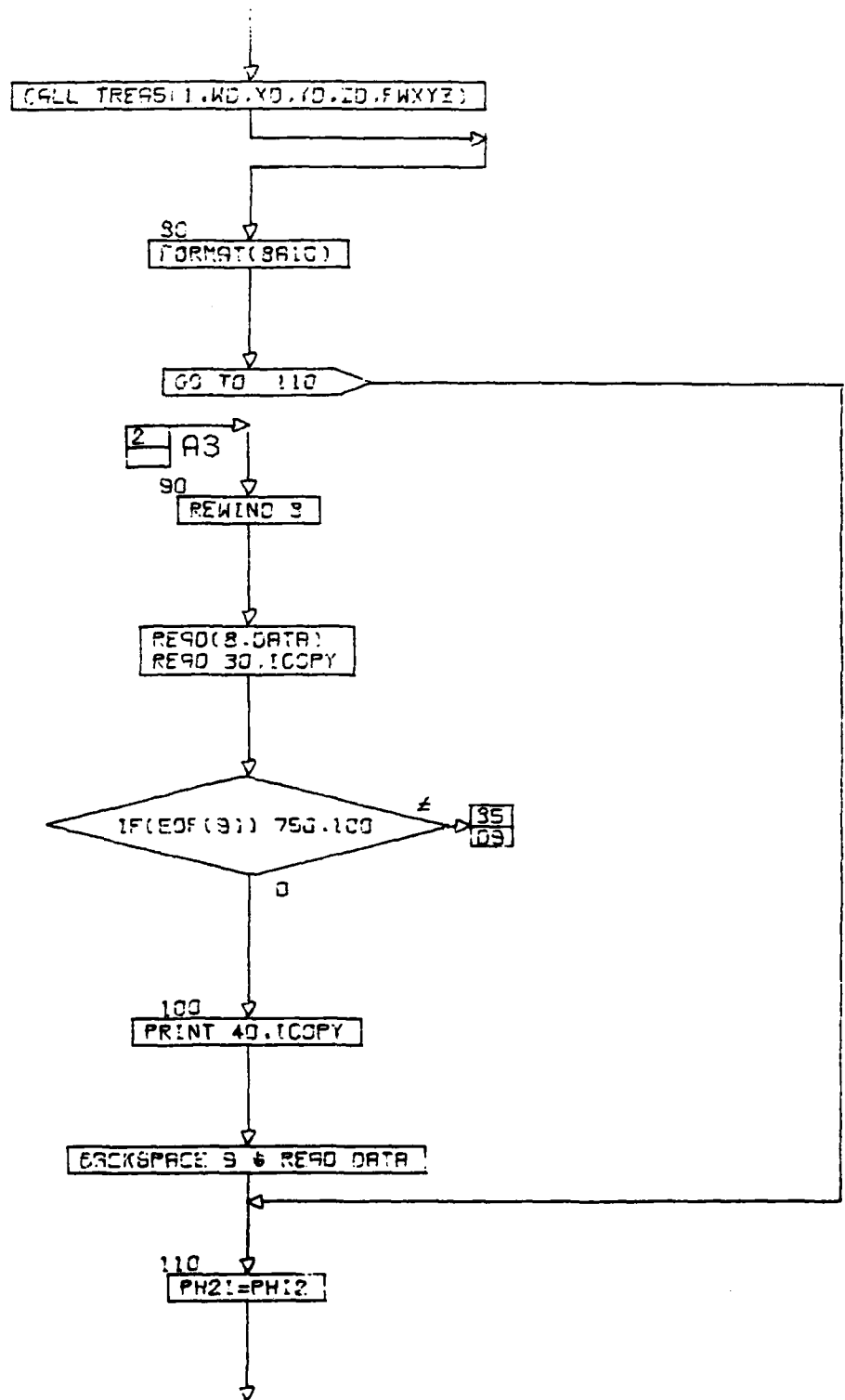
FORMAT(1X.29I,.69.7B:C)

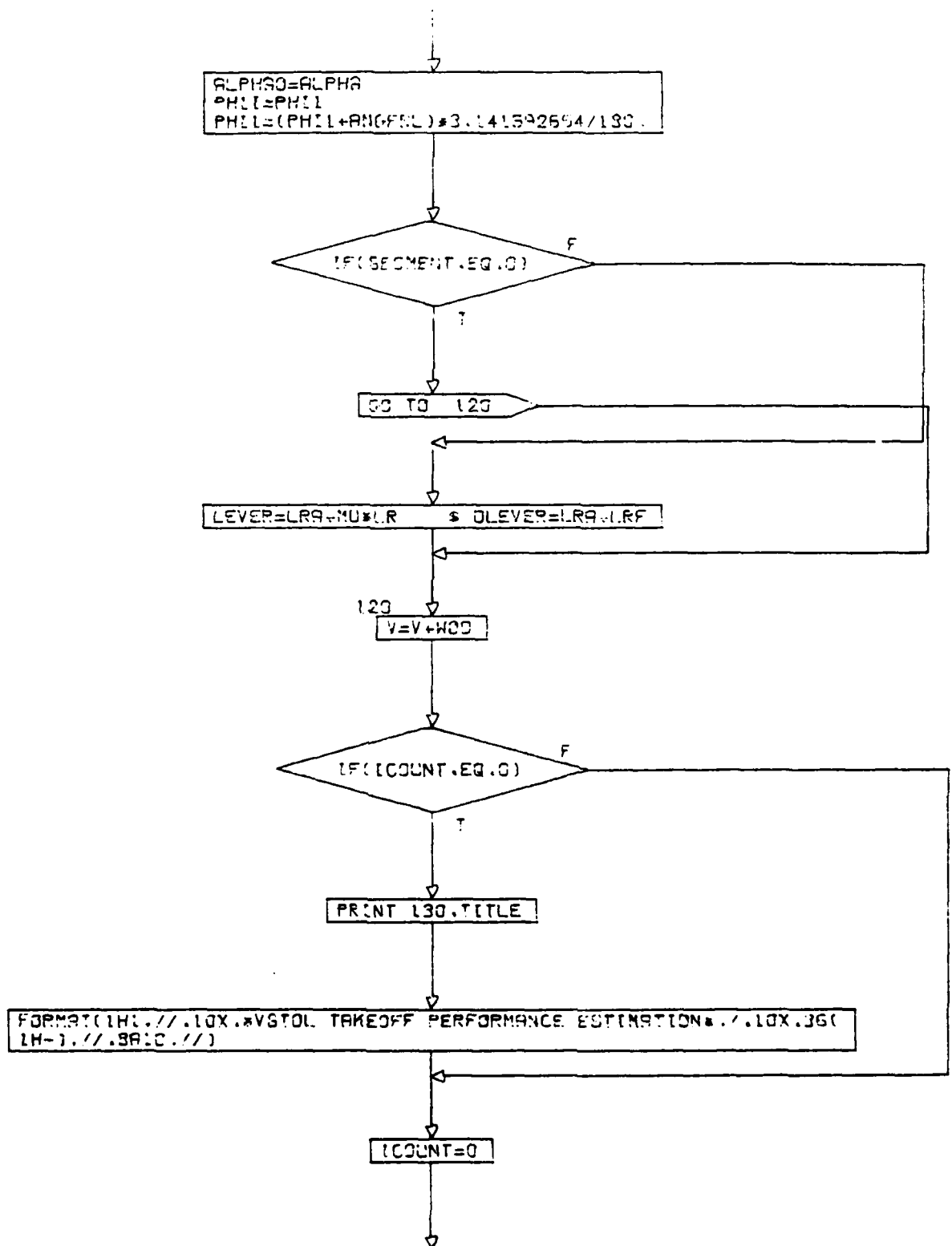
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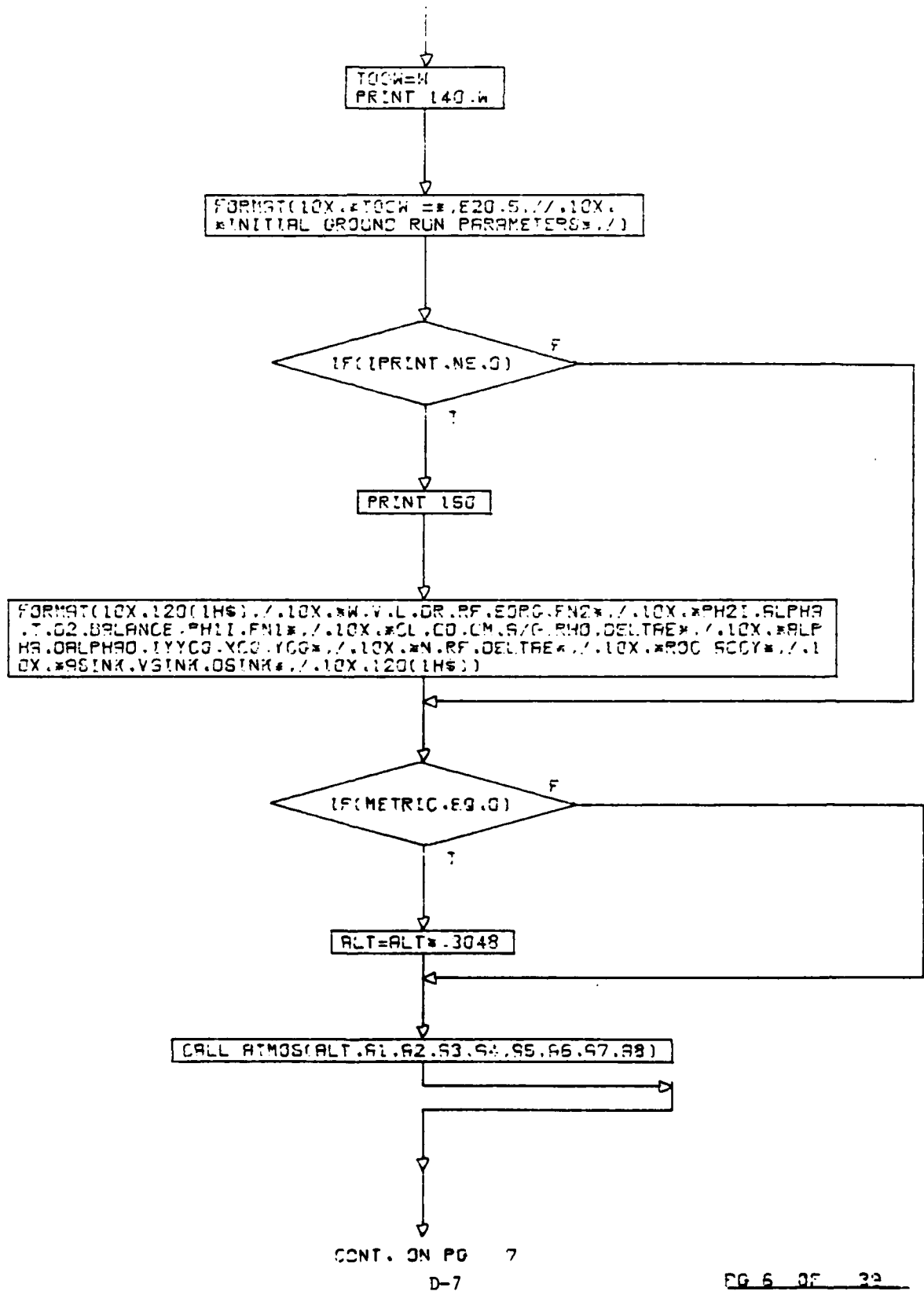
D-3

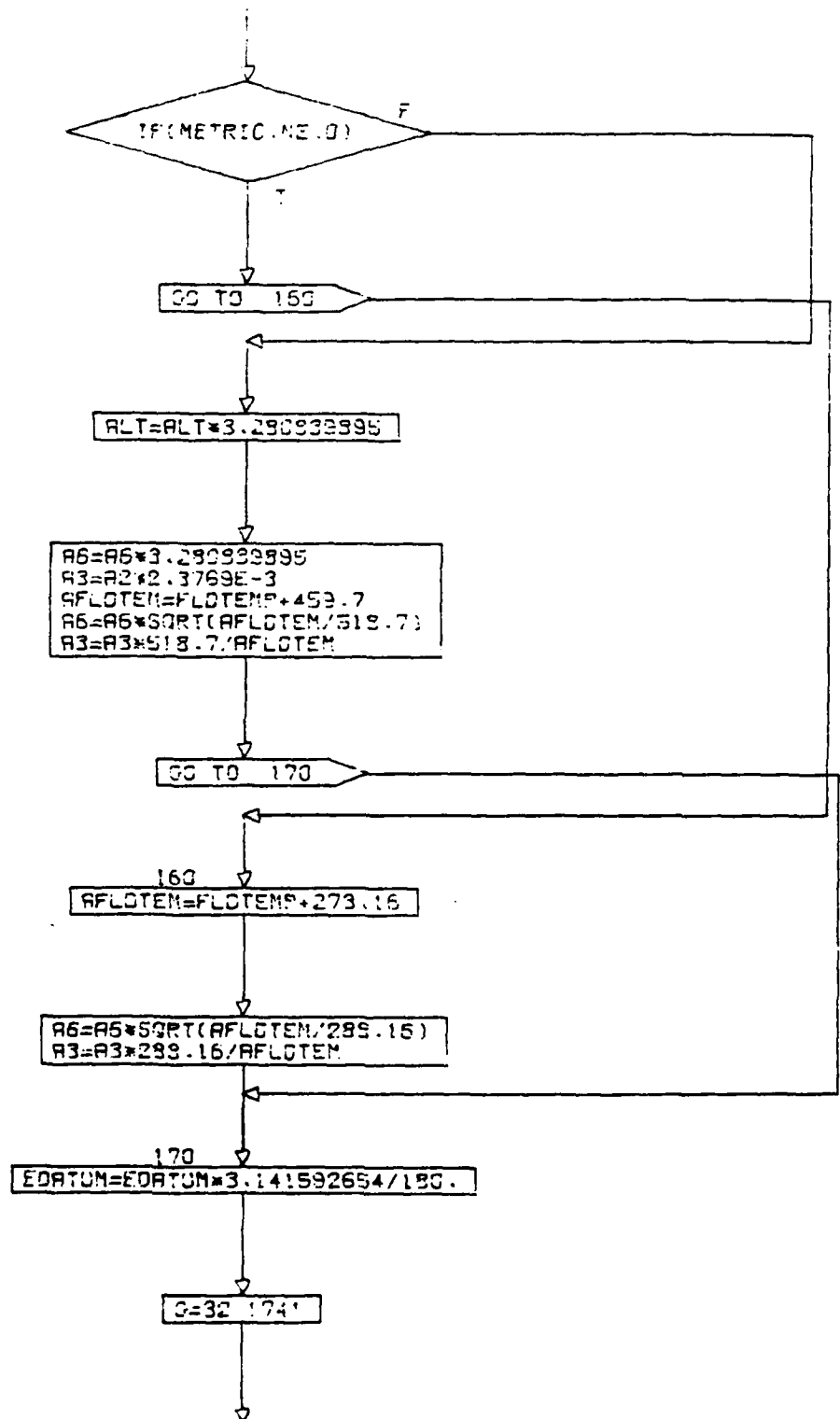
PG 2 OF 39

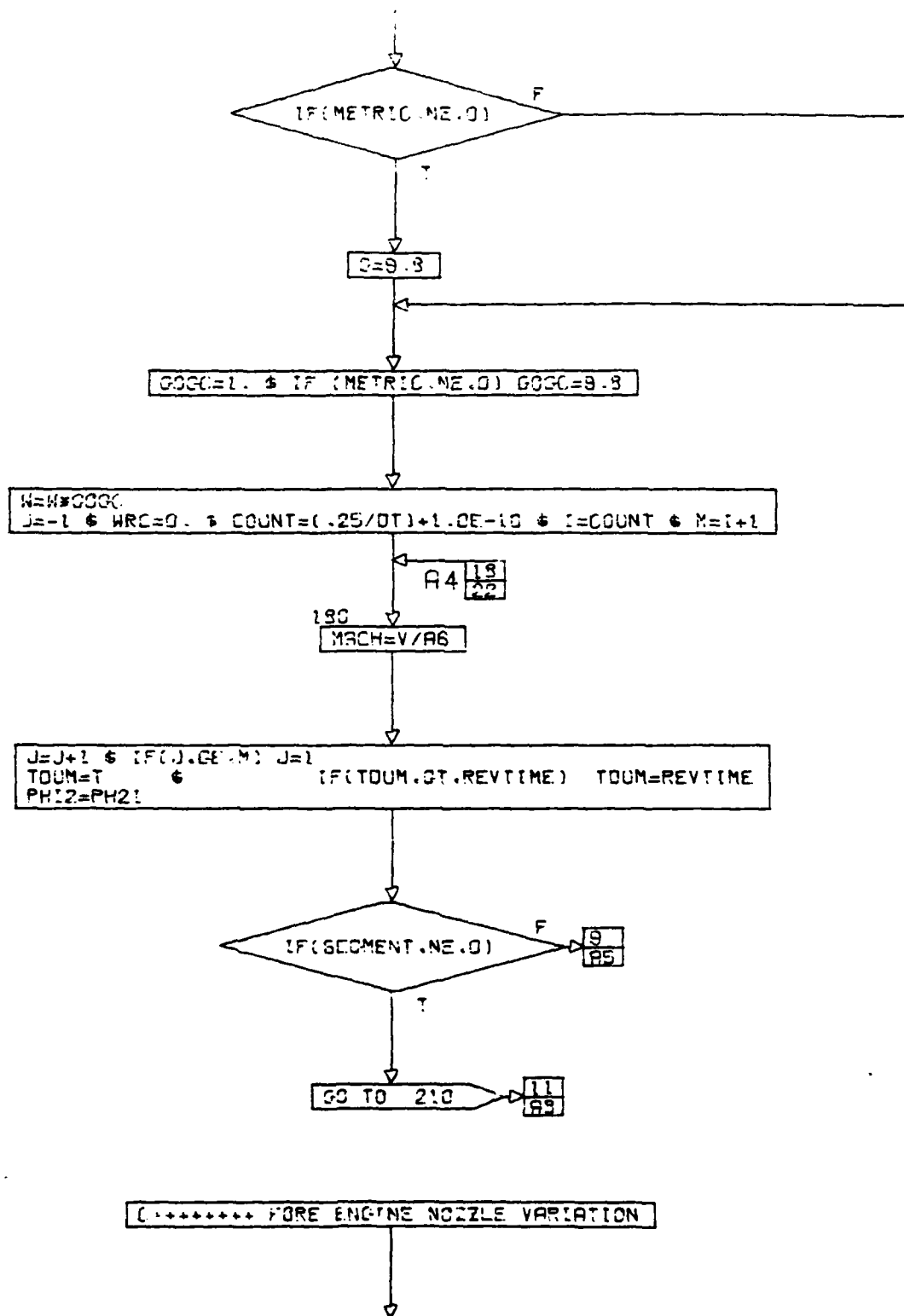


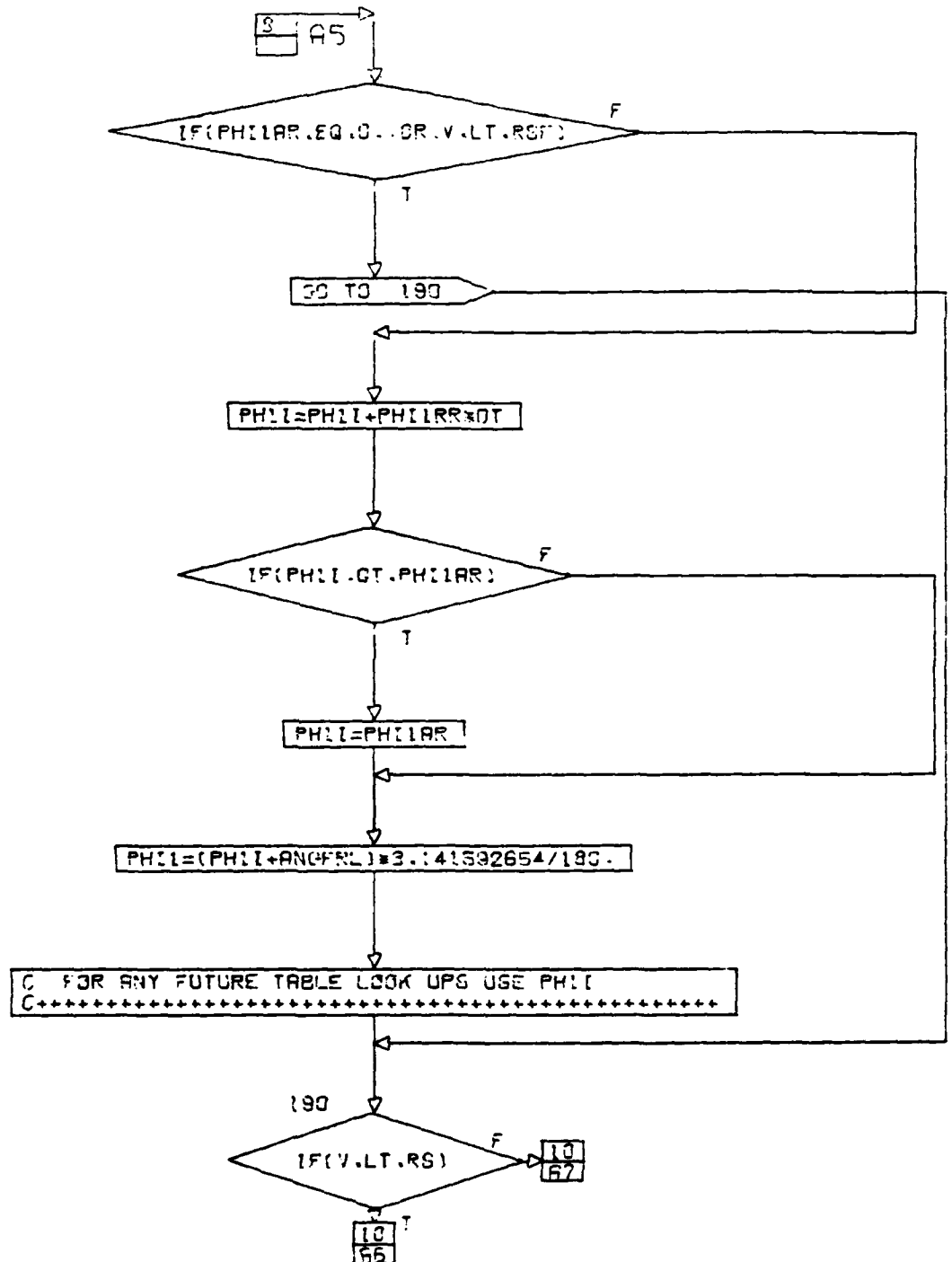


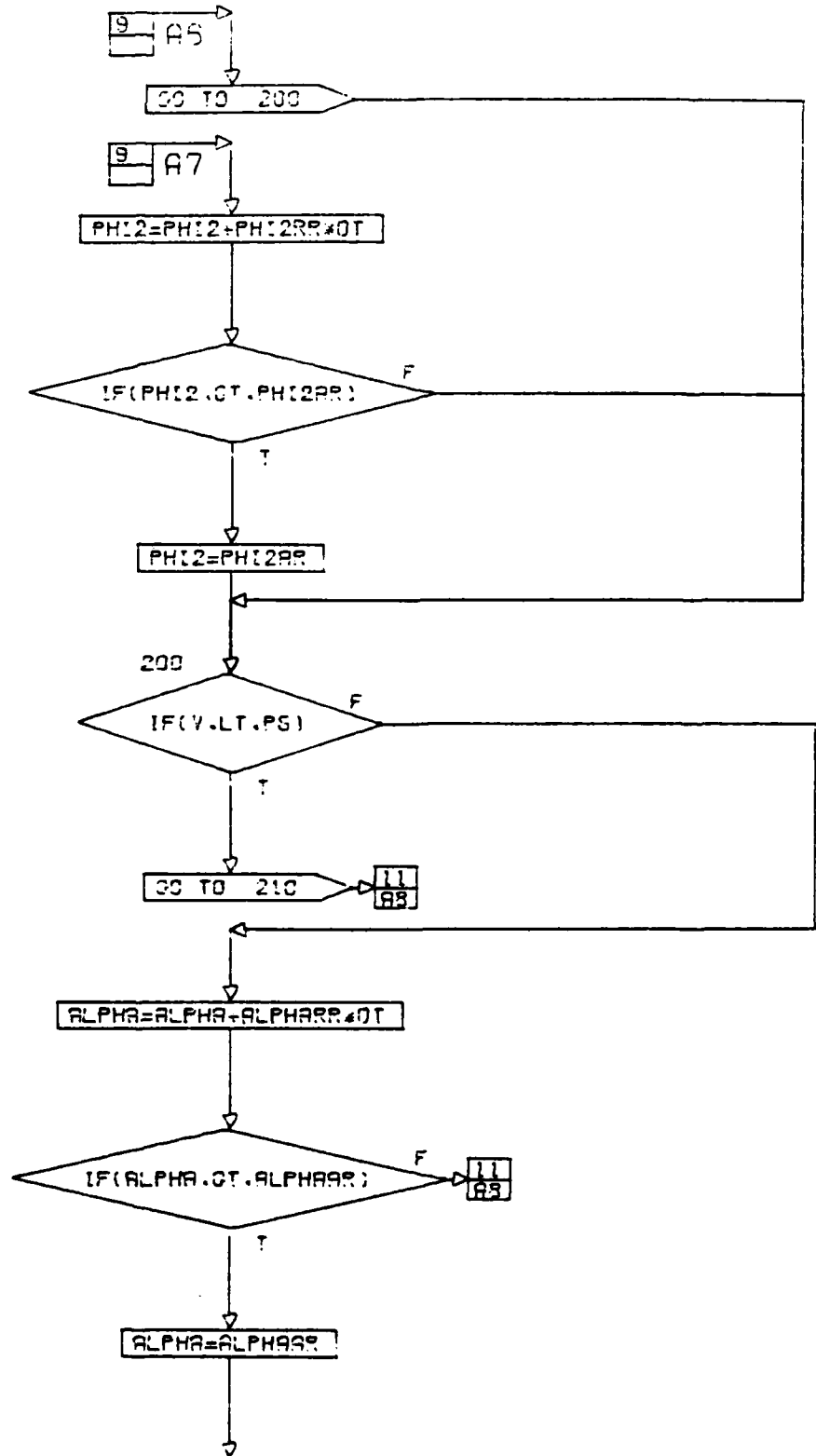


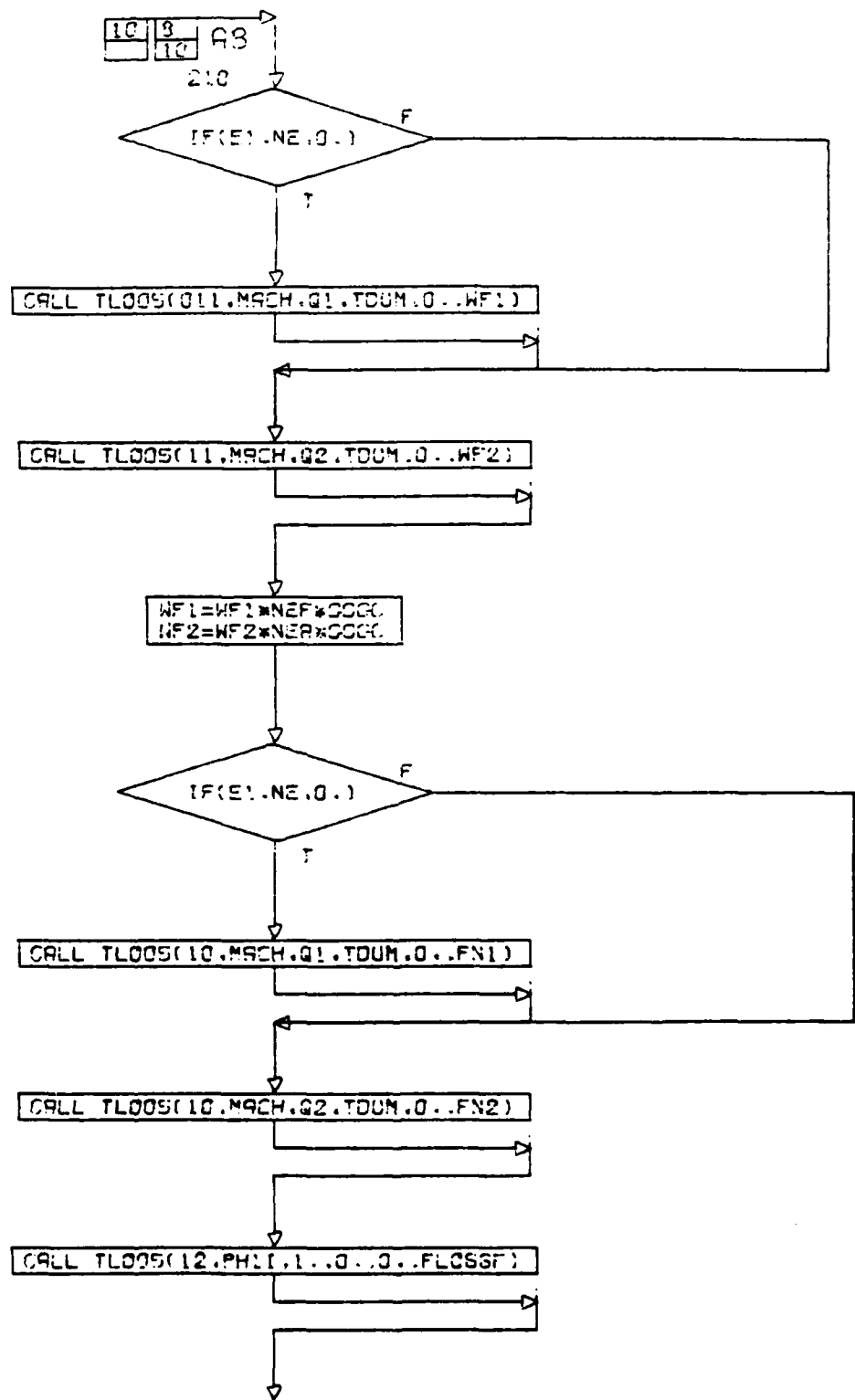


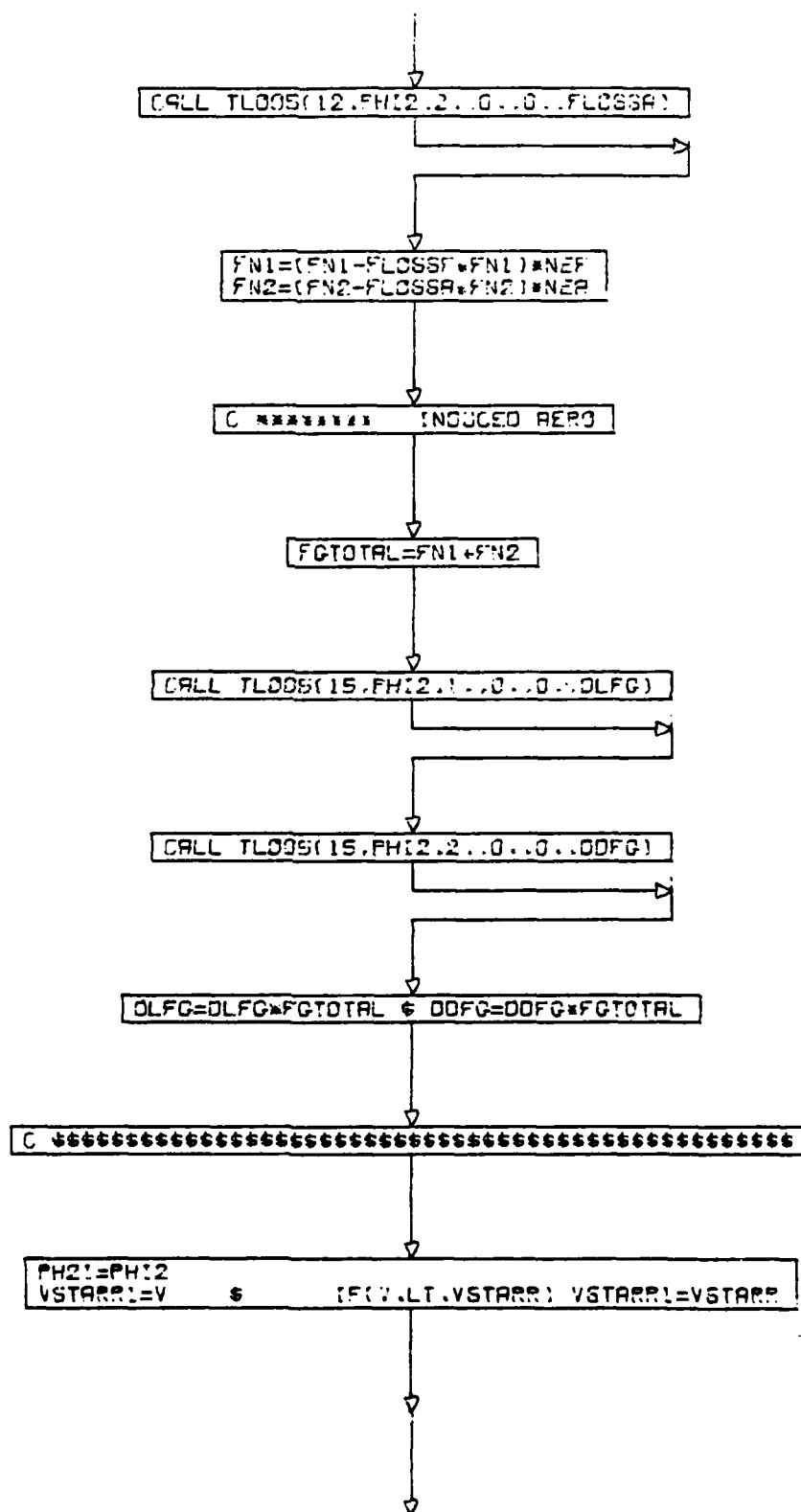


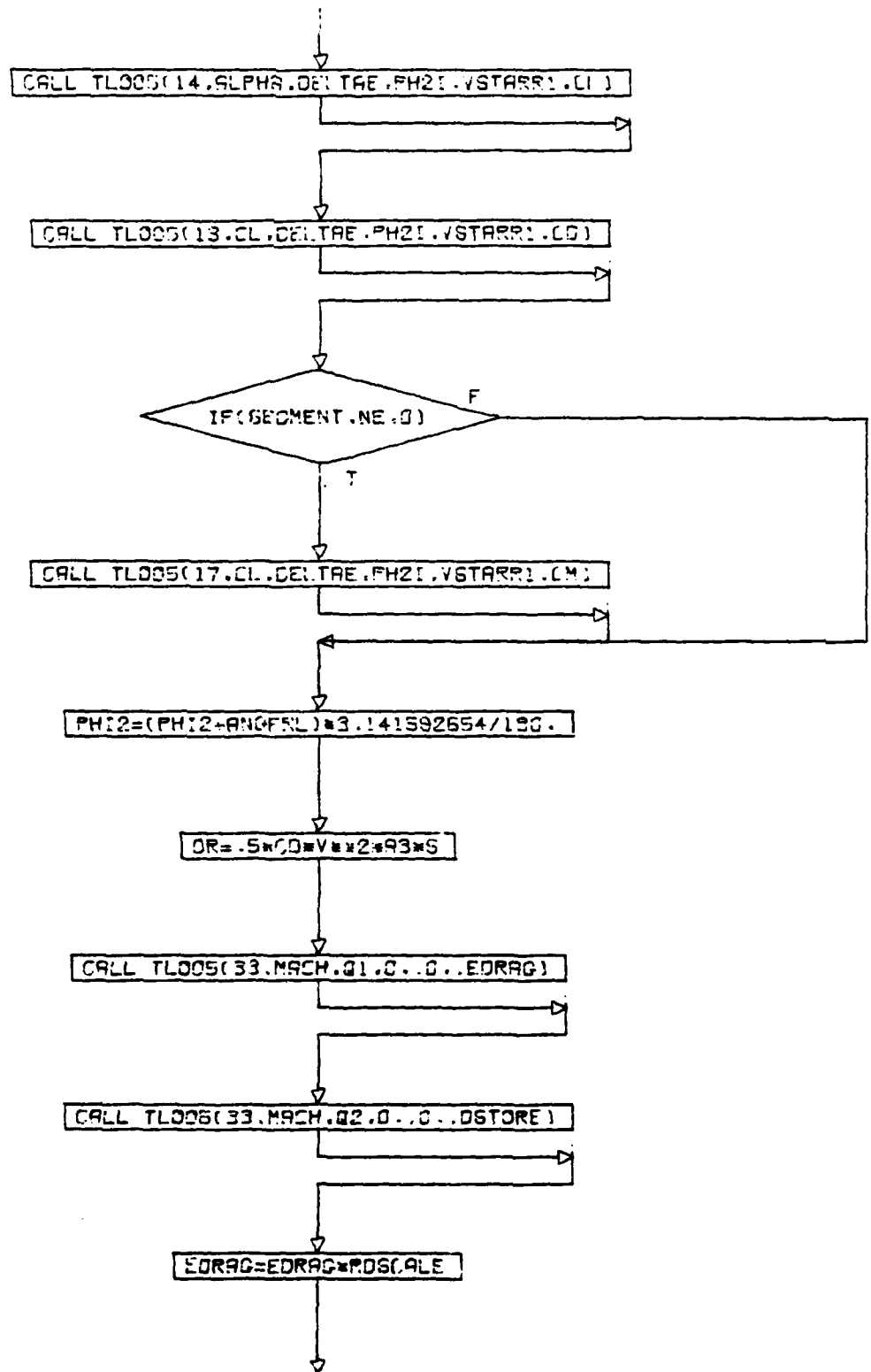


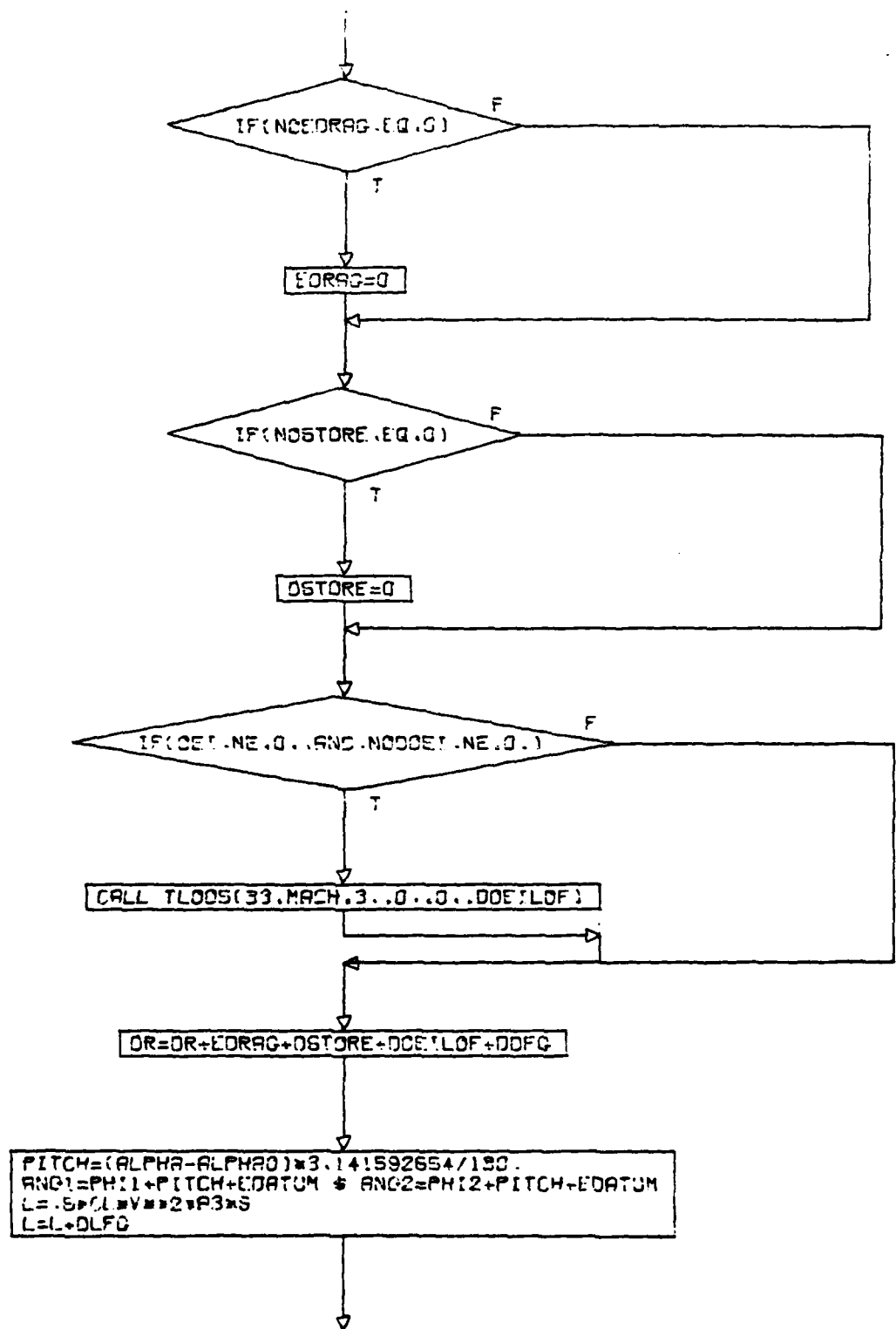


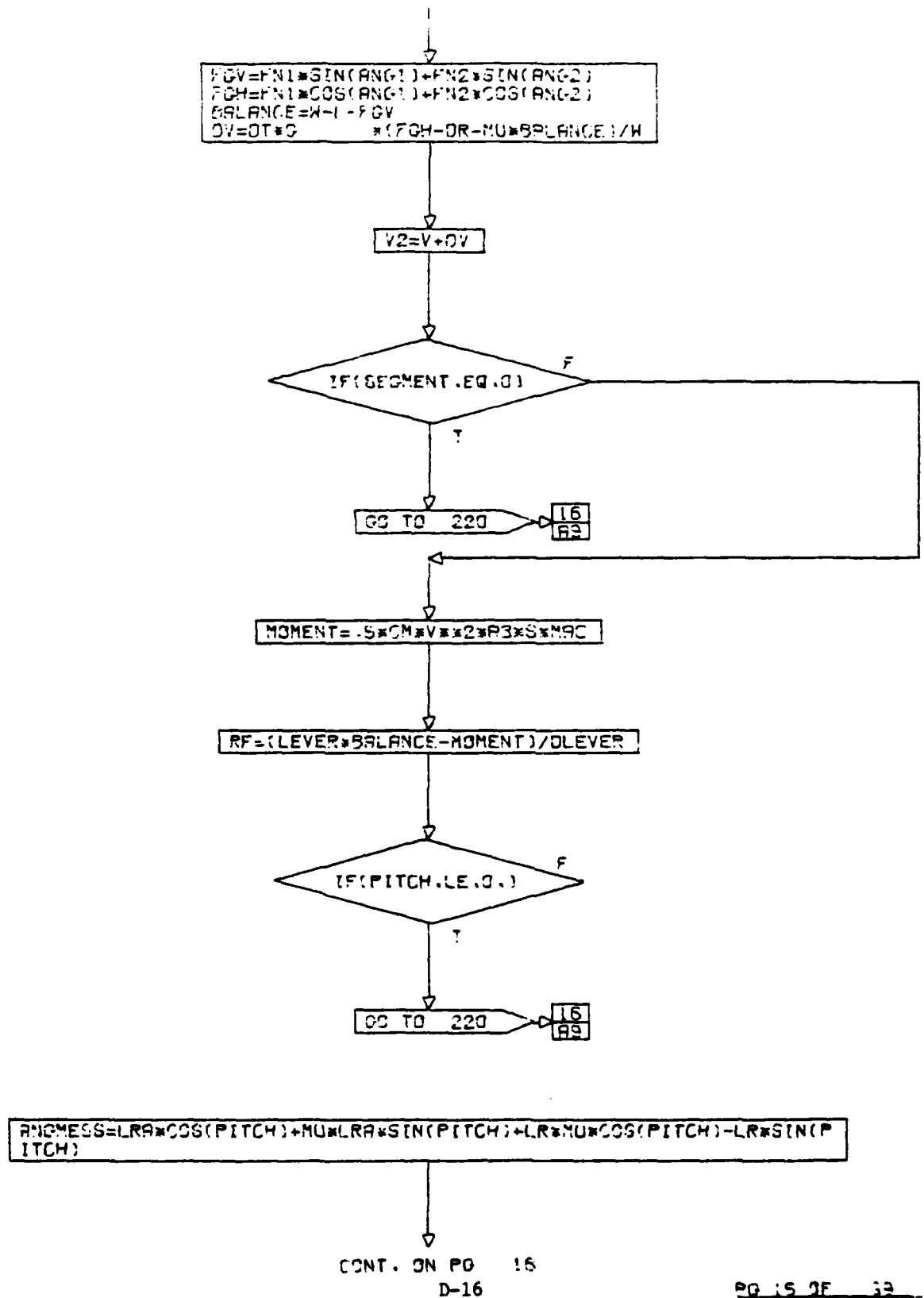


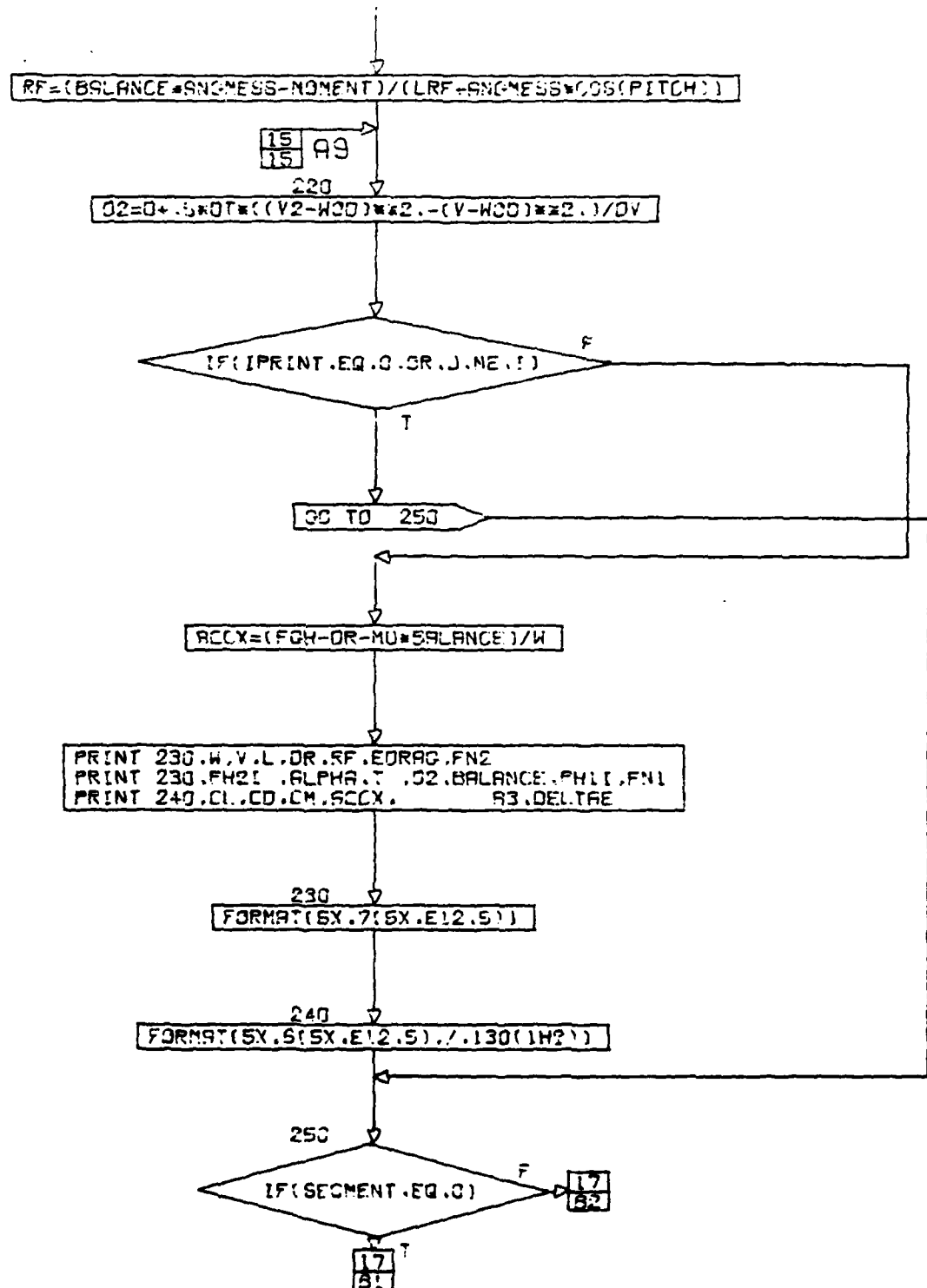


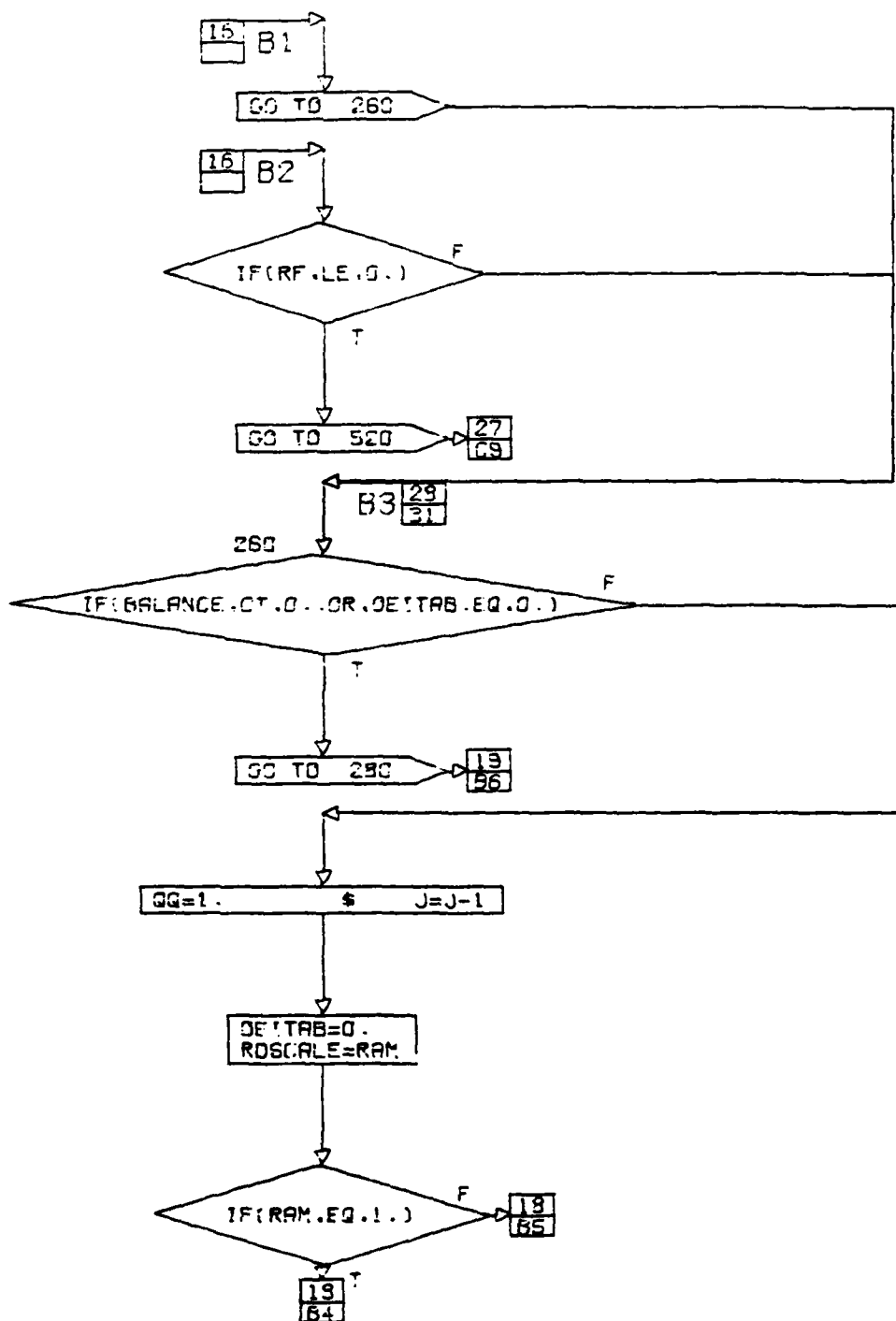


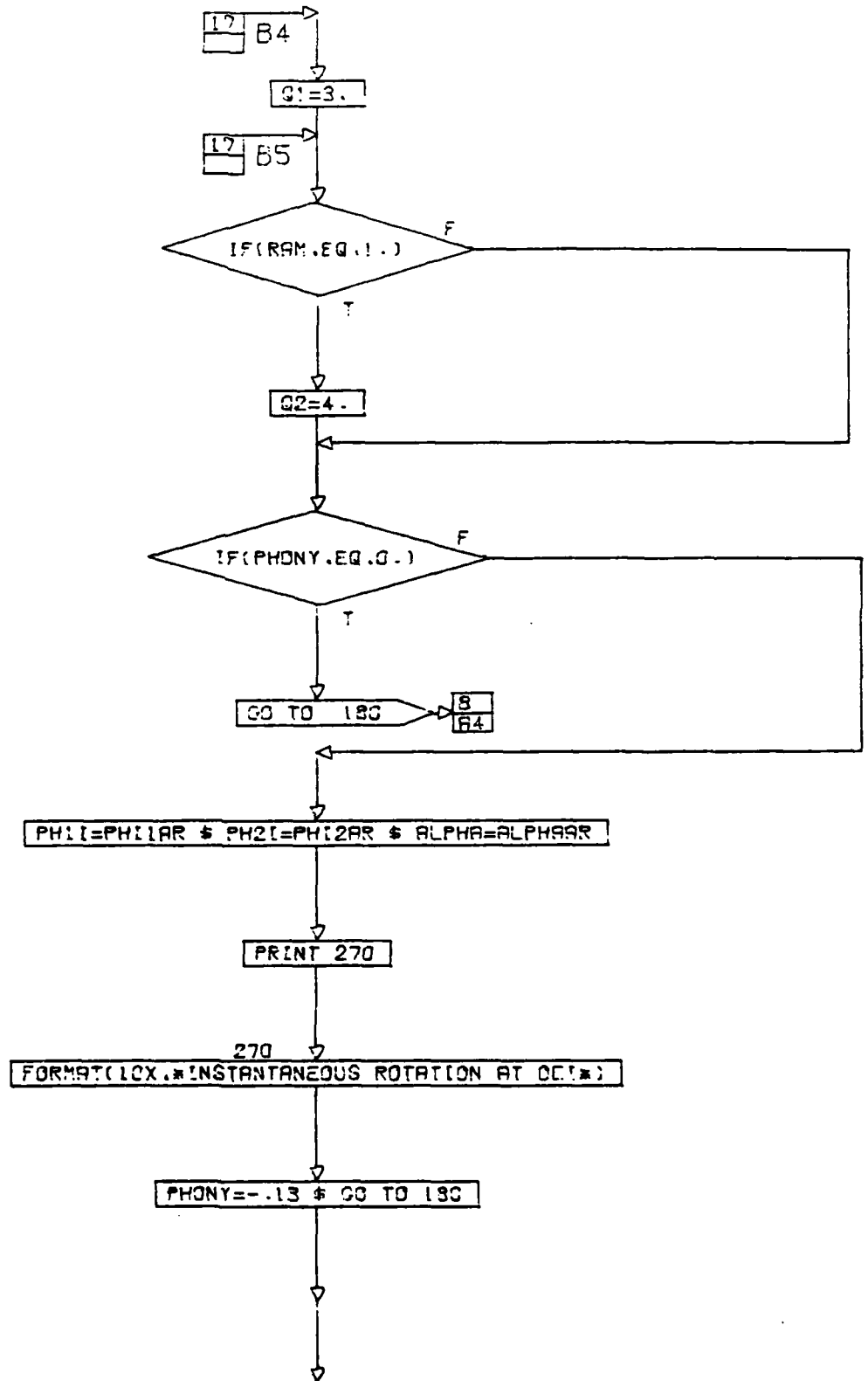


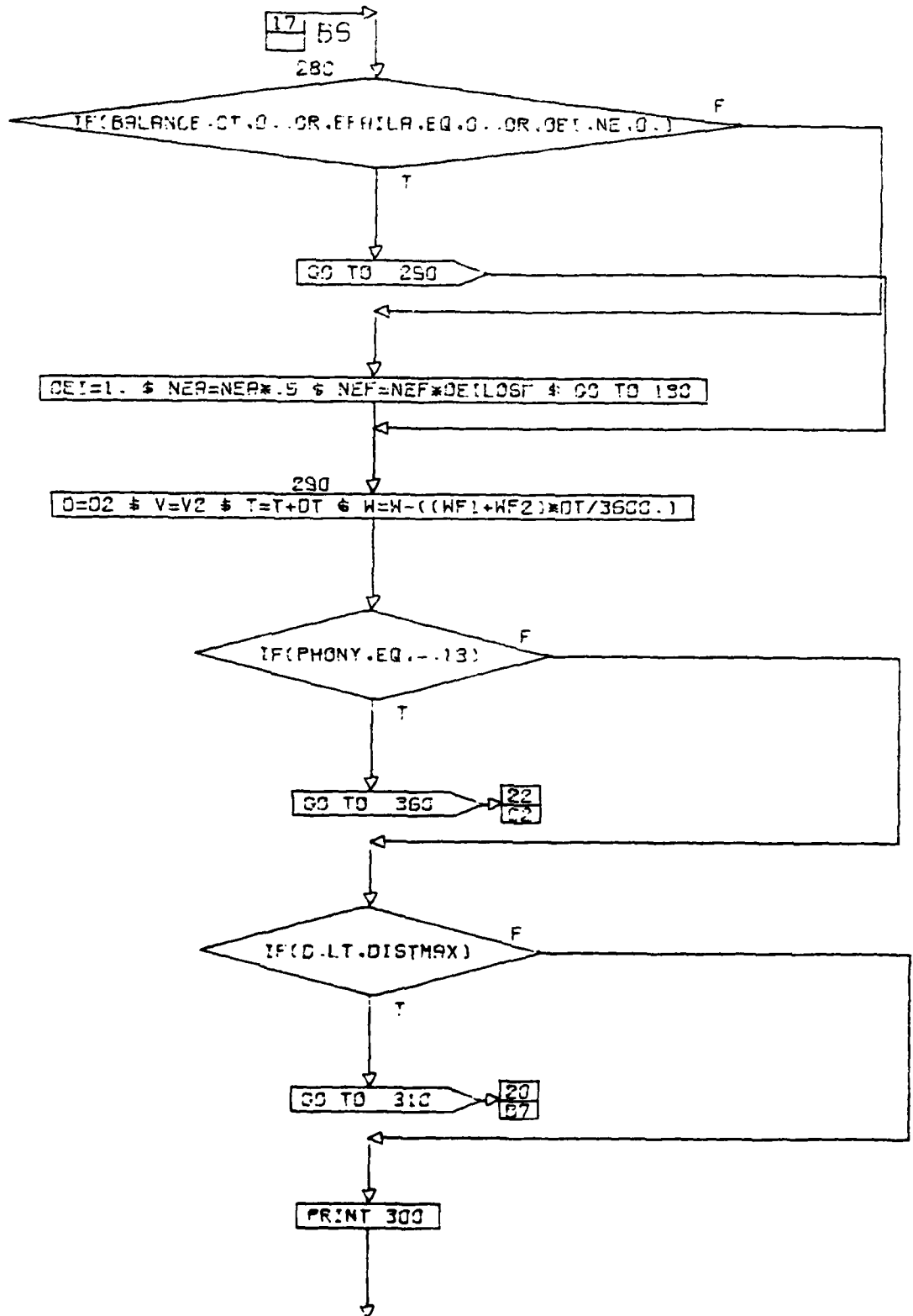


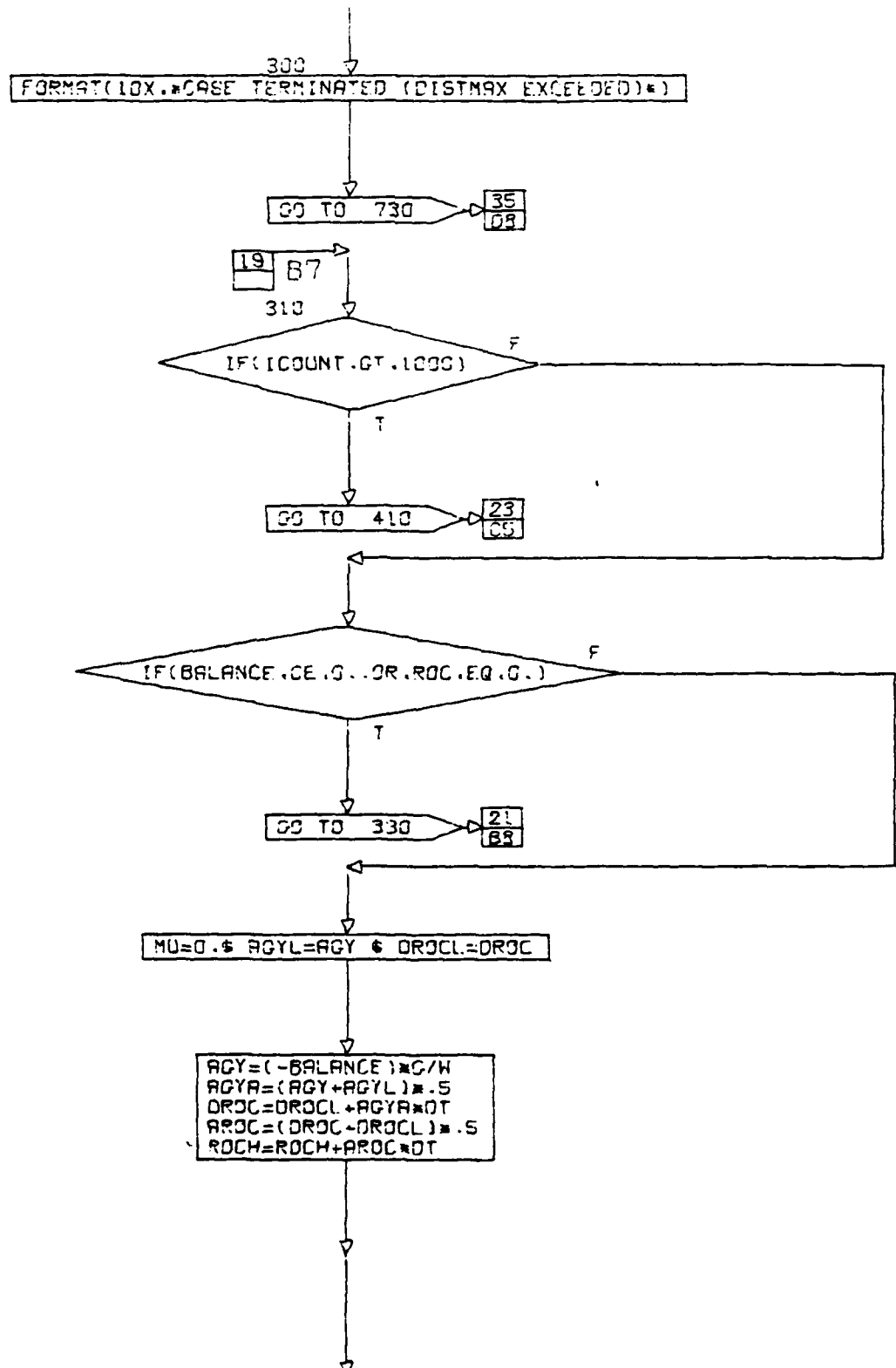


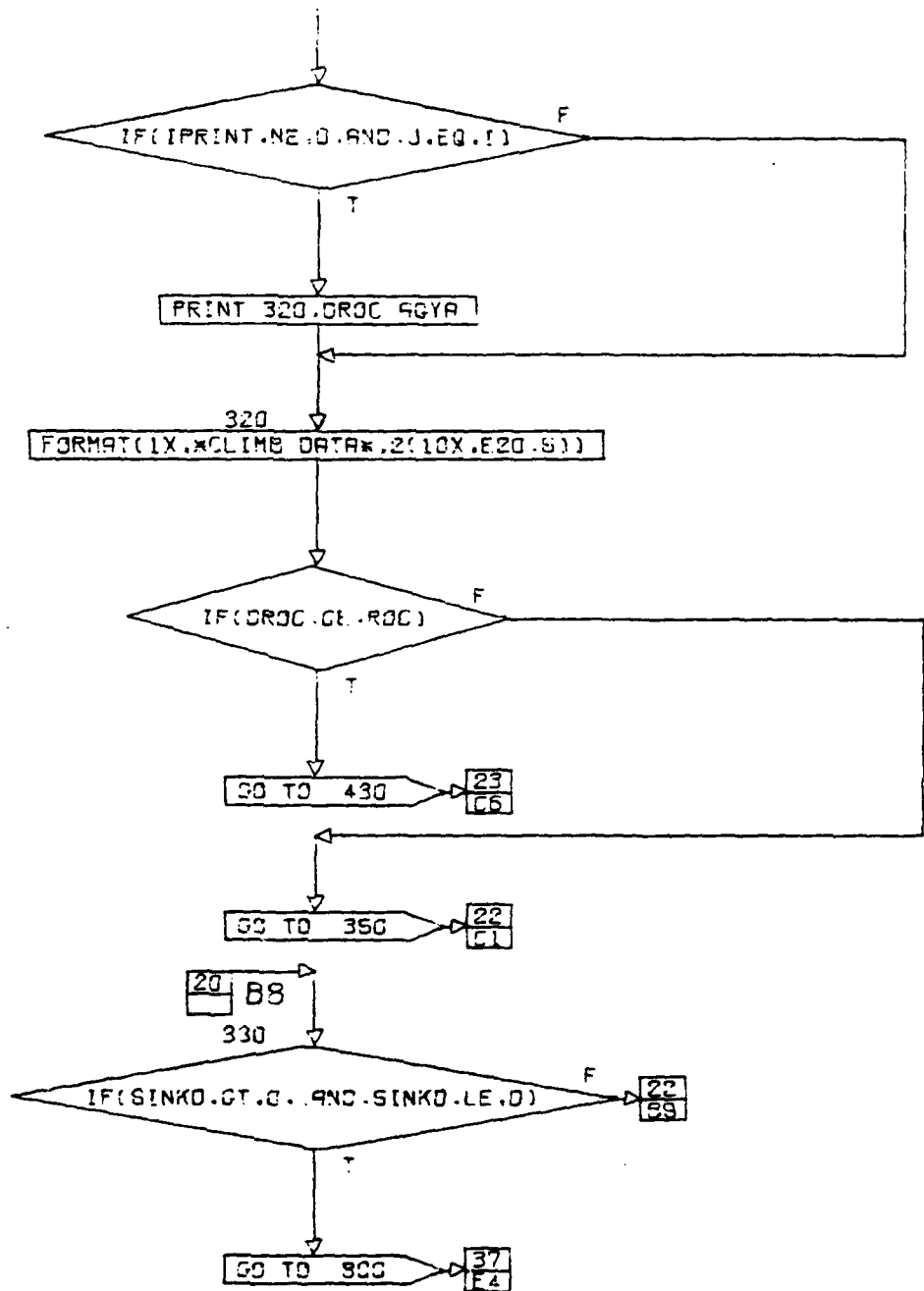


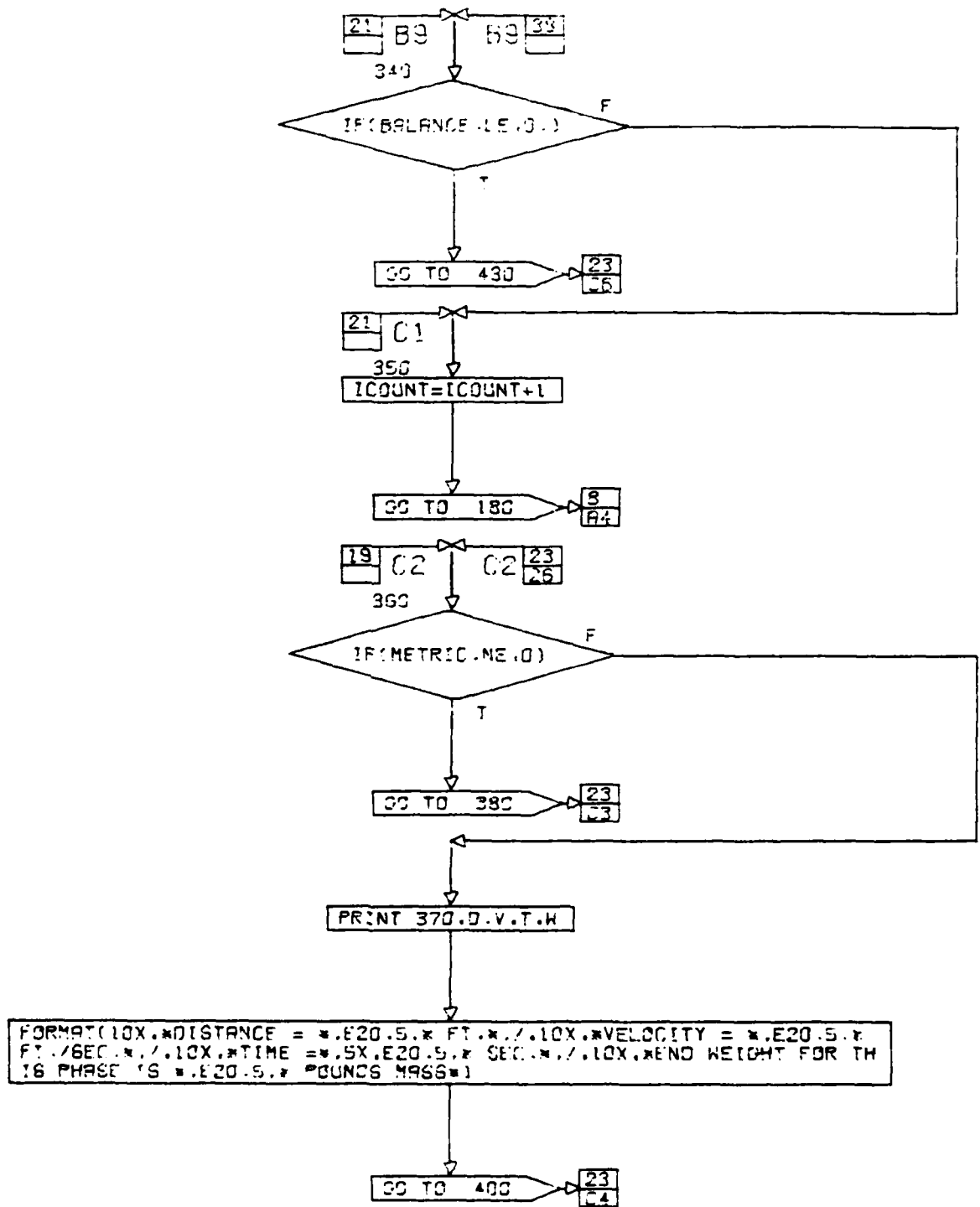


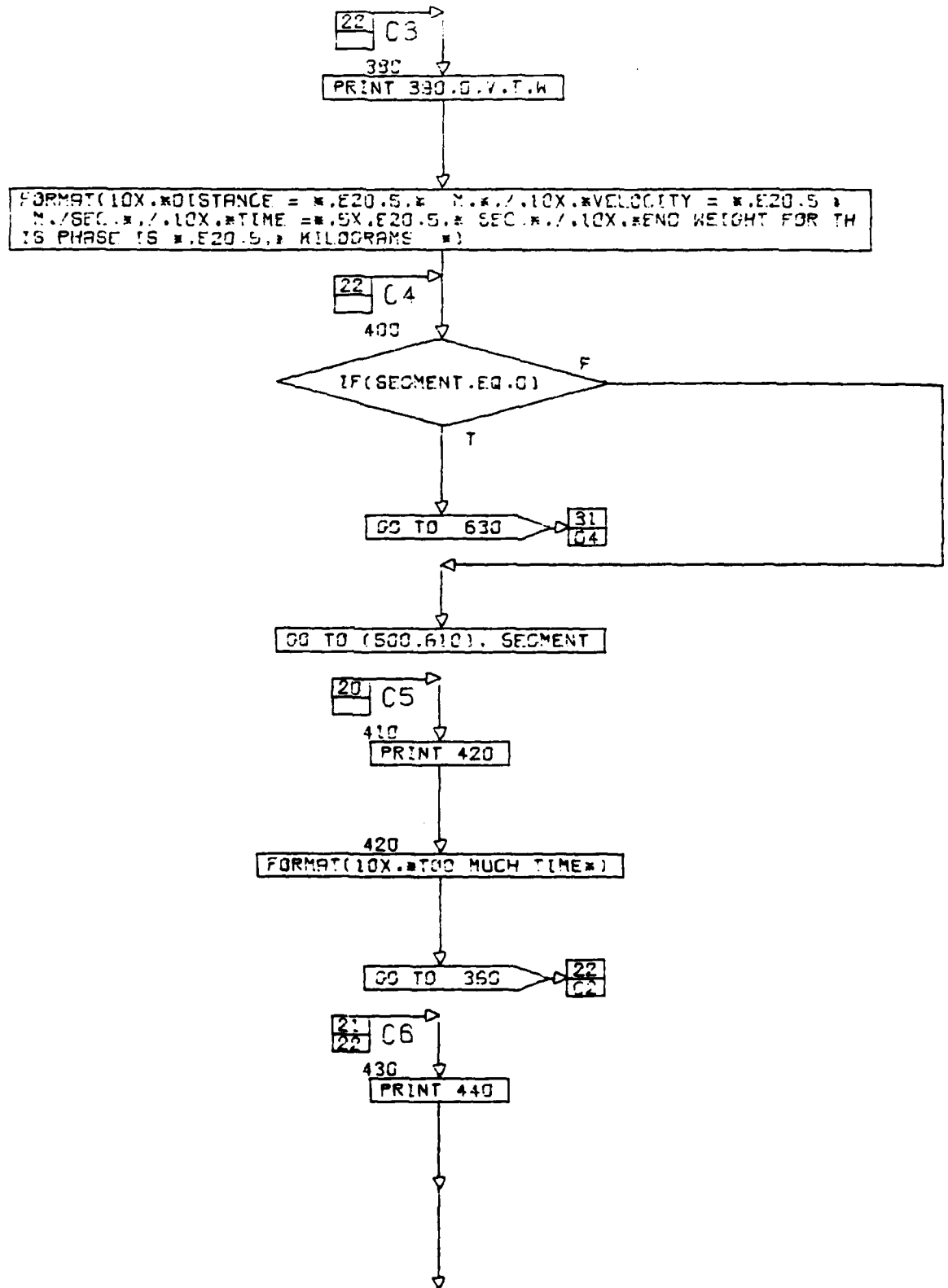


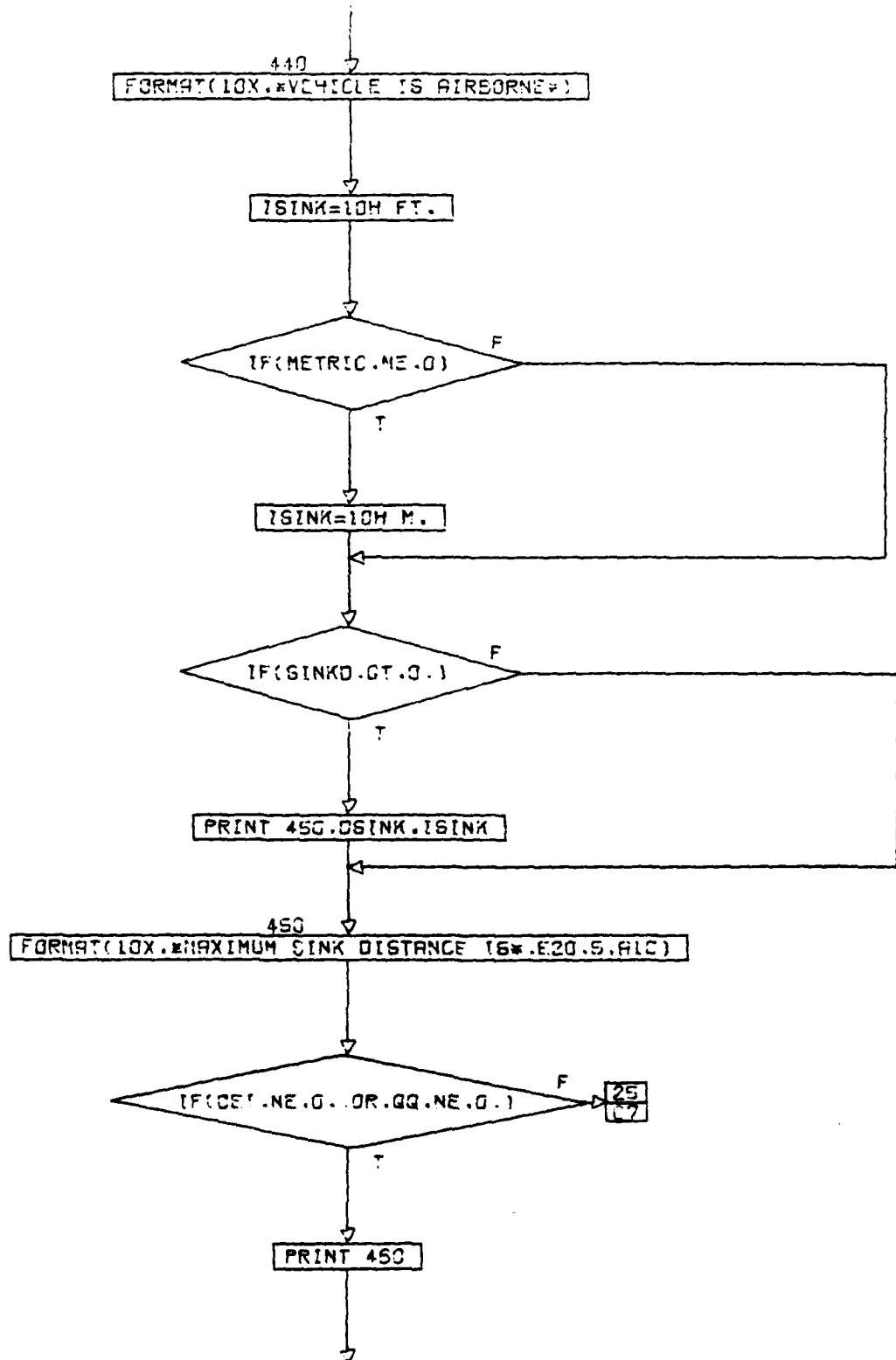


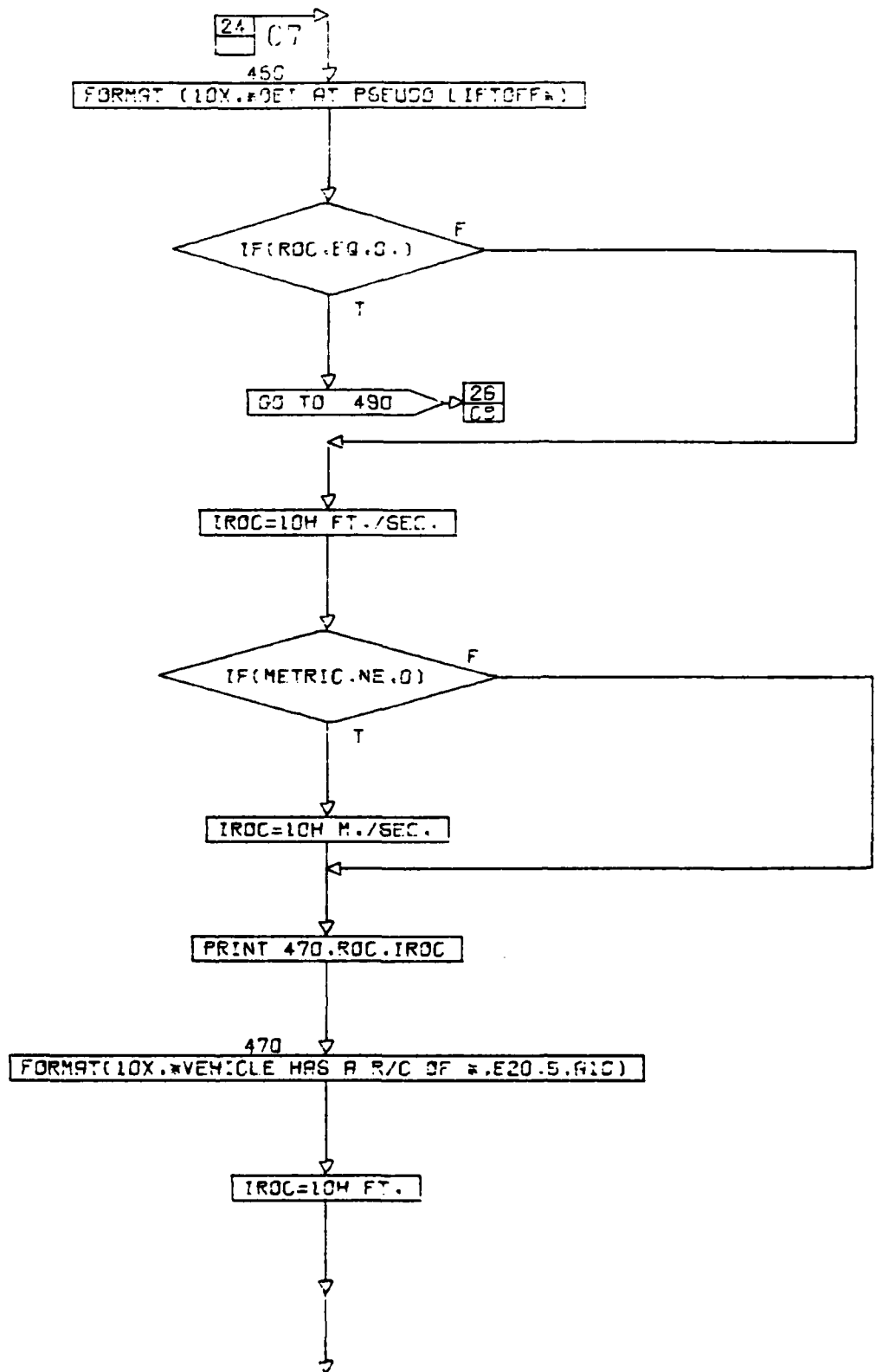


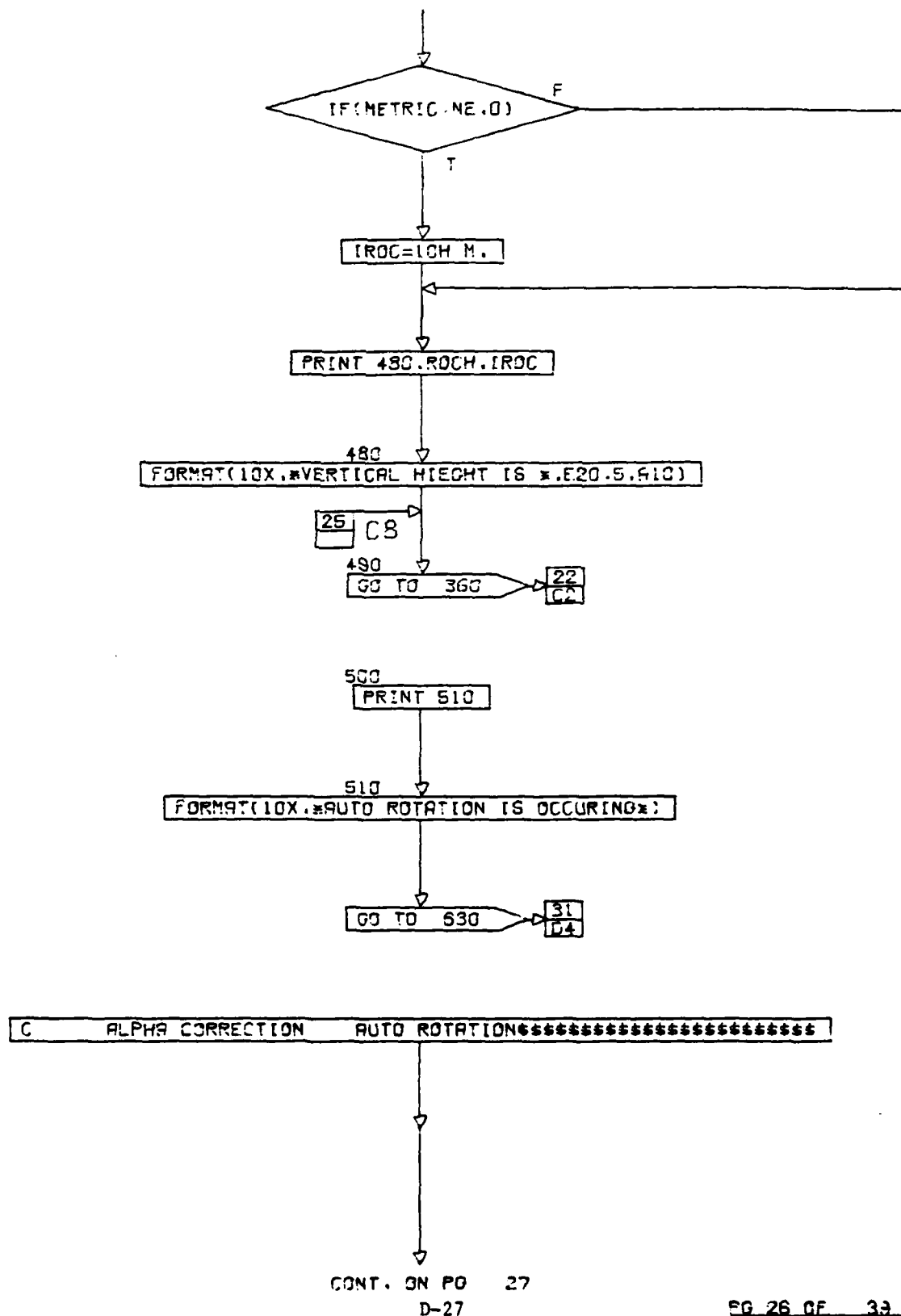


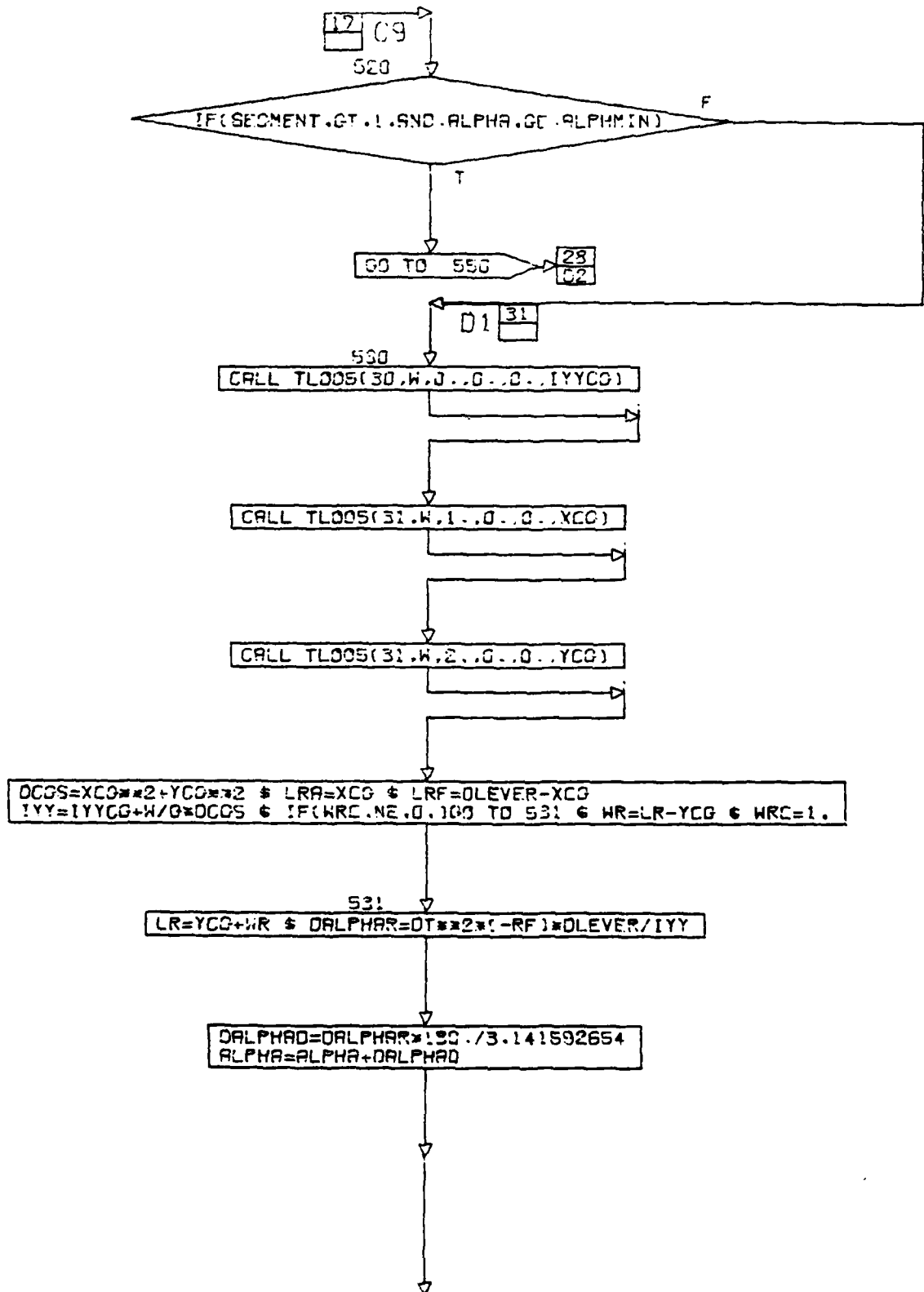


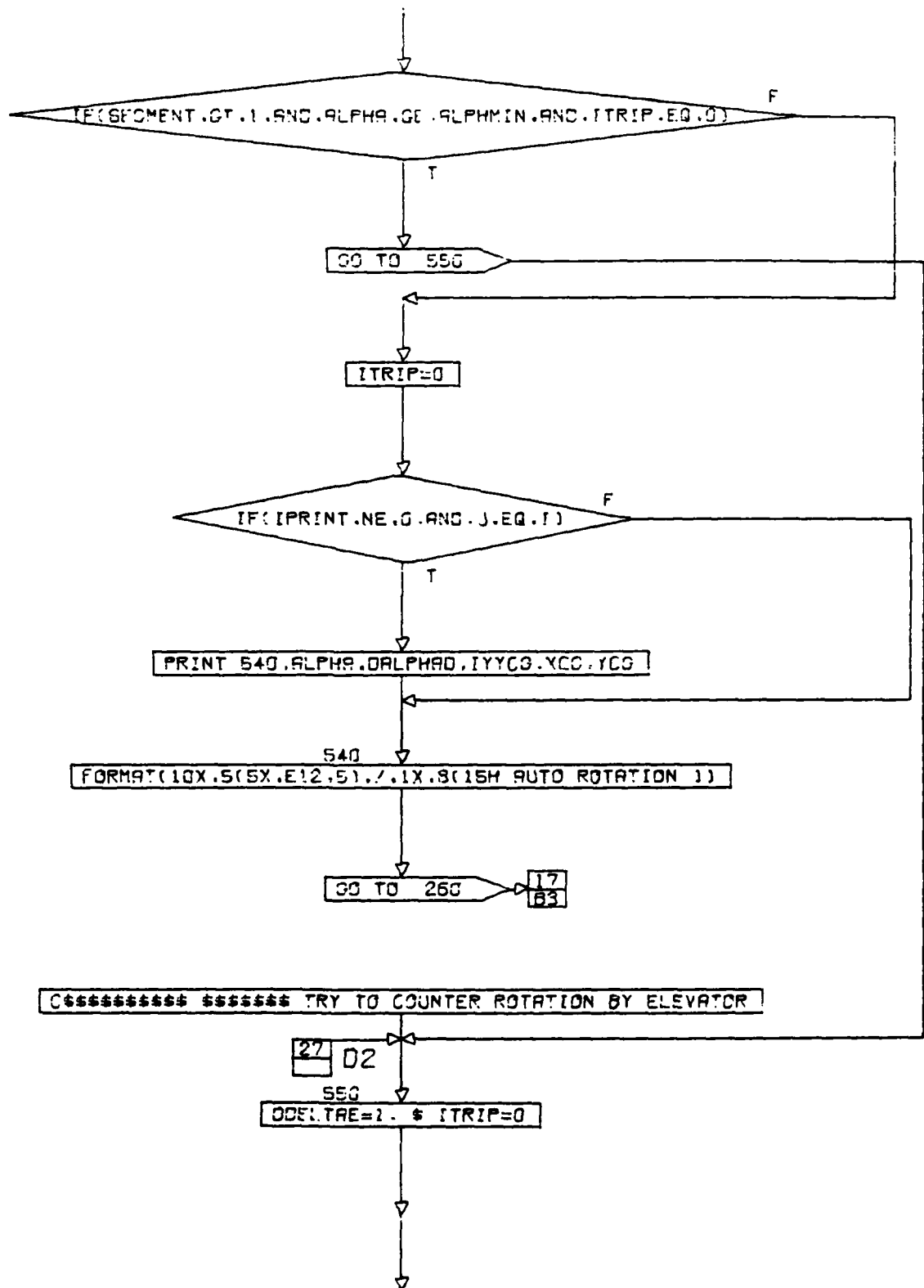


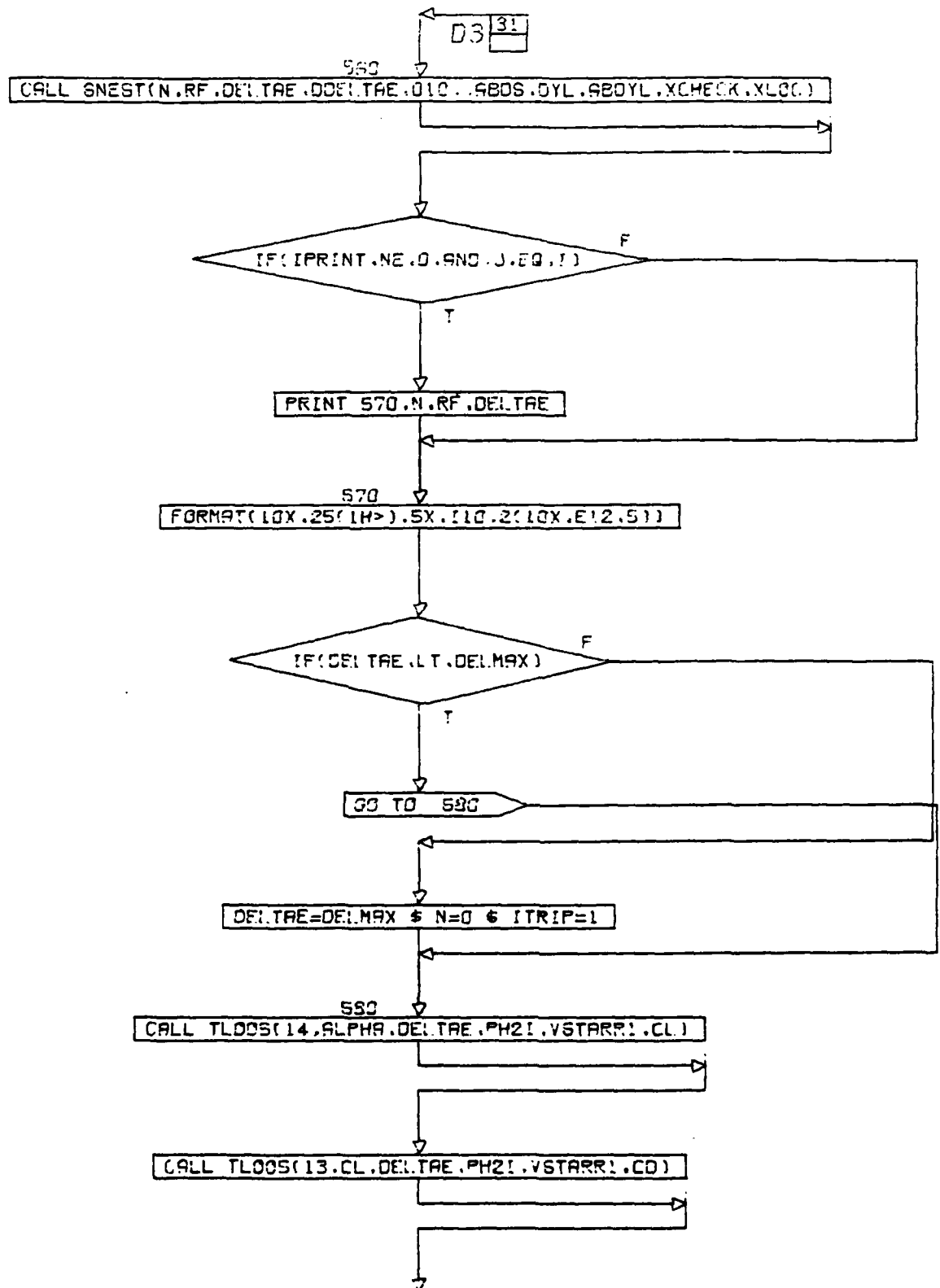












CALL TLOOS(17,CL,DELTA,PH2!,VSTARR!,CM)

$DR = .5 * CD * V^2 * A3 * S$
 $DR = DR + FDRAG + DSTORE + DCE * LOF + DDFG$
 $L = .5 * CL * V^2 * A3 * S$
 $L = L + DLFG$
 $BALANCE = W - L - FGV$
 $OV = DT * G * (FGH - DR - MU * BALANCE) / W$
 $V2 = V + OV$
 $MOMENT = .5 * CM * V^2 * A3 * S * MAC$

$RF = (LEVER * BALANCE - MOMENT) / DLEVER$

IF (PITCH, LE, Q.)

GO TO 530

$ANGMESS = LRA * COS(PITCH) + MU * LRA * SIN(PITCH) + LR * MU * COS(PITCH) - LR * SIN(PITCH)$

$RF = (BALANCE * ANGMESS - MOMENT) / (LRF + ANGMESS * COS(PITCH))$

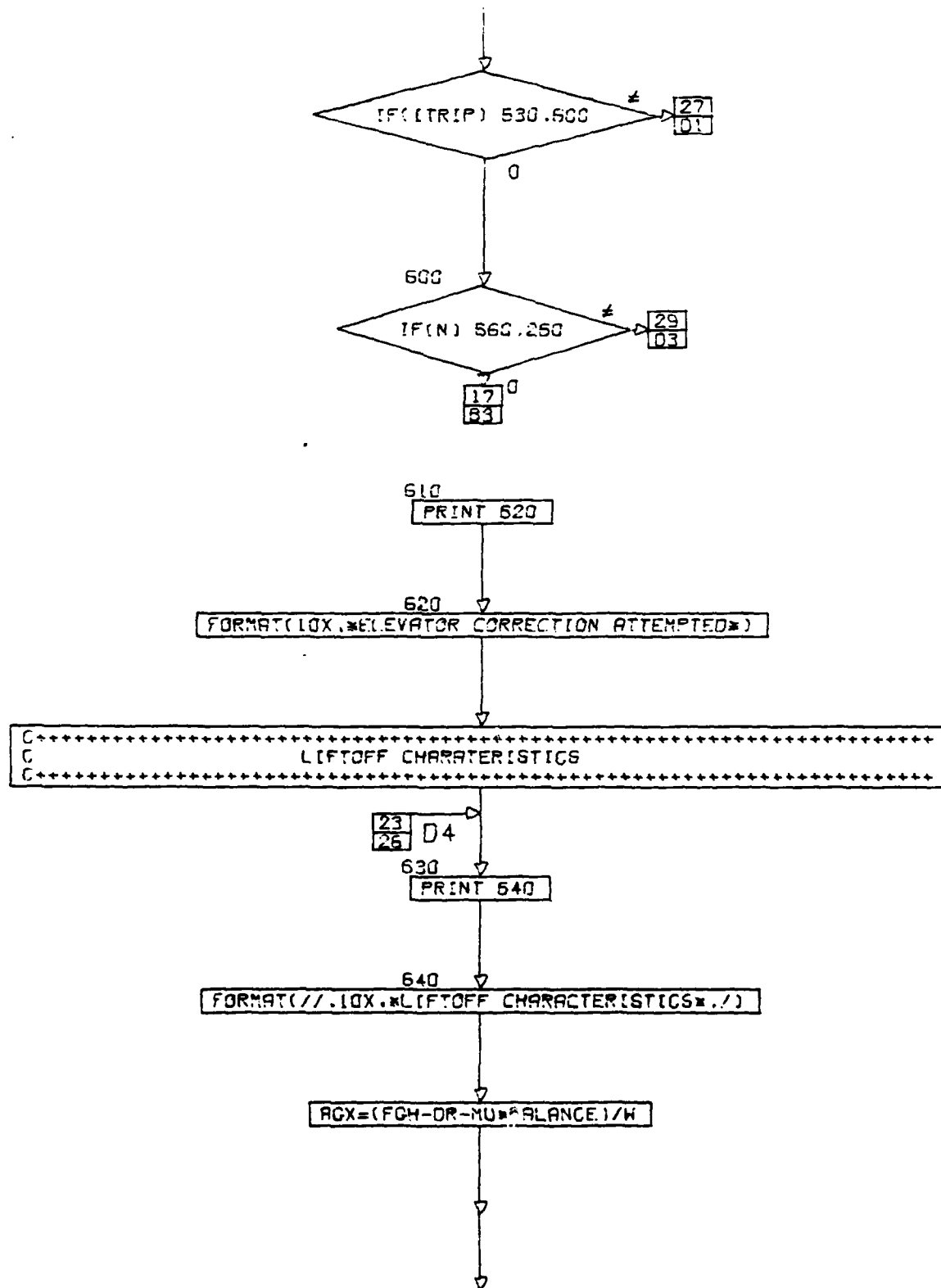
530

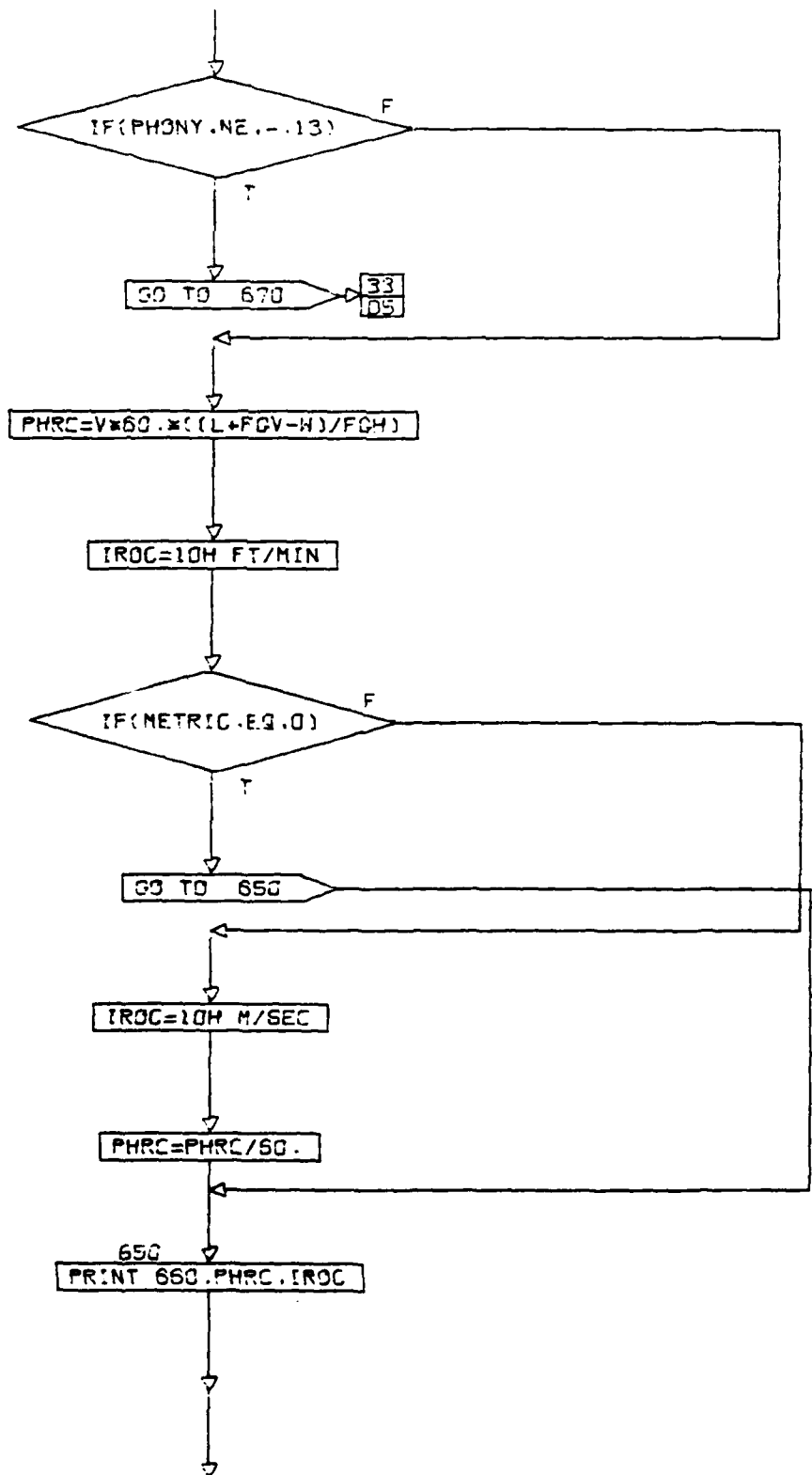
$D2 = D + .5 * DT * ((V2 - WCD)^2 - (V - WCD)^2) / OV$

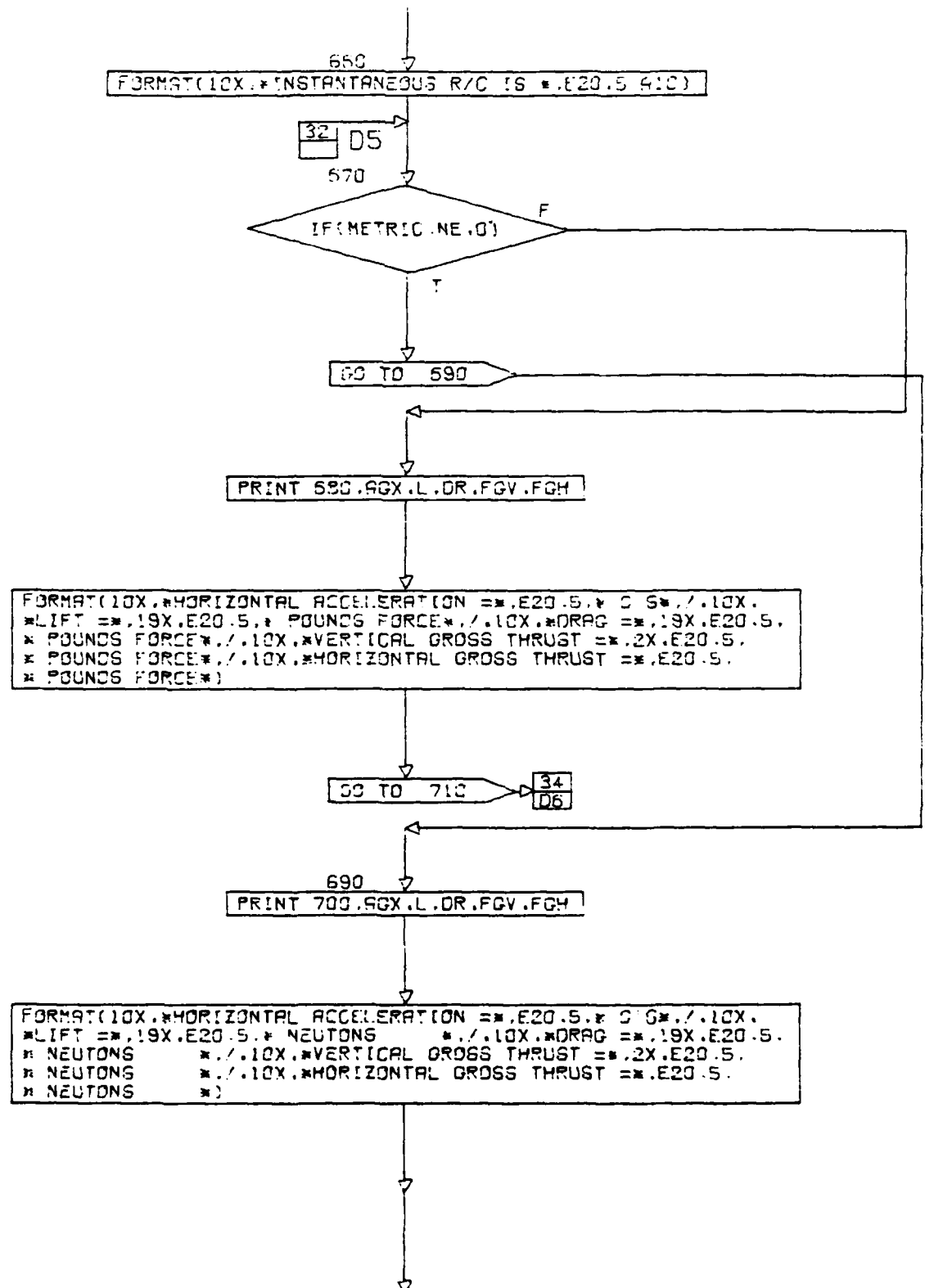
CONT. ON PG 31

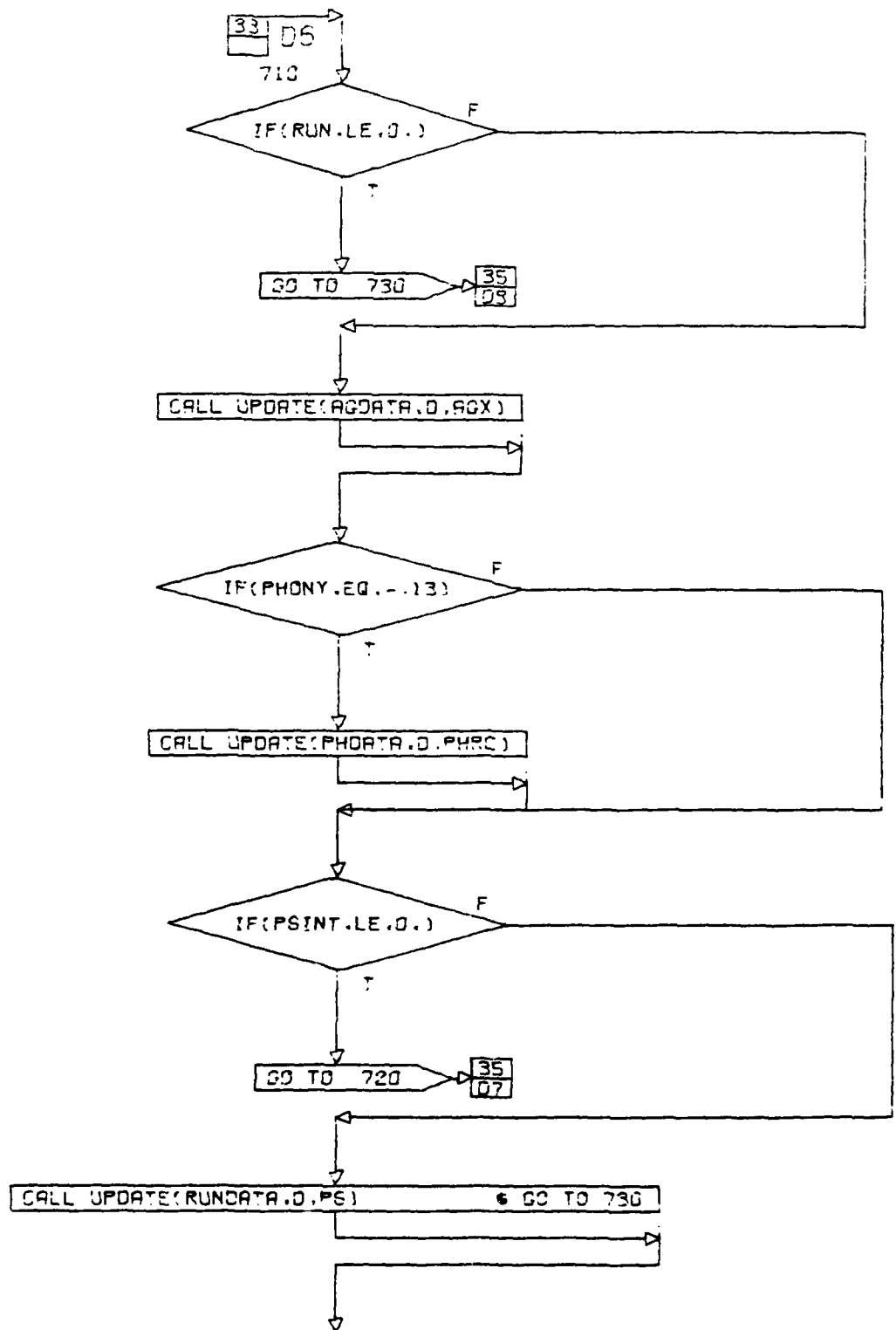
D-31

PG 30 OF 33









AD-A109 861 NAVAL AIR DEVELOPMENT CENTER WARMINSTER PA AIRCRAFT --ETC F/G 1/3
A SHORT TAKEOFF PERFORMANCE COMPUTER PROGRAM.(U)
NOV 81 D B KOBUS

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NL

2 2

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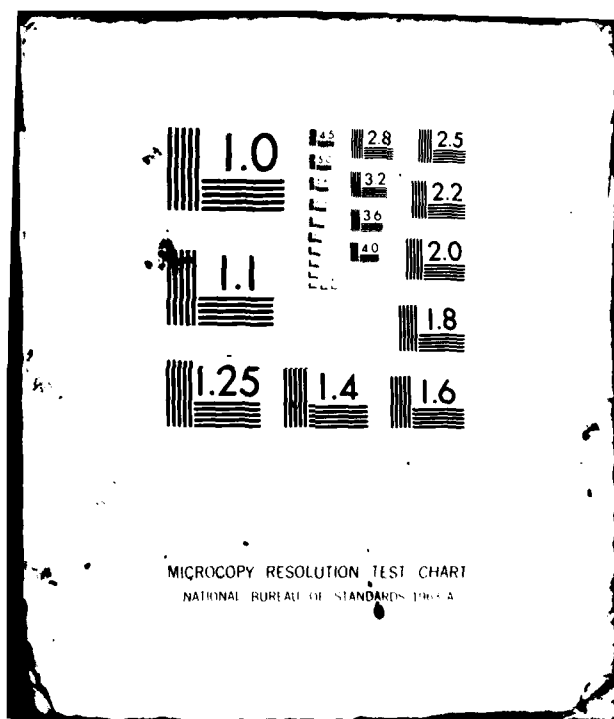
END

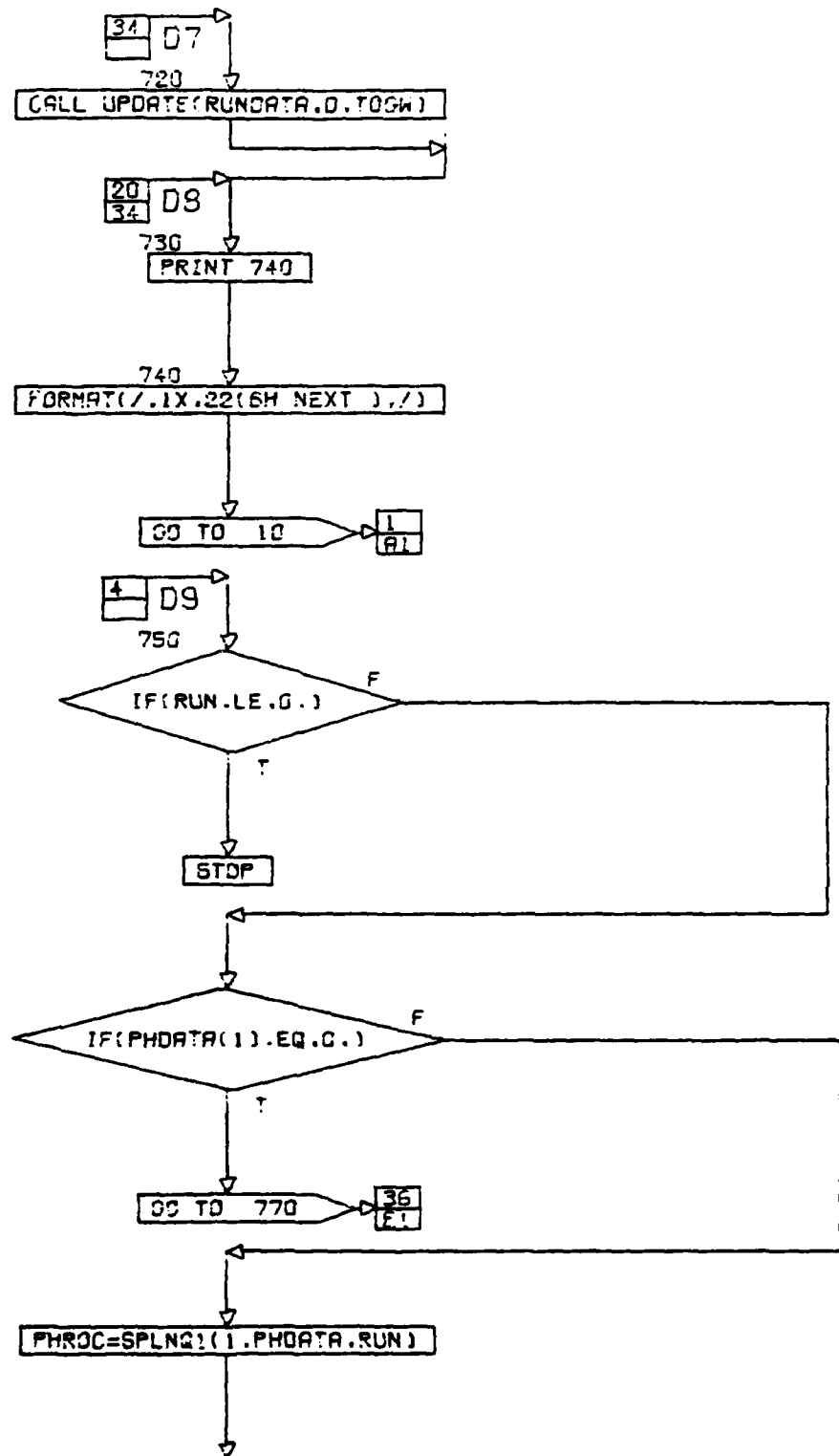
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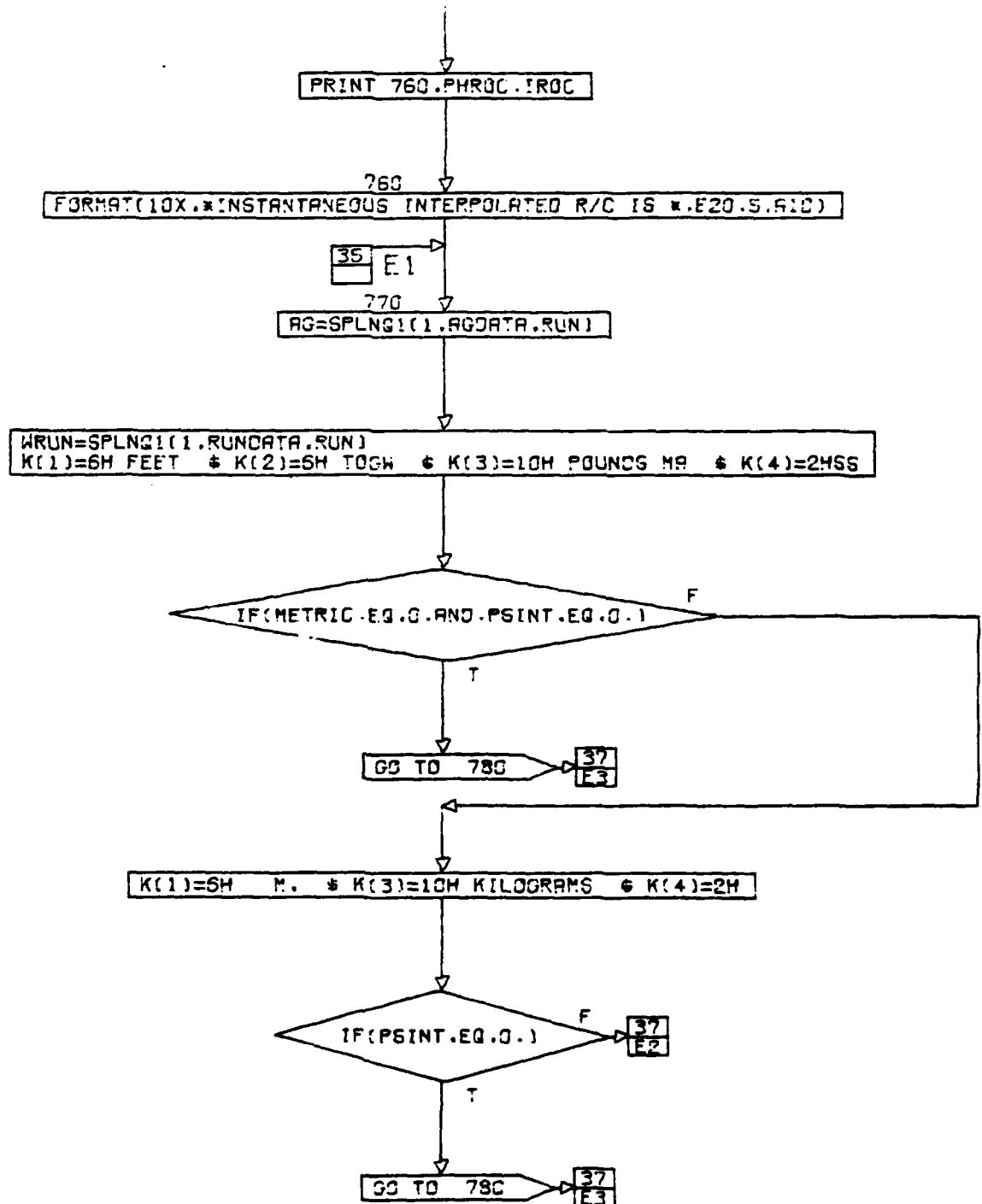
FILED

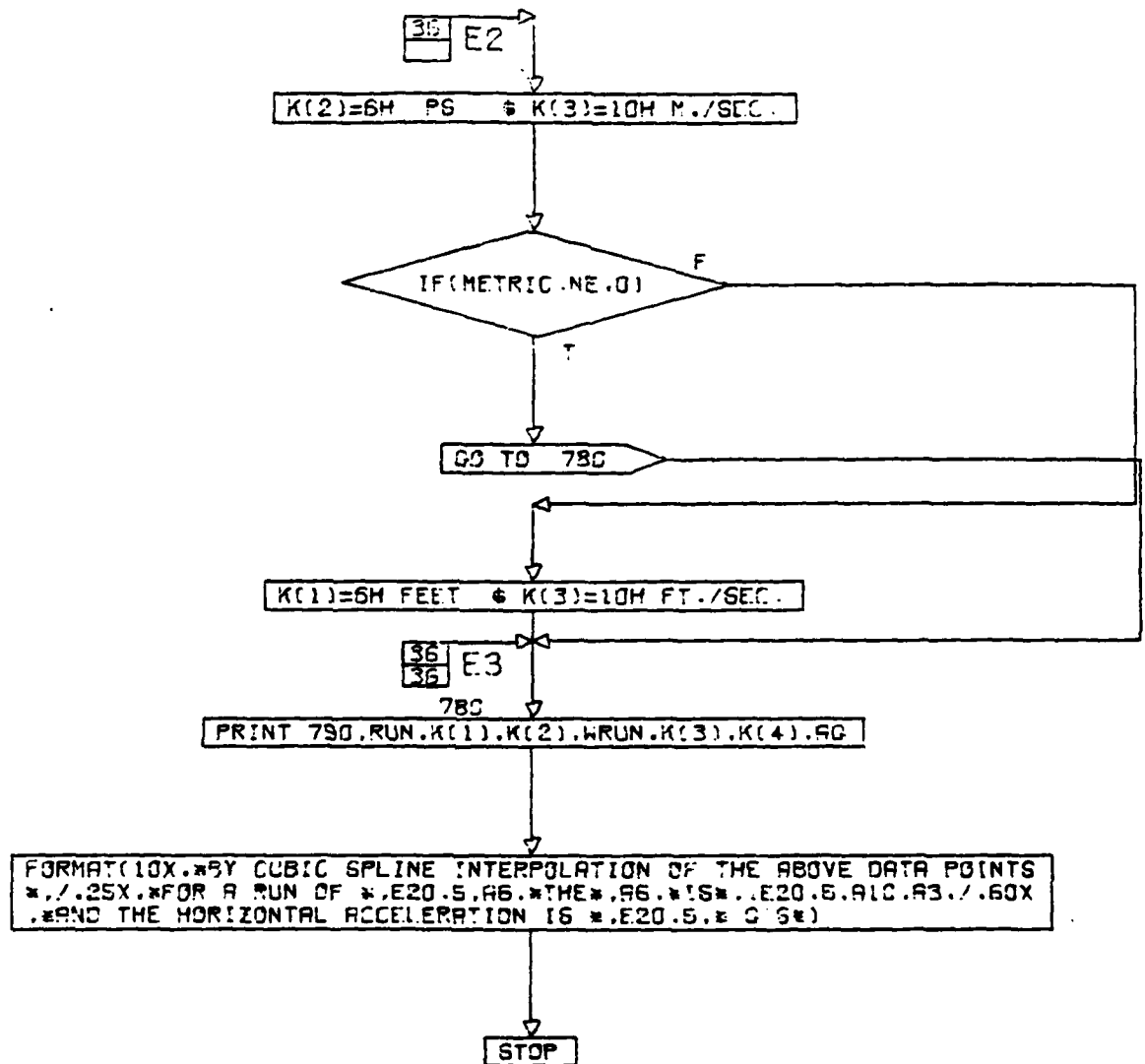
2 82

DTIC

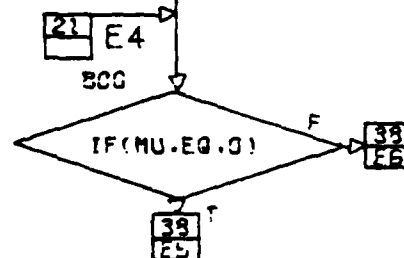


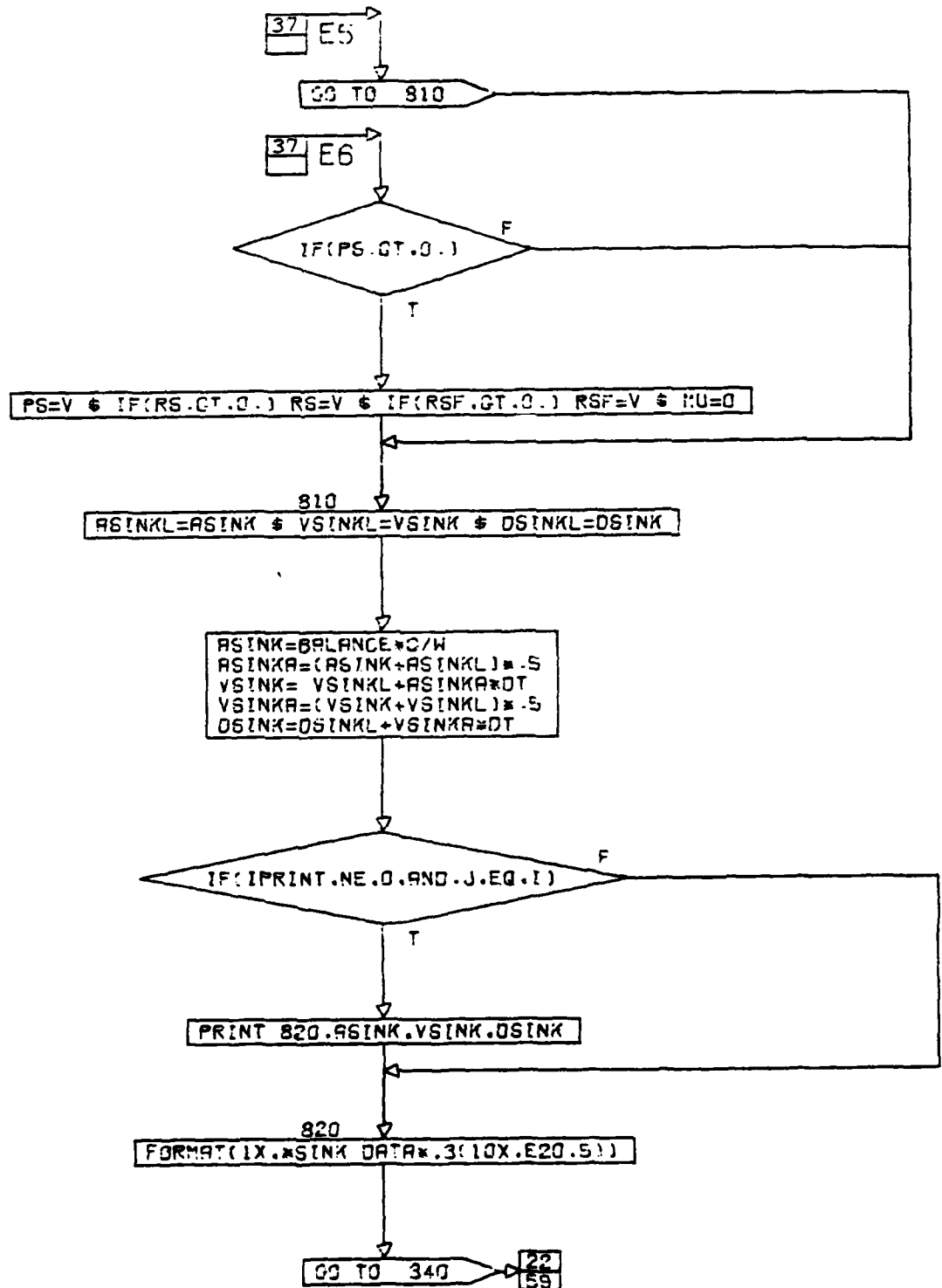


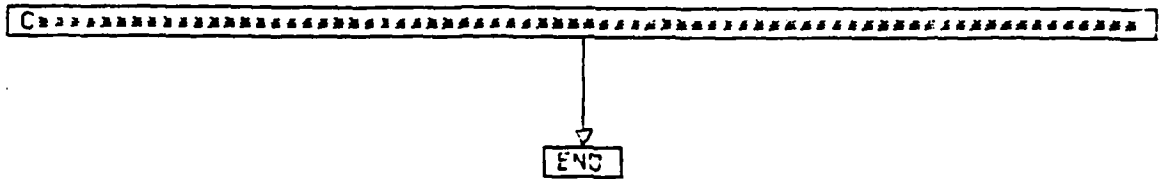


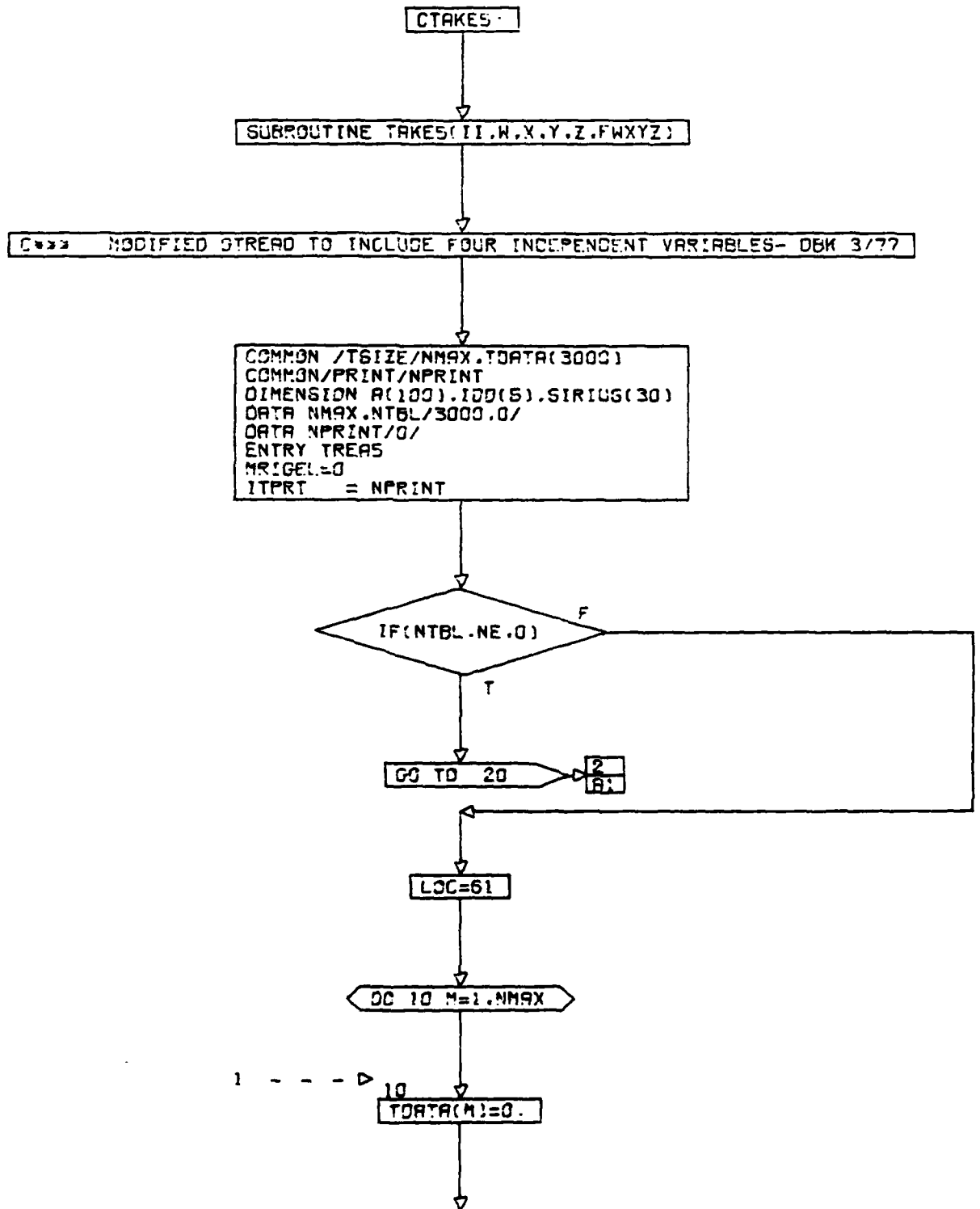


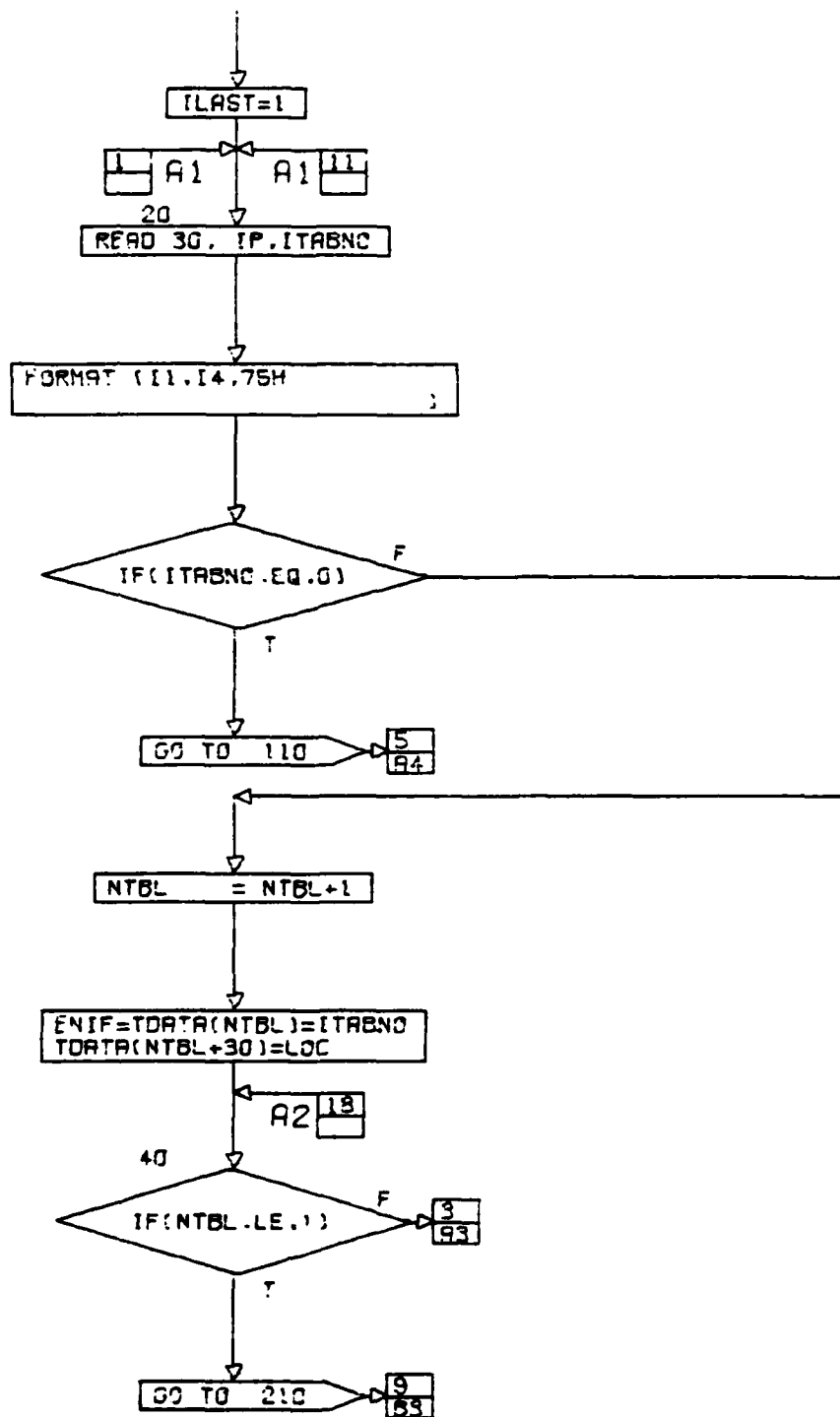
C2???????????????? SINK OFF THE BOW CALCULATIONS

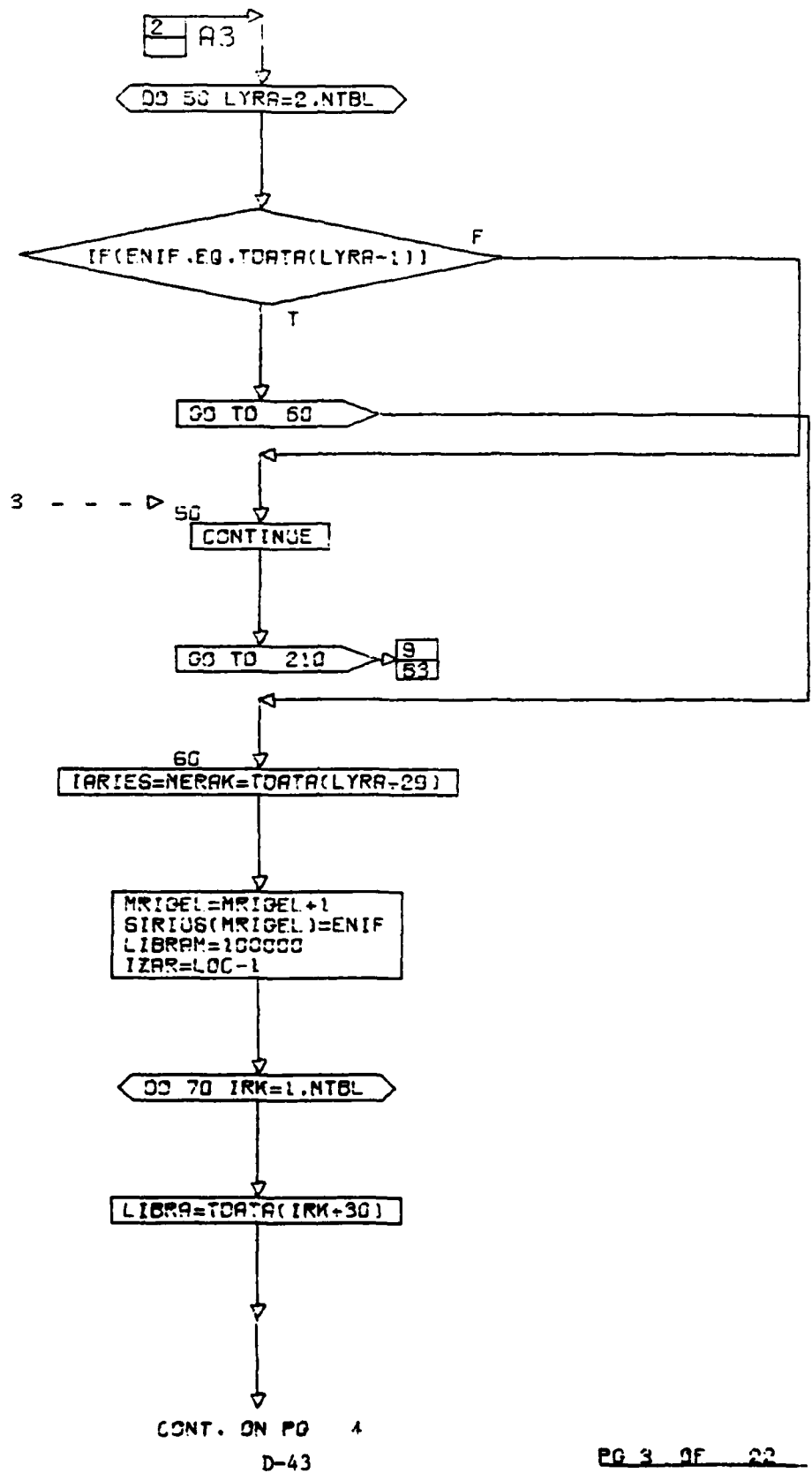


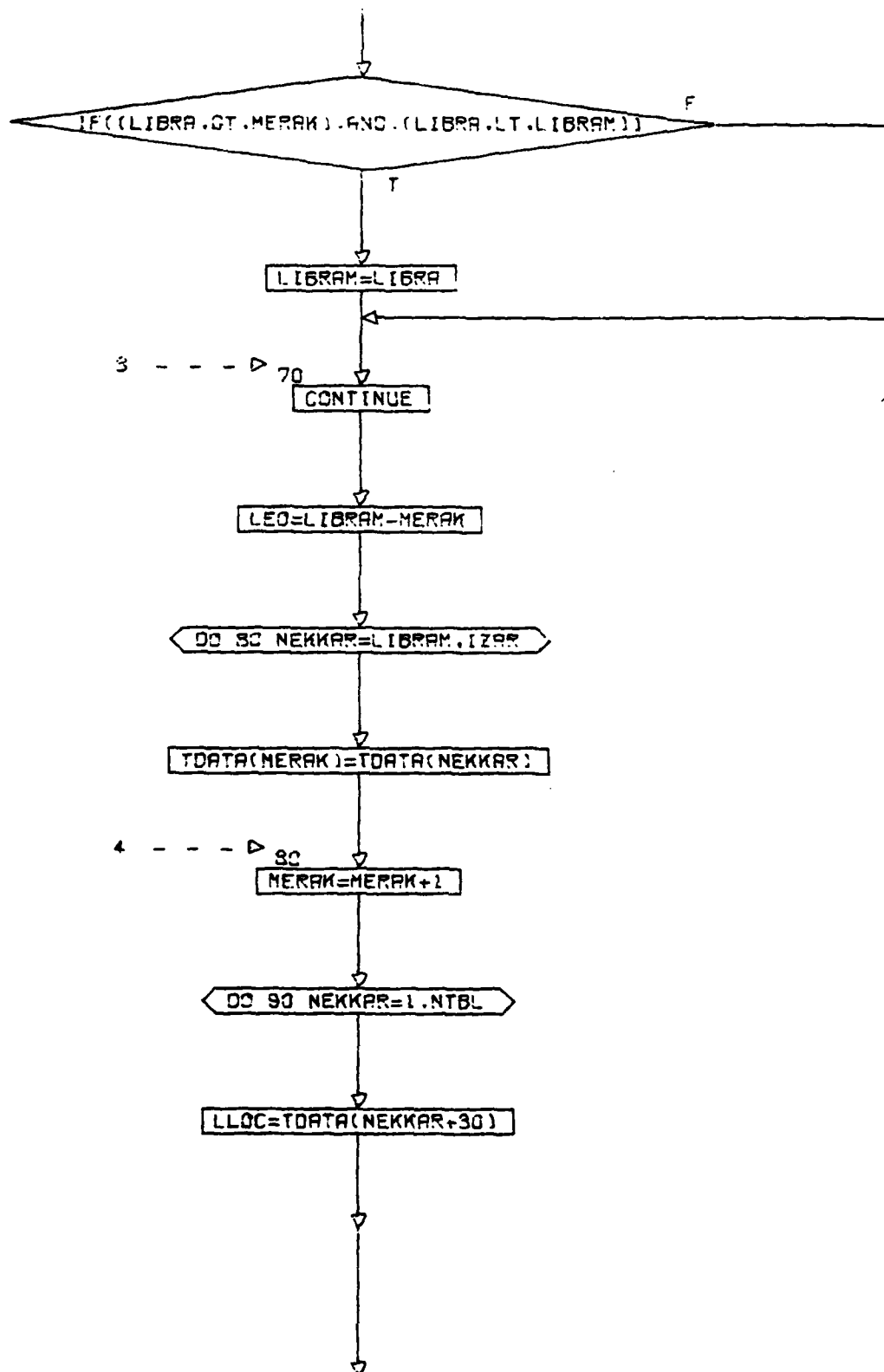








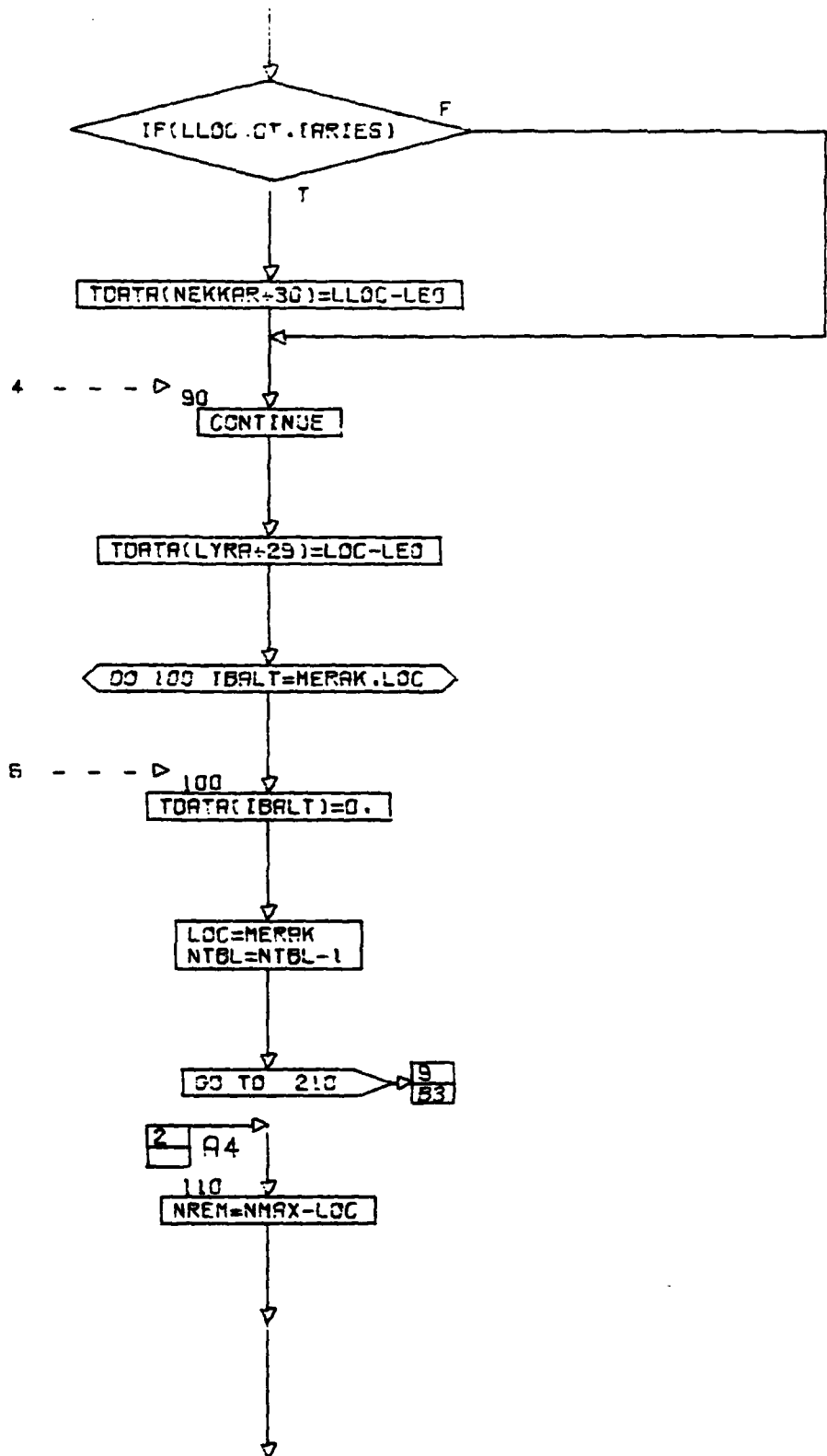




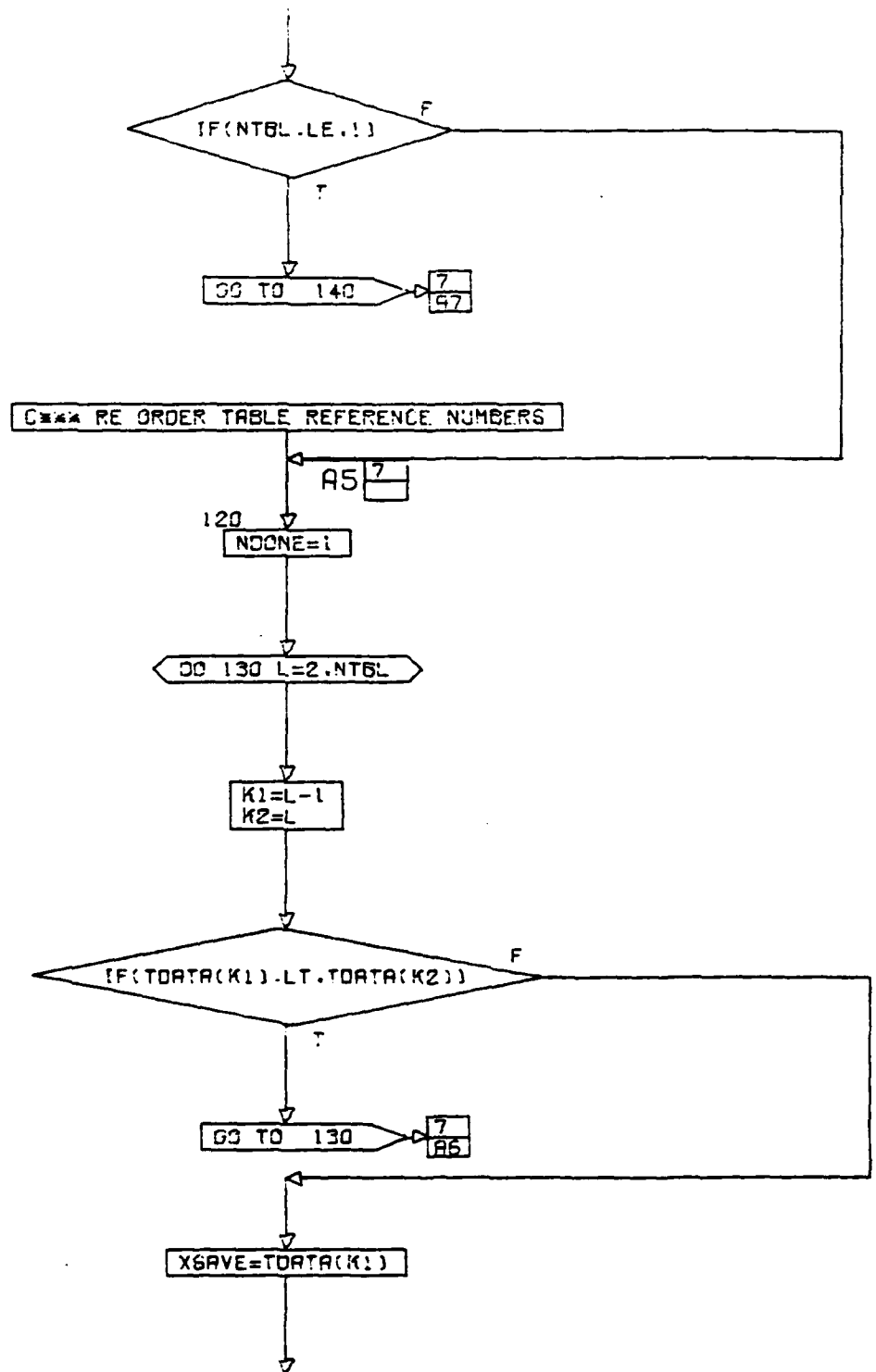
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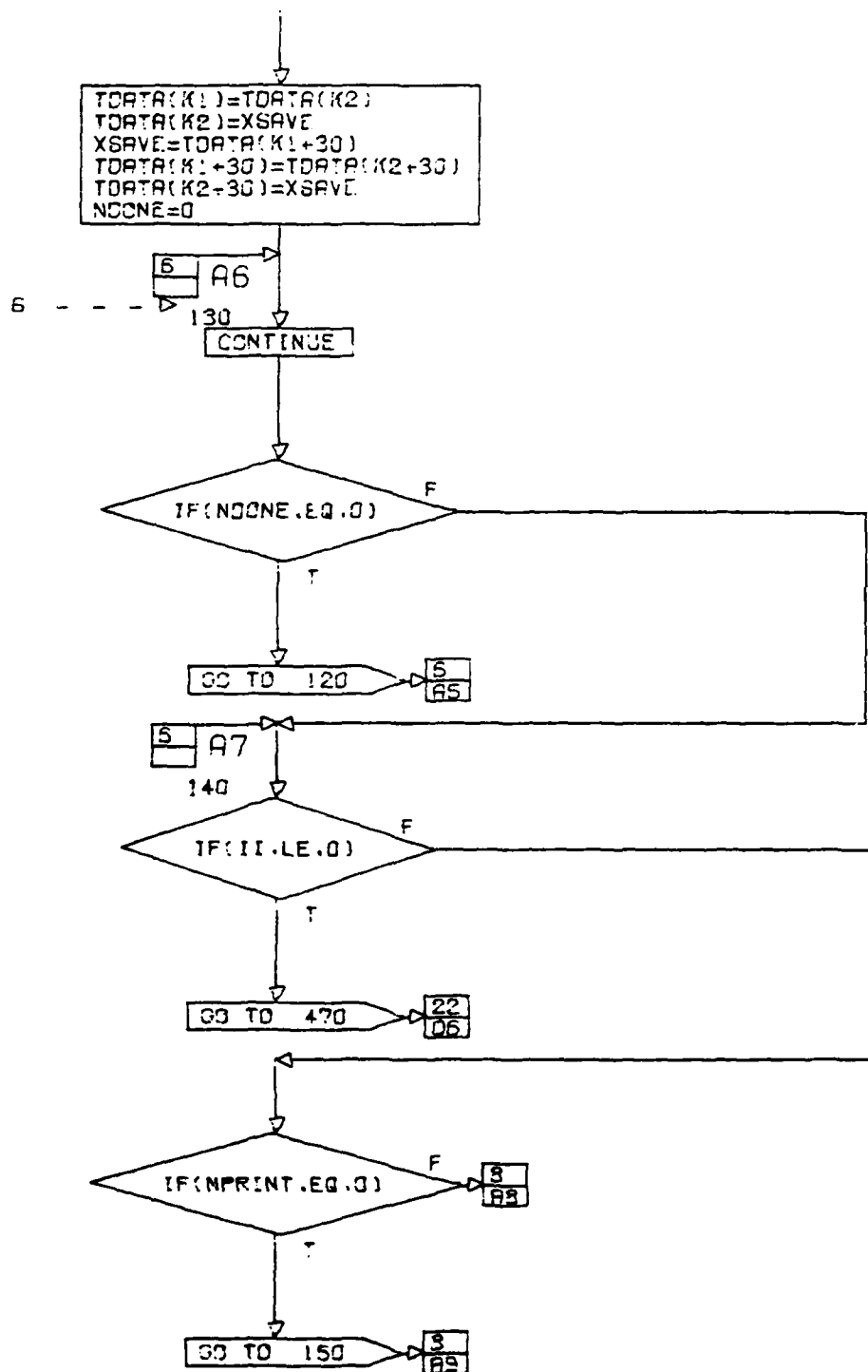
D-44

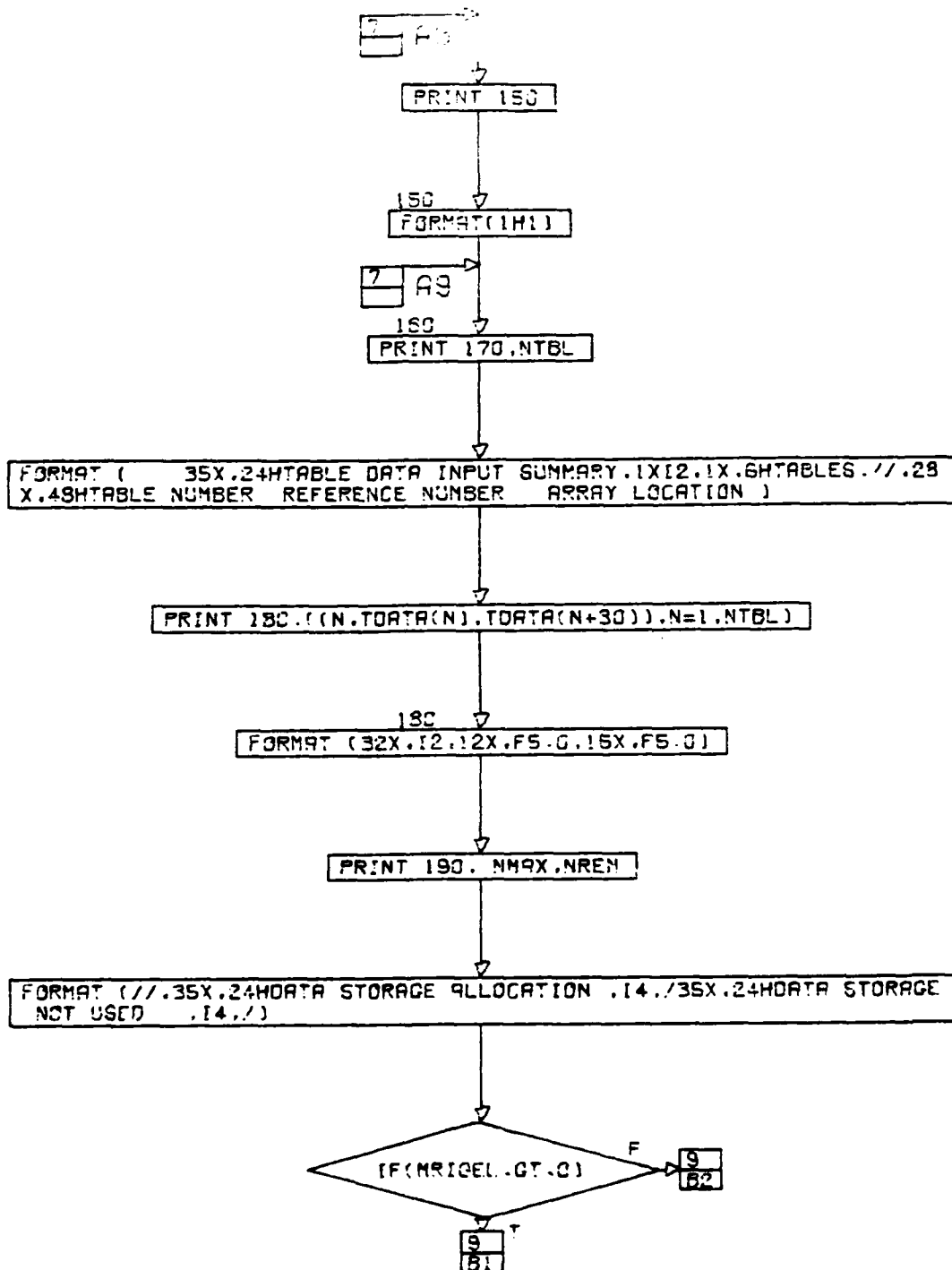
PG 4 OF 22

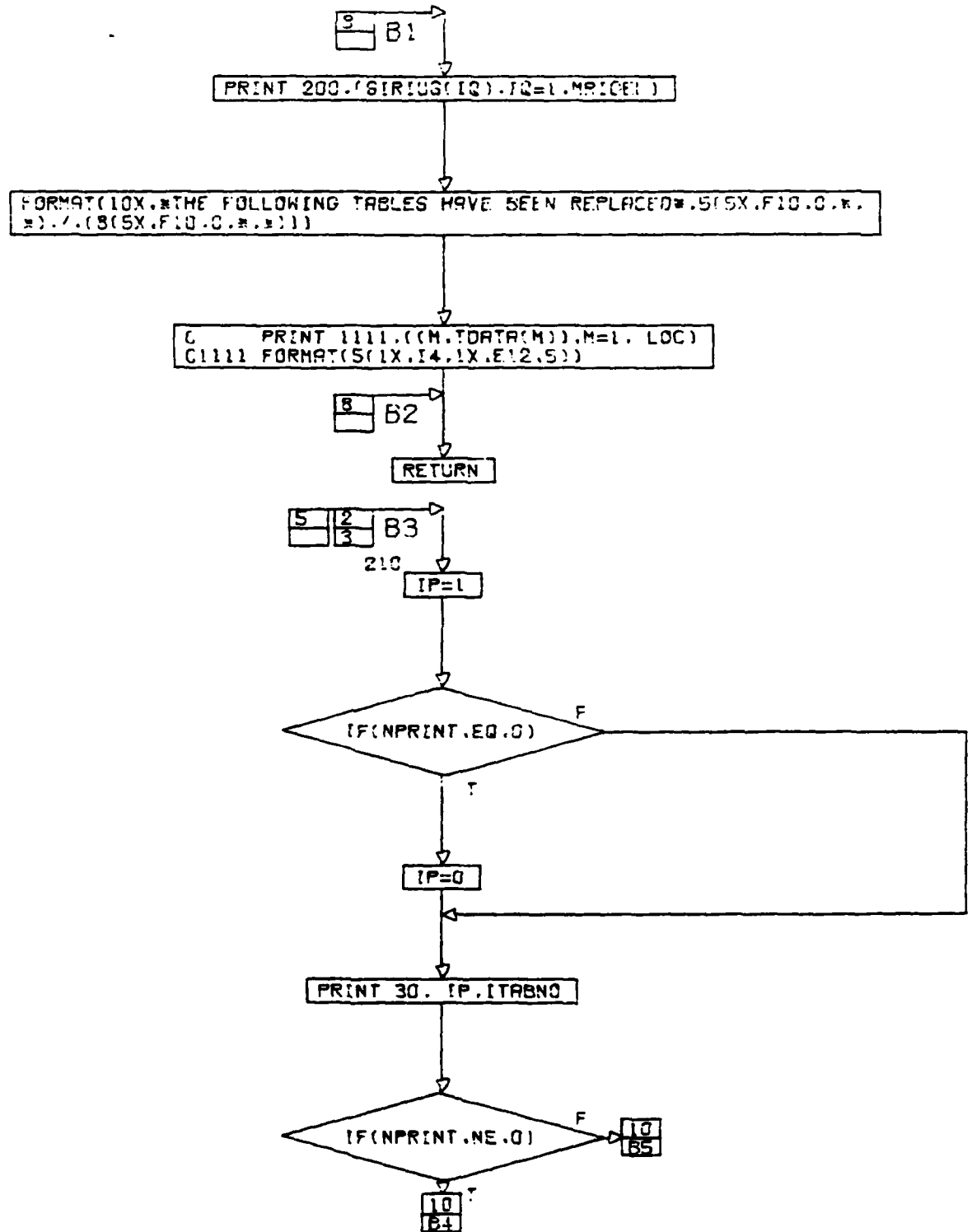


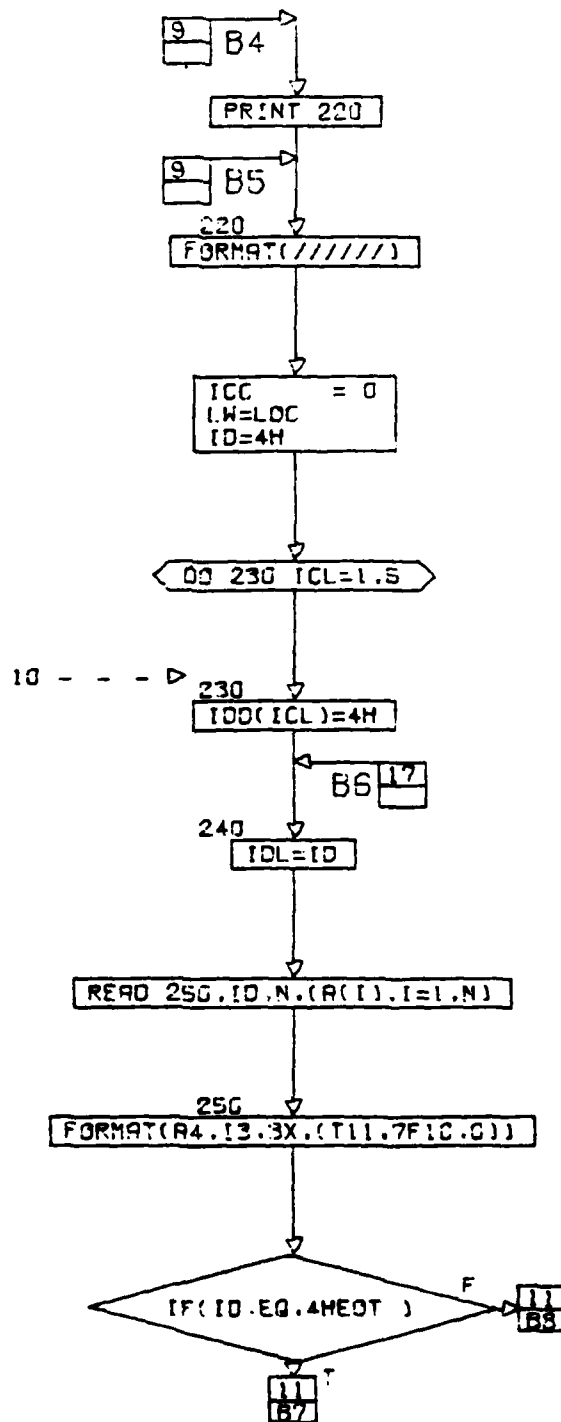
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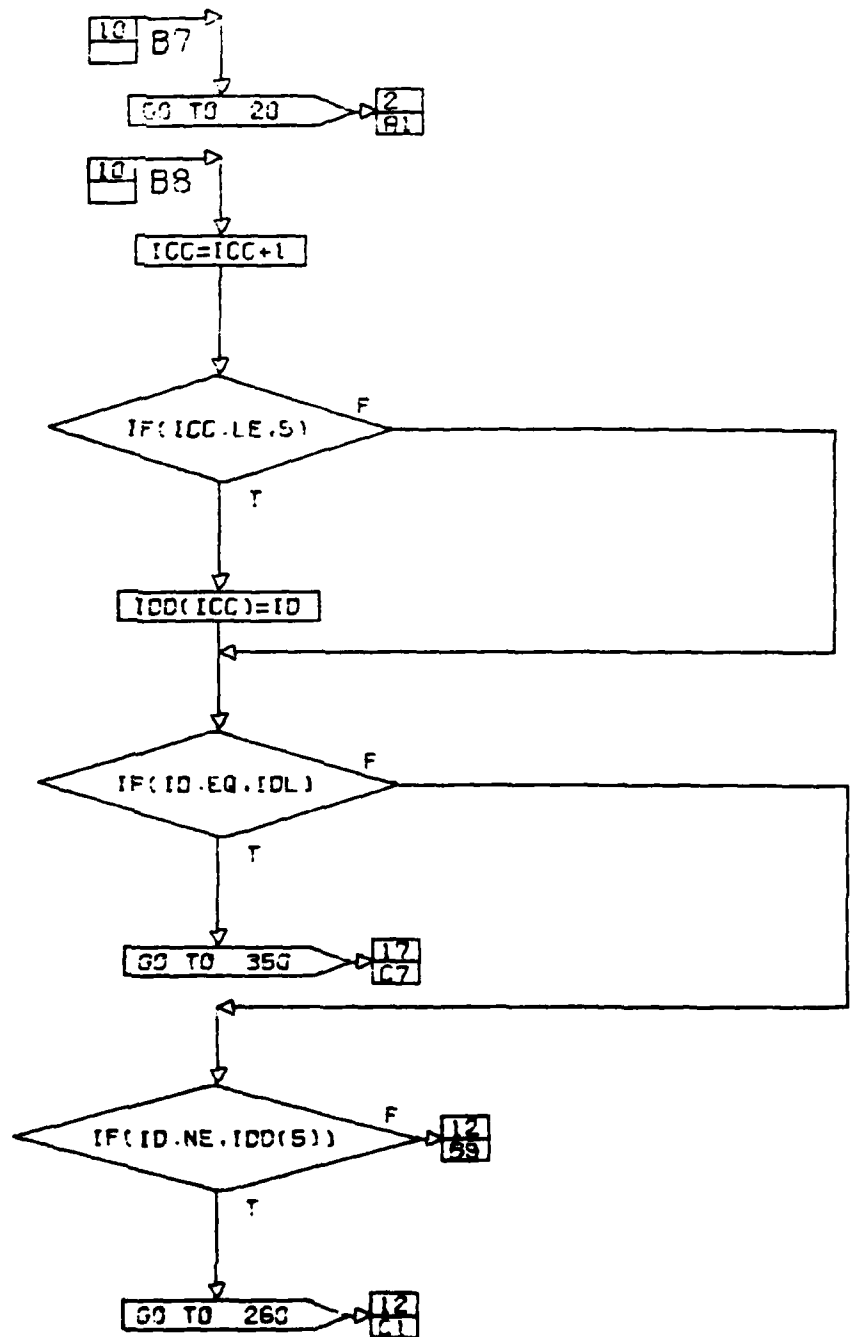


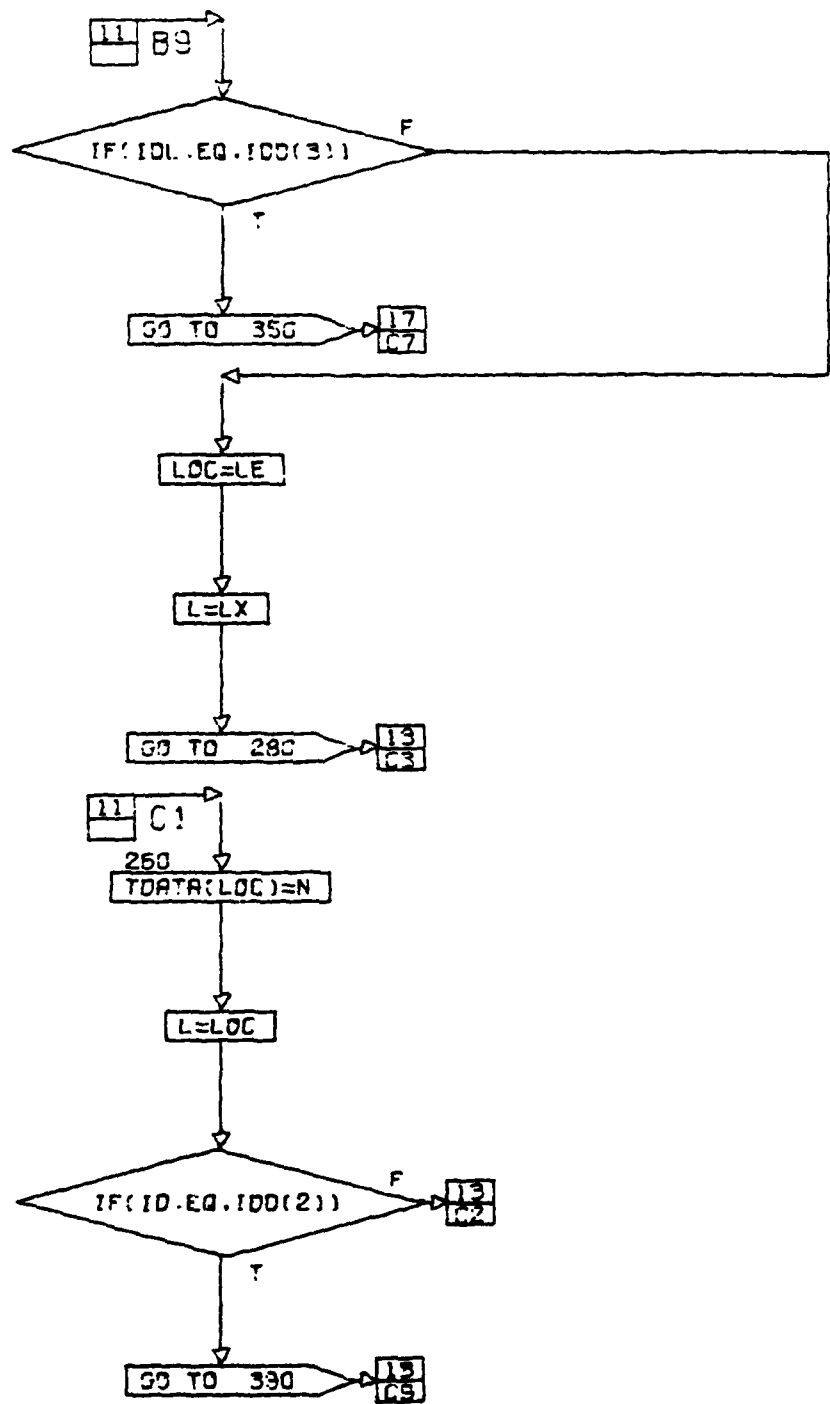


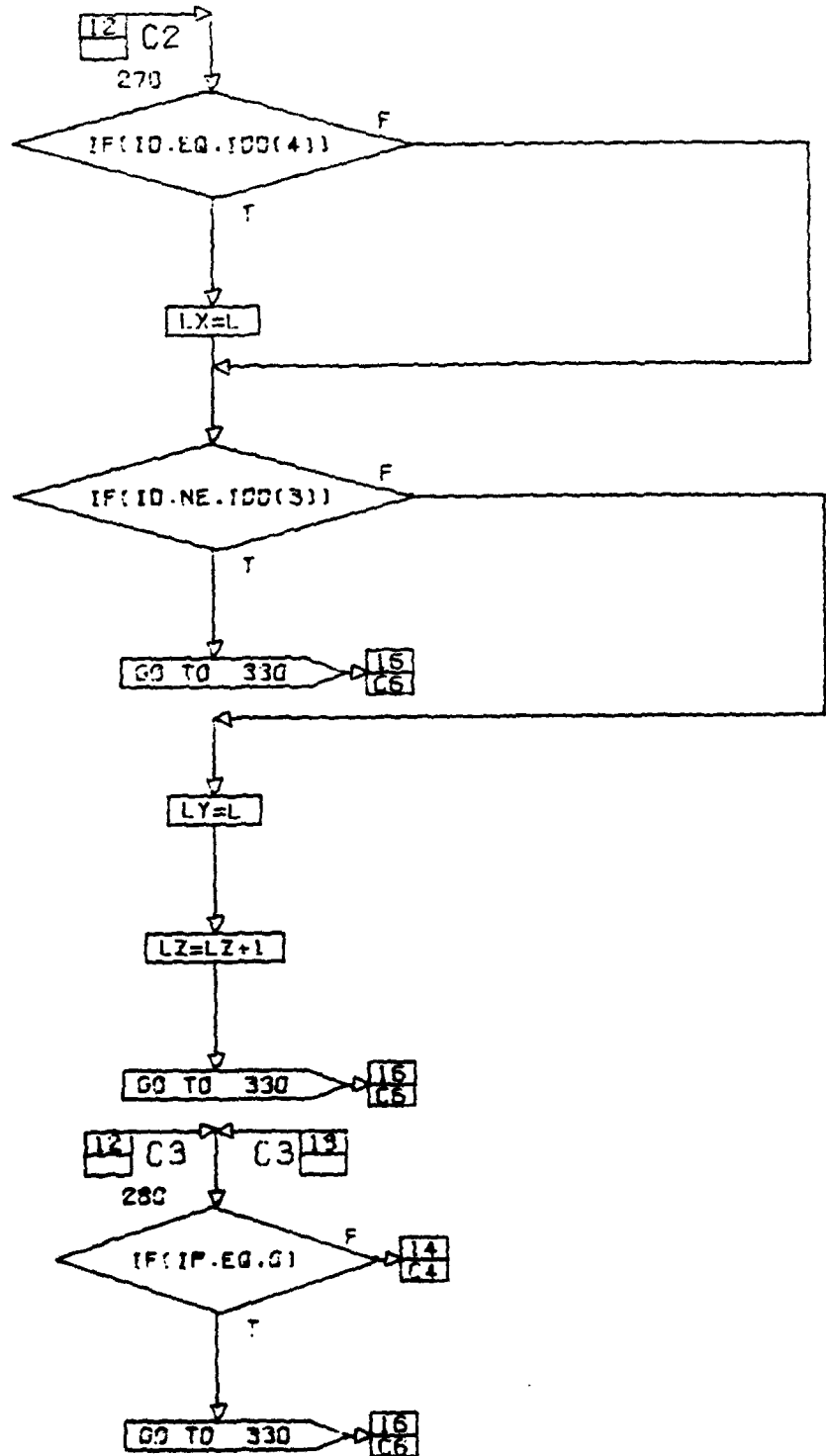


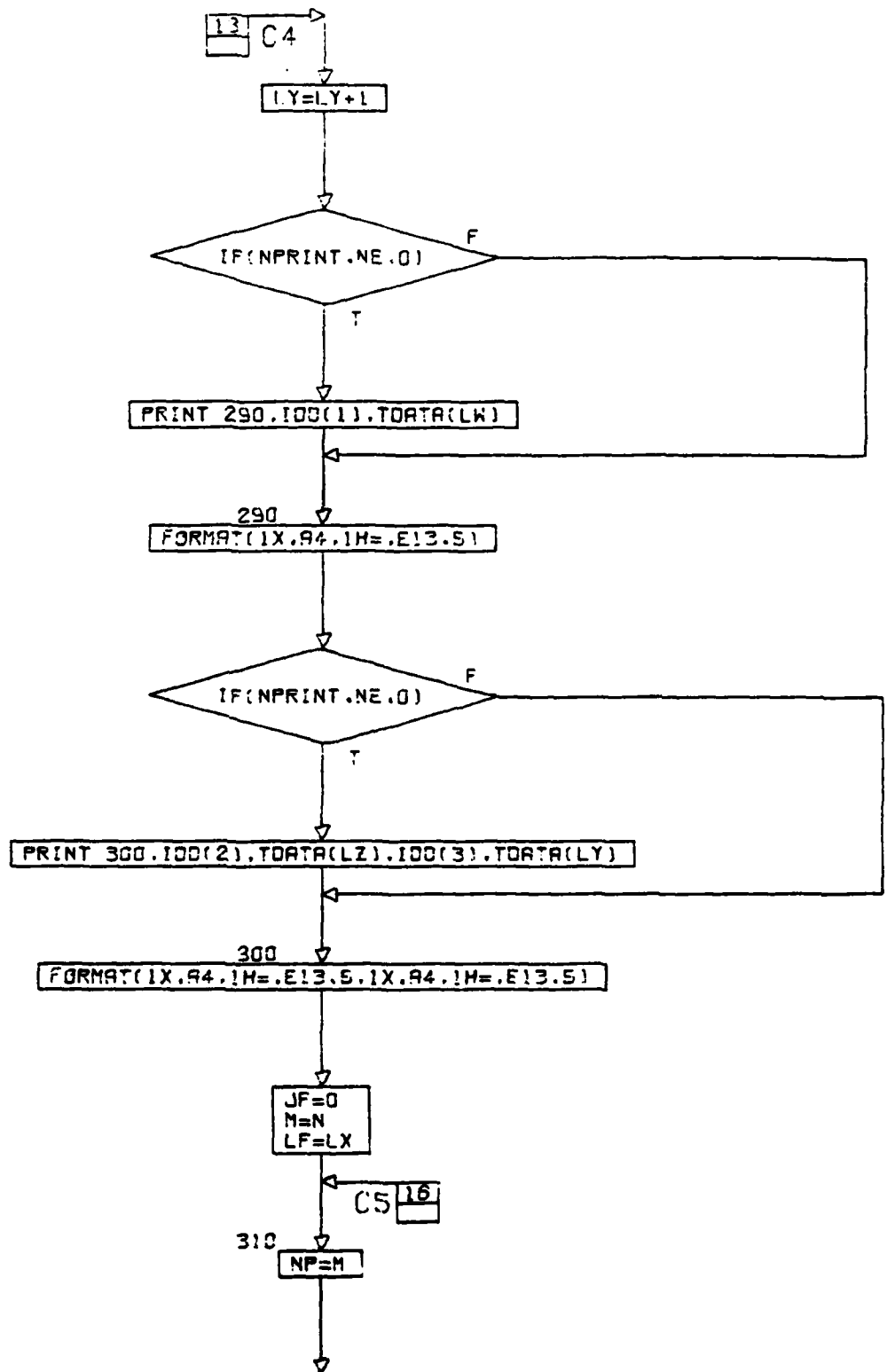


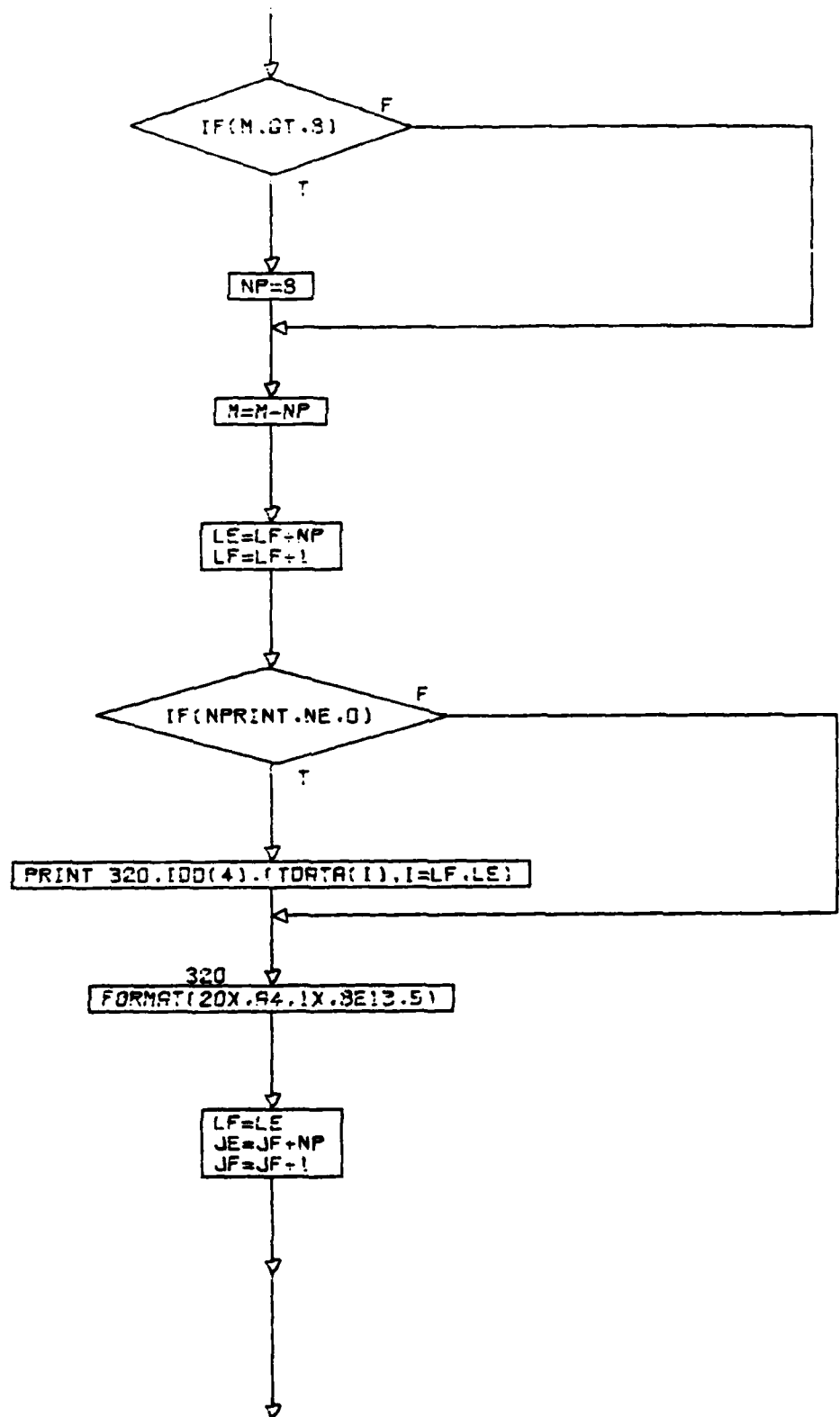


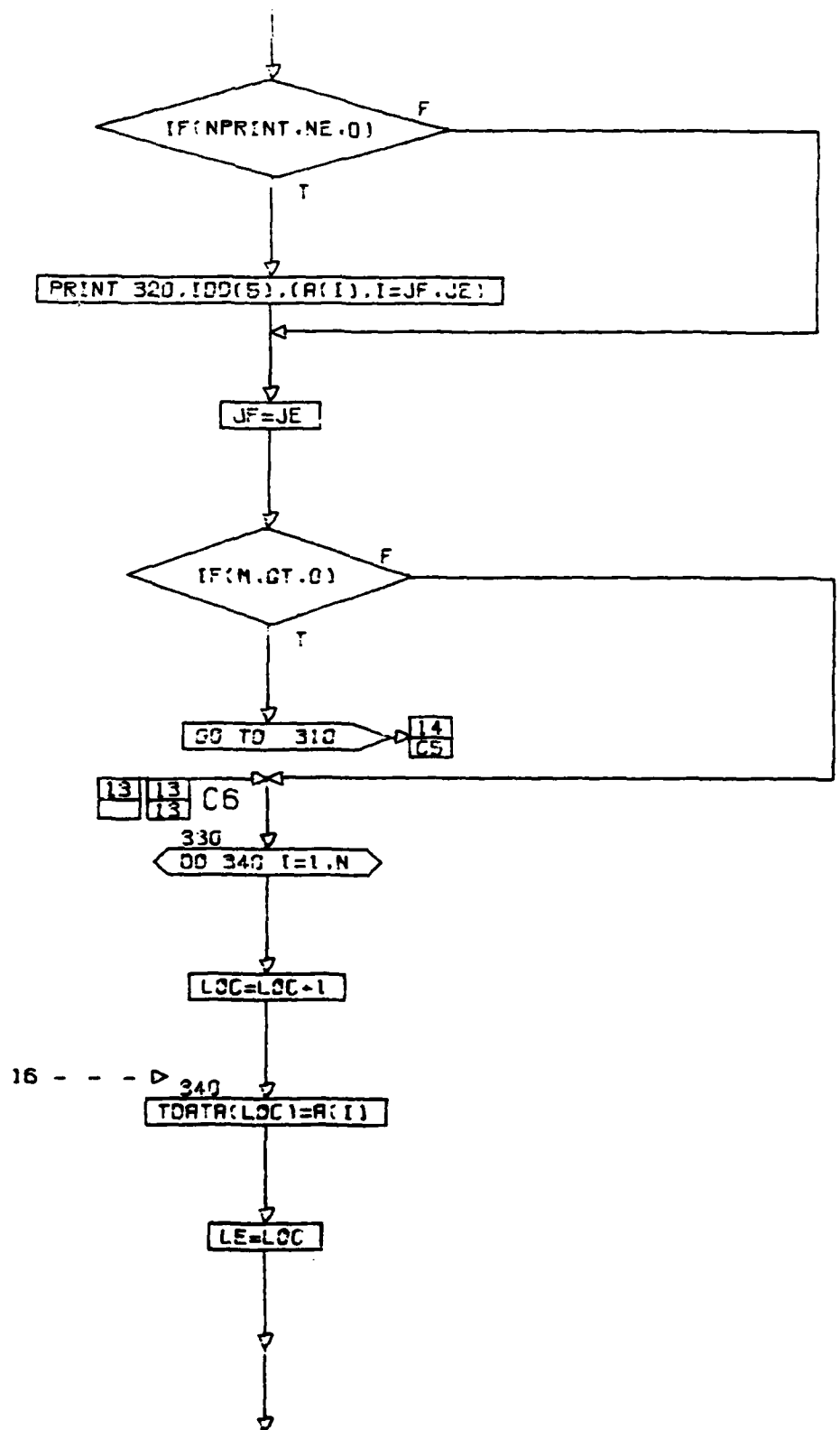


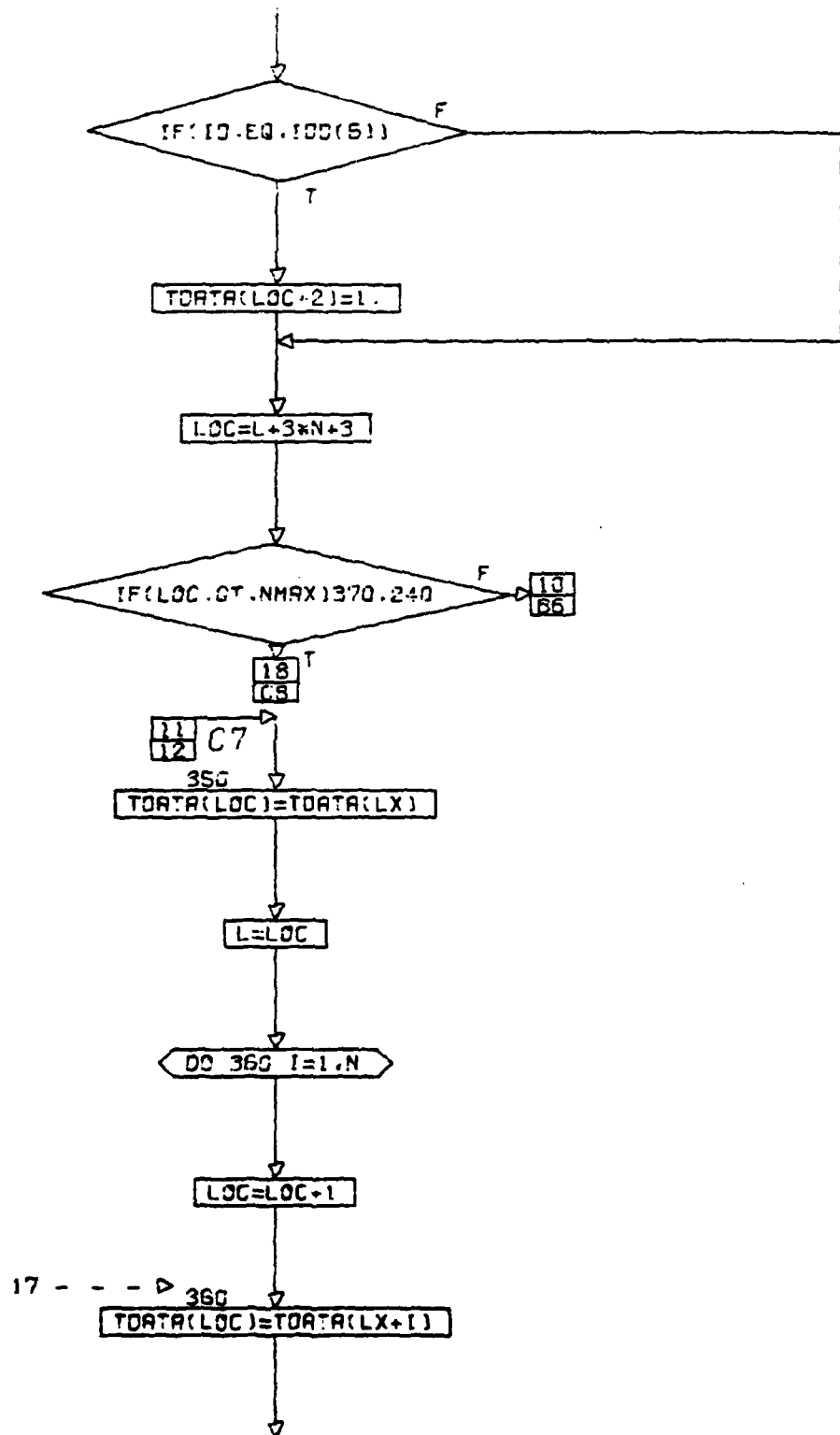


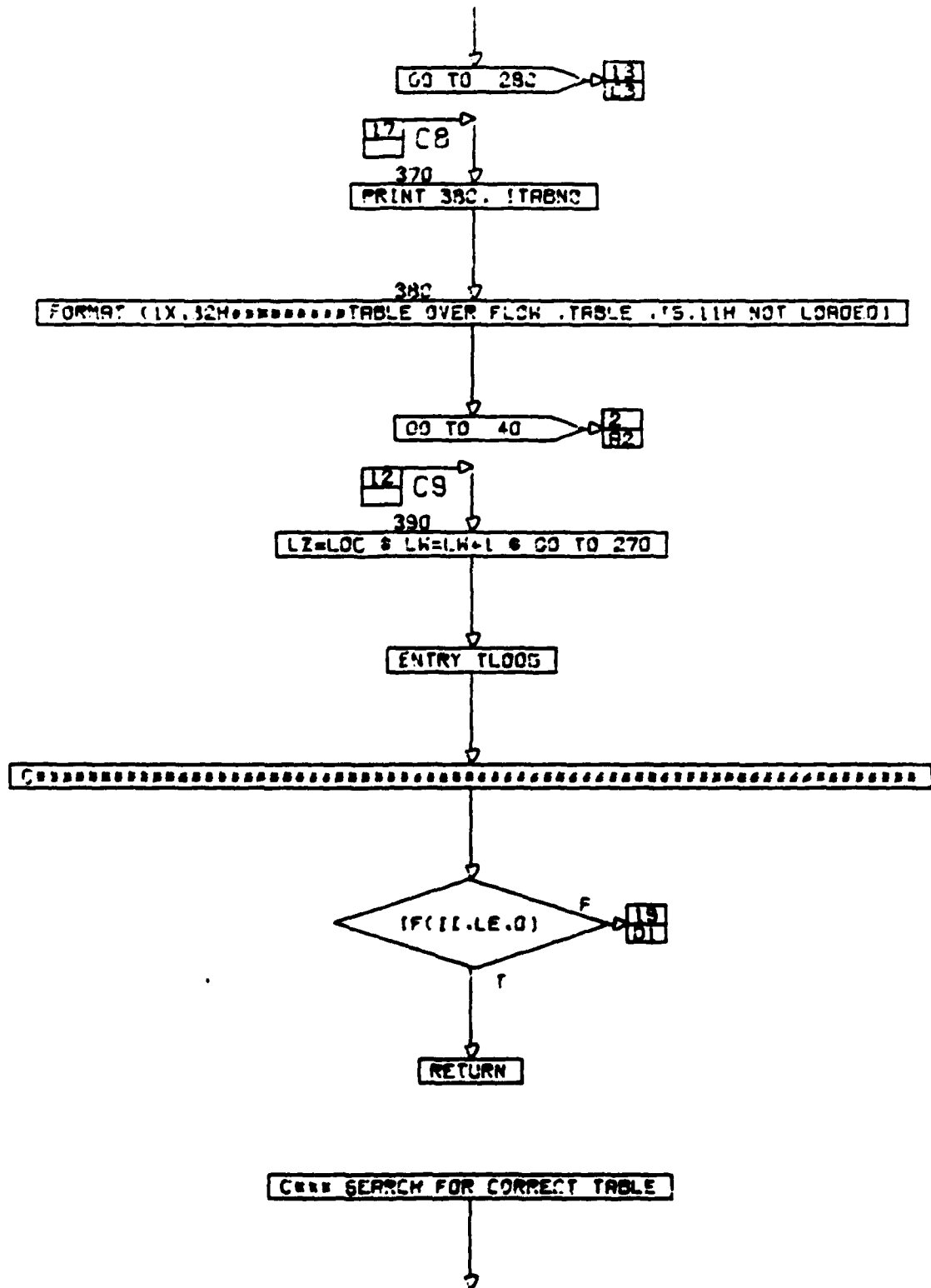


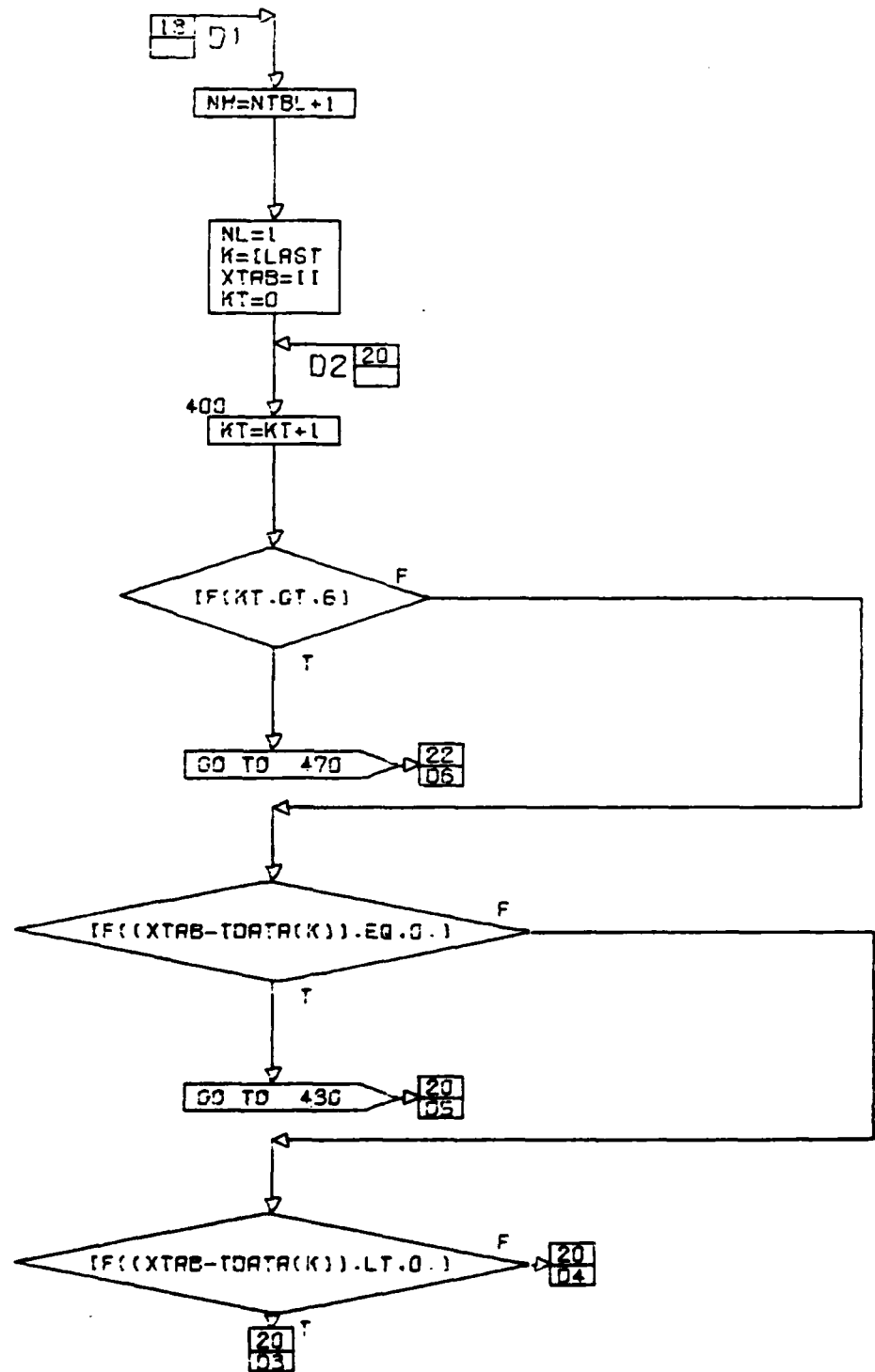


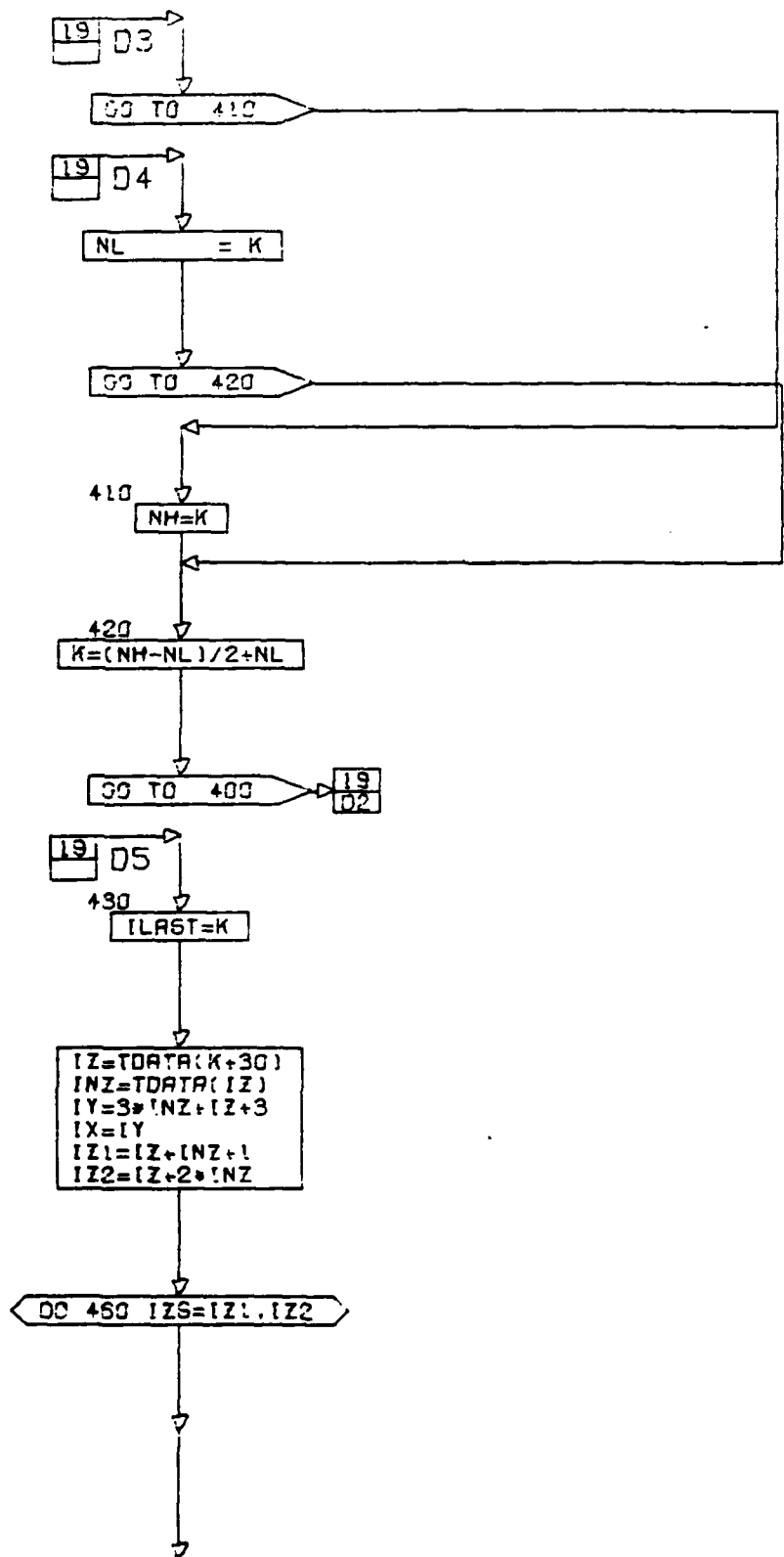


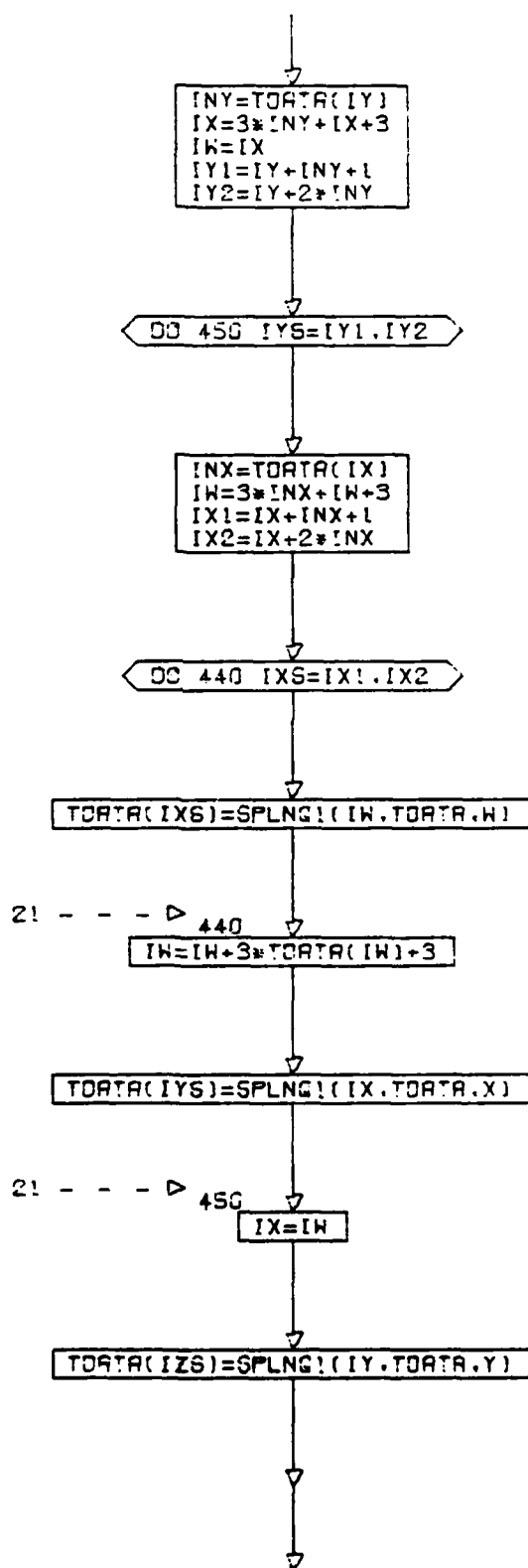




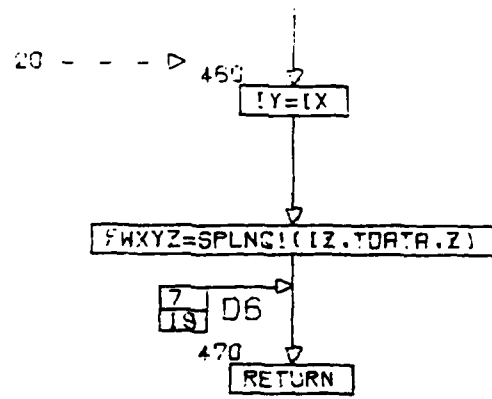








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